

CITY OF LAS VEGAS		DATE:
INTER-OFFICE MEMORANDUM		March 24, 2016
TO: Land Development Services Department of Building & Safety		FROM: Albert Sung, P.E. Flood Control Project Engineer Department of Public Works
SUBJECT:	Drainage Study for: The SEVENTY	COPIES TO: GCW Engineers
Cross Streets:	SWC of Rampart & Alta	Seventy Acres LLC
File Number:	F:\Depot\DSMemos\DS4787A.ZNA.doc	Bart Anderson, P.E., DevCo
Parcel Number:	138-32-301-005, 006, 210-008	CCRFCD
Zoning Action:	SDR-62393; GPA-62387; ZON-62392	
FEMA Flood Zone	YES X NO	
Proposed Storm Drain	YES X NO	

HISTORY	DATE RECEIVED	DATE REVIEWED	COMMENTS	REVIEW FEES	FEES PAID Payment Trn #
1 st Submittal	3/3/2016 & 3/9/2016	3/23/2016	See Comments Below	\$400.00	425231: \$400
TOTAL FEES (LDDRS):				\$400.00	----

REMARKS: This site development is within a FEMA SPECIAL FLOOD HAZARD AREA, Zone A. No permits of any kind will be issued for this project until a Conditional Letter of Map Revision (CLOMR/CLOMR-F) is received from FEMA.

The Drainage Study for the subject project has been reviewed and:

	is approved subject to conformance to all City standards and the following conditions:
X	must be resubmitted or supplemented including the following:
	is conditionally approved subject to Clark County Regional Flood Control District concurrence.
	is conditionally approved subject to NDOT concurrence.

1. This site development is located within a FEMA SPECIAL FLOOD HAZARD AREA, Zone A. **No permits will be issued until a Conditional Letter of Map Revision (CLOMR/CLOMR-F) is received from FEMA. Permits may be issued upon the receipt of Conditional Letter of Map Revision (CLOMR or CLOMR-F) from FEMA.**
2. A Letter of Map Revision (LOMR/LOMR-F) must be obtained from FEMA after the completion of any project within a FEMA Special Flood Hazard Area, Flood Zone "A". The bonded improvements shall include a line item of **\$50,000.00** for the LOMR. The bonded improvements will not be released until the LOMR/LOMR-F is obtained from FEMA and filed with the City of Las Vegas.
3. Sites with a grade difference of 2 feet above or below existing are required to have approval from the *City Planning and Development Department*. The engineer must submit copies of the grading plans and detail sheet with a letter justifying the grade difference to the *City Planning Department* (229-6301). The engineer must provide Planning approval with the next submittal.
4. The site is located within the Flood Zone A and is adjacent to an existing or proposed *Clark County Regional Flood Control District* (CCRFCD) master planned facility. Therefore, CCRFCD concurrence is required prior to final approval of the drainage study.

5. Please obtain necessary 404 permits from US Army Corps of Engineers and provide a copy of the permit to City of Las Vegas Flood Control Section prior to issuance of the grading permit. Contact the St. George Field Office of the US Army Corps of Engineers for permit information.
6. Provide a comparison table between the 2013 MPU flow rates and the proposed condition at key system locations. The system design shall use the greater flow rates in the analysis. Review and revise the flows accordingly and resubmit the updated analysis. Once the updated analysis is confirmed, update the Report, Tables and Exhibits to match the revised flows.
7. Review the Development Area 4 drainage parameters to refine the density of the lot sizes in the various locations to better determine the drainage impacts of this 183 acre area. Update the hydrology of this area to reflect the impacts of the proposed development.
8. The proposed RCB system velocities are excessive and are routinely above 35 fps. This is well above the allowable 25 fps in the HCDDM. Review and revise the RCB design to reduce the velocity to a maximum of 35 fps. Review the overall impacts to the proposed RCB system to take into account the future upstream system extensions to see where the system can be modified to reduce the velocity within the RCB's. Velocities above 25 fps shall include additional design parameters to mitigate the high velocities. Discuss the mitigation options and recommendations for City and CCRFCD approval.
9. The provided WSPG analysis used an *n-value* of 0.015. Provide an additional WSPG analysis of the two main line RCB's using 0.013 for sensitivity analysis to see the impacts to the velocity.
10. Include new cross sections that incorporate the detailed grading plans for the inlet structures within the HEC-RAS analysis.
11. Provide an overall exhibit that shows the entire storm drain system, labels the publically maintained storm drain system and all maintenance access roads on a single sheet.
12. Proposed storm drain laterals have been identified to collect flows from Peccole West Lot 9 and Queensridge Fairway Homes. Extend the storm drain system to collect the 100-year flows from these adjacent subdivisions.
13. The proposed facilities will be a change to the existing CCRFCD Master Plan and will necessitate a Master Plan Change (MPC) with Regional Flood. Flood Control recommends that the MPC be included with the next Master Plan Update and not be a separate submittal with this project. Coordinate the MPC information and requirements with Regional Flood.
14. The referenced FEMA flow rates used in the downstream analysis are slightly lower than the fully developed condition values. Flood Control shall require that the FEMA analysis include the fully developed condition in the CLOMR request for this project.
15. Provide complete *Plans and Project Specifications* for approval by the *City of Las Vegas*. The Structural Plans and Details shall be a part of the Civil Improvement Plan set. This project is considered as a *Capital Improvement Project* (CIP) with developer funding.
16. Structural plans for the proposed storm drain improvements and pertinent flood control facilities must be submitted for review. Provide a soils report, structural calculations and specifications, two wet stamped structural sets, and a grading plan to the *Building Department* for processing. The engineer must provide a copy of *Building Department* approval of the structures to *Flood Control* prior to final acceptance of the drainage study.
17. All proposed improvements associated with the Storm Drain facilities shall be bonded and inspected. This project shall require Special Inspection. Coordinate the requirements of and the Agreements needed for Special Inspection with the Building Department.

18. The proposed improvements show drainage facilities of a size that must be reviewed for access and maintenance concerns. The engineer must submit an extra set of improvement plans to the *City Streets & Sanitation Department* for their review and comments. *Streets & Sanitation Department's* approval must be secured prior to the conditional drainage study approval.
19. Storm drain facilities are located on cut/fill slopes. Revise the slopes and/or the storm drain alignment to maintain 16-foot access roads. Provide a cross section detail of the maintenance access.
20. Provide a minimum 25-foot concrete pad at the inlet structures of the RCB's to allow for proper maintenance. Include 16-foot wide concrete access ramps (10% maximum slope) to the RCB inverts. Provide detailed grading plans for all of the inlet structures as well as grading transitions. Provide cross sections of these facilities.
21. Provide a concrete pad and maintenance access to the inlet structures for the local storm drains. Show the needed drainage easements for these facilities.
22. The plans show preliminary mass grading with collection facilities within the parcels to intercept the flows prior to entering the infrastructure drainage improvements. The inlet collection system needs to incorporate stormwater quality (SWQ) features and Best Management Practices (BMP's) at these interim collection points. Revise to incorporate appropriate SWQ and BMP measures. How will these collection facilities be maintained without graded access to the structures?
23. Provide maintenance access road (12-foot wide with a minimum of 6" Type II) to manholes and discharge structures located outside of the improved roadways.
24. Revise the storm drain lateral layouts to eliminate the main line lateral bends and concrete collars. Provide manholes for change in alignment and grade.
25. Provide plan and profile for all proposed storm drain improvements. Include the Q and HGL on all profiles.
26. Relocate manholes to the sides of the RCB's and at a maximum 400-foot spacing. Provide manhole steps and provide 30-inch manhole covers for access. Show concrete collars for the manholes.
27. Verify and correctly label the existing drainage and sewer easements. Provide an Exhibit that shows the drainage easements that are being Vacated and an Exhibit that shows the proposed easements.
28. Provide for the new public drainage easements (privately maintained by the property owner) for the area of the site impacted by the proposed improvements. The easement shall note that the private drainage improvements are privately maintained and the easement must be dedicated and recorded by separate document prior to the final acceptance of the improvement plans. Provide legal description and an exhibit of the drainage easement to Flood Control and *Mary Wulff* (702-229-2139) of *City of Las Vegas Right of Way Section* for the recordation process after the subject drainage study is conceptually approved.
29. The existing and proposed utility crossings of the storm drain must be shown on the storm drain plan and profiles sheets and on the lateral profiles. Indicate the type of pipe material for water and sewer lines. Review separation requirements between utilities and show all of the utility crossings of the storm drains.
30. Show the size of the proposed riprap areas and include a detail on the plans. Include the Type 2 and geofabric in the detail section. It is noted that the minimum size of a riprap pad is $d_{50}=8"$. Revise all pertinent plans and callouts accordingly.
31. Technical drainage studies are required for each of the future development super pads. The technical drainage studies for the developments may not be submitted until the conditional approval

of this pertinent infrastructure drainage study is obtained. Final approval for the infrastructure study must be obtained prior to conditional approval of the impacted development super pad drainage studies.

32. The proposed on-site drainage facilities are to be privately maintained. Add a note to the grading plan that *"All on-site surface drainage facilities are to be privately maintained."*
33. Complete the Construction Notes on the Grading Plan including pavement section and reference details for the call-outs of proposed improvements, i.e. RCB's, rip-rap, structure details, manholes, inlets, etc.
34. Provide a note on all grading plans: Property Owner is responsible to maintain the best management practices such as but not limited to the removal of accumulated sediment and debris and care of the vegetation.
35. This project currently has no Proposed Buildings or Structures. Should the project propose changes to this design assumption, then the Engineer is to update the drainage study detailing the flood zone impacts and provide addresses for each building in a FEMA Flood Hazard Zone prior to obtaining a grading permit. This information is necessary to insure that the elevation certificates are provided for each address prior to completion of construction. This information is required until such time as a LOMR is approved that removes the development from the SFHA.

NOTE: Please be advised that all land surface area disturbances over 1 acre or any area adjacent to a water way must submit to the *Nevada Division of Environmental Protection* a "Notice of Intent" to discharge that certifies a stormwater pollution prevention plan has been developed and is maintained on site; for inclusion in the Stormwater General Permit No. NVR100000. A phased construction unit in a contiguous subdivision is considered under construction until all stripped or disturbed surface areas have been covered by paving, building construction or planting. For more information, including forms and applications see <http://ndep.nv.gov/bwpc/storm01.htm> or call (775) 687-9429.

NOTE: The engineer must submit the drainage study to FEMA for a Conditional Letter of Map Revision (CLOMR). A favorable CLOMR must be obtained prior to the issuance of any permits. This site is located in a FEMA Zone A. Clark County Regional Flood Control District (CCRFCD) review and approval is required prior to recordation of final map or issuance of building/grading permits. The Engineer must send a copy of the report to the CCRFCD for review. The developer/engineer must also obtain a Letter of Map Revision (LOMR) using the approved drainage study as technical support to inform FEMA of the modifications within the flood zone. The approved LOMR must be submitted to the City of Las Vegas prior to the release of the bond. FEMA Elevation Certificates, showing as-built finish floor elevations, must be completed for each building in the FEMA A Zone. The certificate must be submitted to the City of Las Vegas Flood Control Section prior to scheduling a framing inspection.

END OF REMARKS
Ays/pbj

T/R/S: T20S/R60E/12
AREA L-32

**TECHNICAL DRAINAGE STUDY
FOR
THE SEVENTY**

840-050

March 2016

Prepared For:

**Seventy Acres LLC, Fore Stars LTD, and 180 Land Co LLC
9775 West Charleston Boulevard
Las Vegas, NV 89117
Phone: (702) 940-6930
Fax: (702) 940-6931**

GCV
ENGINEERS \ SURVEYORS

HYDROLOGIC CRITERIA AND DRAINAGE MANUAL

DRAINAGE STUDY INFORMATION FORM

Name of Development: The Seventy Date: March 2016

Location of Development a) Descriptive (Cross Streets) North/South: Hualapai Way
East/West: Rampart Boulevard

b) Section: 31, 32 Township: 20S Range: 60E

c) APN: 138-32-301-005, 138-32-301-006, 138-32-210-008, 138-32-202-001, 138-31-702-002 and 138-31-801-002

Name of Owner: Seventy Acres LLC, Fore Stars LTD, and 180 Land Co LLC

Telephone No.: 702-940-6930 Fax No. 702-940-6931 E-Mail Address: Not available

Address: 9775 W. Charleston Blvd., Las Vegas, Nevada 89117

Contact Person-Name: Ryan R. Belsick, PE Telephone No.: (702) 804-2000

* E-Mail Address: rbelsick@gcwengineering.com Fax No.: (702) 804-2299

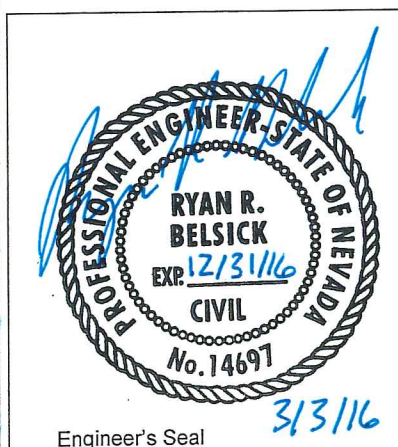
Firm: GCW, Inc

Address: 1555 S. Rainbow Blvd, Las Vegas, NV 89146

Type of Land Development/Land Disturbance

<input type="checkbox"/>	Rezoning	<input type="checkbox"/>	Subdivision Map	<input type="checkbox"/>	Clearing and Grading Only
<input type="checkbox"/>	Parcel Map	<input type="checkbox"/>	Planned Unit Development	<input checked="" type="checkbox"/>	Other (Please specify below)
<input type="checkbox"/>	Large Parcel Map	<input type="checkbox"/>	Building Permit	Conceptual Drainage, Rough Grade and Storm Drain	

- Total Owned Land Area: At Site: +/- 70.52 acres Being Developed/Disturbed: +/- 70.52 acres
- Is a portion or all of the subject property located in a designated FEMA Flood Hazard Area? ☒ Yes** ☐ No
- Is the property bordered or crossed by an existing or proposed Clark County Regional Flood Control District Master Planned Facility? ☒ Yes** ☐ No
- Proposed type of development (Residential, Commercial, Etc.): Conceptual Drainage, Rough Grade and Storm Drain Improvements
- Approximate upstream land area which drains to the subject site: +/- 3.73 sq. mi.
- Has the site drainage been evaluated in the past? ☒ Yes ☐ No If yes, please identify documentation: Peccolle Ranch West Master Study, Queensridge LOMR, Queens Borough Culvert Study
- If known, please briefly identify the proposed discharge point(s) of runoff from the site: Existing dual (2) - 12'x12' RCB at northeast corner of site
- Briefly describe your proposed schedule for the subject project: ASAP



Submit this form as part of the required drainage study to the local entity which has jurisdiction over the subject property. This form may provide sufficient information to serve as the Conceptual Drainage Study.

*New Required Field

**Review and concurrence of the Clark County Regional Flood Control District is required.

Local Entity File No.

Revision

Date

REFERENCE:

STANDARD FORM 1

HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

DRAINAGE SUBMITTAL CHECKLIST

Project Name: The Seventy	Map ID:
Firm Name: GCW, Inc.	Engineer: Ryan R. Belsick
Address: 1555 S Rainbow Blvd	
City: Las Vegas	State: NV Zip: 89146
Phone Number: (702) 804-2000	Fax Number: (702) 804-2299
Property Owner: Seventy Acres LLC, Fore Stars LTD, and 180 Land Co LLC	
Address: 9755 W. Charleston Blvd	
City: Las Vegas	State: NV Zip: 89177
Reviewed By:	Date Received: Date Accepted for Review:

The following checklist is intended as a guide for the engineer preparing a Technical Drainage Study to submit to the local entity and Clark County Regional Flood Control District (if necessary). The listed items are the minimum information required prior to the entity performing a review. The engineer will remain responsible to ensure the Technical Drainage Study is prepared within the guidelines as set forth in the Clark County Regional Flood Control District (CCRFCD) Hydrologic Criteria and Drainage Design Manual (MANUAL).

This document is intended as an aid in preparing Technical Drainage Studies. Each study submitted is reviewed for compliance with local and regional criteria. This form is not intended to be all inclusive and does not limit the extent of the information, calculations or exhibits which may be necessary to properly evaluate the intended land use.

If items are not applicable for the subject site, provide N/A.

I. GENERAL REQUIREMENT

- | Yes | No | |
|-------------------------------------|--------------------------|---|
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Design Manual Standard Form 1 with the engineer's seal and signature. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Design Manual Standard Form 4 . |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | 2 copies of the 24" x 36" Drainage Plan. |
| <input type="checkbox"/> | <input type="checkbox"/> | <u>N/A</u> A notarized letter from the adjacent property owner(s) allowing off-site grading or discharge. |

II. MAPS AND EXHIBITS

- | Yes | No | |
|-------------------------------------|--------------------------|---|
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | A copy of a current Flood Insurance Rate Map (FIRM) with the site delineated. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | A copy of the current CCRFCD Master Plan Update Figure, (F-x), for Flood Control Facilities and Environmental areas with the site delineated. |

REFERENCE:

STANDARD FORM 2

HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

DRAINAGE SUBMITTAL CHECKLIST

II. MAPS AND EXHIBITS (Continued)

Yes No

- ☒ ☐ Off-site drainage basin maps for existing, interim and future conditions showing the existing topography, basin boundaries, concentration points, and flows in cfs.
- ☒ ☐ On-site drainage basin maps for existing and proposed conditions showing the existing topography, basin boundaries, concentration points, and on-site and off-site flows in cfs.
- ☒ ☐ Vicinity Map with local and major cross streets identified and a north arrow.

III. DRAINAGE PLAN

Yes No

- ☒ ☐ Sheet size: 24" x 36" sealed by a registered engineer in the State of Nevada.
- ☒ ☐ Minimum scale: 1" = 60'.
- ☒ ☐ Project name.
- ☒ ☐ Vicinity Map with local and major cross streets.
- ☒ ☐ Revision box.
- ☒ ☐ North arrow and bar scale.
- ☒ ☐ Engineer's/consultant's address and phone number.
- ☒ ☐ Elevation datum and benchmark.
- ☒ ☐ Legend for symbols and abbreviations.
- ☒ ☐ Cut/fill scarps, where applicable.
- ☒ ☐ Street names, grades, widths.
- ☒ ☐ Proposed future and existing spot grades for top of curbs and street crowns at lot lines, grade breaks, and along curb returns on both sides of the street.
- ☒ ☐ Existing contours encompassing the site and 100 feet beyond with spot elevations for important locations, where appropriate.
- ☐ N/A Minimum finish floor elevations with top-of-curb elevations at upstream end of lot.
- ☐ N/A Proposed typical street sections.

REFERENCE:

STANDARD FORM 2

HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

DRAINAGE SUBMITTAL CHECKLIST

III. DRAINAGE PLAN (Continued)

Yes No

- | | | |
|-------------------------------------|--------------------------|---|
| <input type="checkbox"/> | <u>N/A</u> | Streets with off-set crowns. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Proposed contours or spot elevations in sufficient detail to exhibit intended drainage patterns and slopes. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Property lines. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Right-of-way lines and widths, existing and proposed. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Existing improvements and their elevations. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Delineation of proposed on-site drainage basins indicating area and 10-year and 100-year storm peak flows at basin concentration points. |
| <input type="checkbox"/> | <u>N/A</u> | Concentration points and drainage flow direction with Q100 and V100 and D100 in streets. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Cumulative flows, velocity, and direction of flow at upstream and downstream ends of site for the 10-year and 100-year flows. |
| <input type="checkbox"/> | <u>N/A</u> | Location and cross-section of street capacity calculations. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Cross-sectional detail for channels, including cutoff wall locations. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Existing and proposed drainage facilities, appurtenances, and connections (i.e., sidewalk, ditches, swales, storm drain systems, unimproved and improved channels, and culverts, etc.) stating size, material, shape, and slope with plan and profile and HGL calculations. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Existing and proposed drainage easements and widths shown with sufficient detail. A cross sectional detail must be provided that shows appropriate lining and reinforcement. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Location and detail of existing, proposed, and future block wall openings. Minimum size is 16" x 48". Wrought iron gate is required for flows > 10 cfs. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Location and detail of flood walls illustrating depth of flow, proposed grouting height, etc. |
| <input type="checkbox"/> | <u>N/A</u> | Perimeter retaining wall locations. All existing and proposed walls (retaining screen and flood) must be shown with adjacent ground elevations. Flood walls with 8-inch concrete masonry unit. |
| <input type="checkbox"/> | <u>N/A</u> | Building and/or lot numbers. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Alignment of all existing, proposed, or future Regional Facilities adjacent to the site. |
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | Limits of existing floodplain based on current FIRM or best available information; limits of proposed floodplains based on best available information. |

REFERENCE:

STANDARD FORM 2

HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

DRAINAGE SUBMITTAL CHECKLIST

III. DRAINAGE PLAN (Continued)

Yes No

- ☒ ☐ For areas in Zone A, AE, AH, and AO, base flood elevations (BFEs) must be shown for each lot; BFEs may be listed on each lot, or in a table. Finish floor elevations must be a minimum of 18 inches above BFE.
- ☐ N/A Appropriately elevated "humps" 6 inches above the 100 year water surface elevation at site accesses where the intent is to protect the site from the Q100 flows.
- ☐ N/A Street slopes for perimeter and interior streets. The minimum slope is 0.4 percent.
- ☐ N/A Location and detail of best management practice (BMP) for parking lots and low impact development (LID) (if required).

IV. HYDROLOGIC ANALYSIS

Yes No

- ☒ ☐ Appropriate soil information and Soils Map for existing and future conditions with subbasins and property delineated.
- ☒ ☐ Input and output information for existing conditions from computer models (HEC-1 or TR-55). The flow routing diagram must be provided with HEC-1 models.
- ☒ ☐ Input and output information for future conditions from computer models (HEC-1 or TR-55). The flow routing diagram must be provided with HEC-1 models.
- ☒ ☐ Use of correct precipitation values in and around the McCarran Airport rainfall area.
- ☒ ☐ A discussion in the text of the hydrologic analysis justifying subbasin boundaries and cutoffs, supporting assumptions, and calculations.
- ☒ ☐ A summary table of stormwater flows showing basin area, Q10 and Q100 for both individual basins and combined basin flows, where applicable.
- ☒ ☐ Copies of supporting technical information referenced from a previously approved study and a statement accepting these results.
- ☒ ☐ On-site facilities must perpetuate flows through or around the site without significantly impacting adjacent property owners in accordance with current Nevada Drainage Law.
- ☐ N/A Calculation for impervious area for parking lots and LIDs (if required).

REFERENCE:

STANDARD FORM 2

HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

DRAINAGE SUBMITTAL CHECKLIST

V. HYDRAULIC ANALYSIS

Yes No

- | | | |
|----------------|------------|---|
| _____ | <u>N/A</u> | Flow split calculations and supporting documentation or reference for the method of flow split calculations used. |
| _____ | <u>N/A</u> | Normal depth street flow calculations and cross section diagrams for all interior and perimeter streets. Provide "d x v" products for the Q100 and Q10 flows representing the worst case for interior and all perimeter streets. Q100 d x v < 8. Q10 d x v < 6 and 12 foot dry lane for rights-of-way > 80 feet. Calculations must be labeled by street name as indicated on the Grading Plan. |
| _____ | <u>N/A</u> | A summary table of interior and exterior street capacity calculations showing the street name, Q100 flow, slope, depth of flow, velocity and depth times velocity product and streets needing to meet 12 foot dry lane criteria. |
| _____ | <u>N/A</u> | Appropriate hydraulic calculations for block wall openings assuming a 50 percent vertical clogging factor. (Assume the lower half of the opening is plugged.) |
| <u>X</u> _____ | _____ | Appropriate hydraulic calculations at drainage easement entrance and discharge locations to set finish floor elevations. Hydraulic calculations must include submerged weir, superelevation and tee intersection losses, where appropriate. |
| <u>X</u> _____ | _____ | Provide necessary freeboard requirements to set the finished floor elevations of all proposed buildings, 2 x depth of flow or depth of flow plus 18 inches of freeboard, whichever is less. The minimum requirement is 6 inches above adjacent upstream top of curb. Buildings adjacent to drainage easements must always be provided with 18 inches of freeboard above the Q100 weir height or flow depth, whichever is greater. |
| <u>X</u> _____ | _____ | A complete water surface profile analysis (HEC-2, HEC-RAS, etc.) for channel flows and FEMA Zone A flood zones. <ul style="list-style-type: none"> • Field survey data. • Input and output information. • Plotted cross-sections based on survey with proper encroachments. • A map showing the location of the cross-sections. • Analysis of both sub and super-critical flow segments. • A summary table and a discussion of the results in the text of the report. |
| <u>X</u> _____ | _____ | Provide a 50 percent clogging factor in the capacity calculation for drop inlets. |
| <u>X</u> _____ | _____ | Hydraulic calculations for culverts and storm drains. D-Load calculations must be provided for storm drain pipes in public rights-of-way, including headwater pool inundation. |
| <u>X</u> _____ | _____ | The mitigation of nuisance water, both during construction and in the fully developed condition, must be addressed. |
| _____ | <u>N/A</u> | Provide BMP type, size and supporting calculations for parking lots and LIDs (if required). |

REFERENCE:

STANDARD FORM 2



CITY OF LAS VEGAS

MINIMUM DRAINAGE STUDY CRITERIA STANDARD FORM 2 CHECKLIST SUPPLEMENT

(Revised 5/18/11)

The following checklist is intended as a supplemental guide for the engineer preparing a Technical Drainage Study submittal to the City of Las Vegas. This supplement focuses on requirements specific to the City of Las Vegas. The requirements presented are in addition to the Clark County Regional Flood Control District (CCRFCD) Manual Standard Form 2. The listed items are the minimum information required prior to the City performing a review. The engineer will remain responsible to ensure the Technical Drainage Study is prepared within the guidelines as set forth in the CCRFCD Hydrologic Criteria and Drainage Design Manual (Design Manual).

An appointment must be made to preview this checklist in conjunction with CCRFCD Standard Form 2 prior to the City accepting a new drainage study for review. The engineer must contact the Flood Control Section at (702) 229-6541 to schedule a submittal appointment.

If items are not applicable for the subject site, provide N/A.

I. GENERAL REQUIREMENT		
Yes	No	
	N/A	A notarized letter from the adjacent property owner(s) allowing off-site grading. (A copy of the letter must be received prior to final acceptance of the drainage study.)
X		Copies of all conditions of approval for development related to this property. (e.g. zoning, use permit, tentative map, etc.) Verify compliance with conditions.
X		An electronic copy of the complete submittal is required to be submitted with one original hard copy of the study. Electronic documents should be on a universal computer-readable digital output device replicating your submittal. An Indexed Portable Document Format (PDF) or Print Ready CAD file formats with a minimum of 300dpi are the desired formats. If figures are in color, they must be scanned in color and saved as a separate file. <u>RLA</u> by initial here, the engineer on record acknowledges that the electronic copy is an identical replicate of the original hard copy submitted to the City of Las Vegas.

II. GRADING PLAN INFORMATION		
Yes	No	
X		(1) 24" X 36" copy of the Grading Plan, (including all Detail Sheets) sealed by the engineer.
X		Proposed future and existing spot grades for top of curbs and street crowns at lot lines, grade breaks, and along curb returns on both sides of the street. Note: Proposed top of curb elevations must be provided for both sides of roadways even if only half street construction is required.
X		Label existing topography at a minimum 5 foot elevation interval including adjacent developments, finished floor elevations of existing buildings and top of existing curbs extending 100 feet around the perimeter of the site. (*Measured from the centerline of the adjacent roadway.)

Flood Control Section • 333 N. Rancho Drive • Las Vegas, NV 89106
Ph. (702) 229-6541 • Fax (702) 382-8551
www.lasvegasnevada.gov

CITY OF LAS VEGAS MINIMUM DRAINAGE STUDY CRITERIA CHECKLIST

II. GRADING PLAN INFORMATION		
Yes	No	
X		Proposed on-site and off-site storm drains and other flood control facilities with plan and profile sheets for public storm drains showing the class of pipe, (Class III, IV, V, etc.), design hydraulic grade line, (HGL) and 100 year storm flow. A public drainage easement must be provided over on-site storm drains conveying off-site flows. An overflow path must be provided over all storm drains.
X		All existing and "to be constructed" walls with cross-sections showing wall type, (e.g. block wall, retaining wall, flood wall, etc.), with limits clearly defined, adjacent ground elevations. Wall heights must meet current ordinances and in no case exceed 14 feet above the adjacent property.
	N/A	Street slopes for both interior and perimeter streets. Note: The minimum slope for a roadway is 0.4 percent, a minimum 18-inch storm drain must be provided where minimum slopes cannot be met.
	N/A	Back of lot elevations and lot drainage pattern for all lots including common lots.
X		Sites with a grade difference two feet above or below existing ground are required to have approval from City of Las Vegas Current Planning. Current Planning approval is required prior to final approval of the drainage study.
X		On-site facilities must perpetuate flows through or around the site without significantly impacting adjacent property owners. (The project must pass flows through the site every 600 feet where the project is blocking flow paths.)
	N/A	This project uses a solid grouted stem wall (or approved alternate) at the back of sidewalk to provide erosion protection for landscaped areas where the depth of flow in the roadway exceeds the back of walk elevation. A corresponding cross-section detail is included.
	N/A	Commercial and Common Lot Landscape areas are not allowed to drain over the sidewalk. The grading plans show flow lines with grades and sidewalk under drains for all landscape areas draining to the public ROW.

III. Local Entity Criteria - City of Las Vegas – Manual Section 1600

Yes	No	
	N/A	Concrete valley gutters are required in parking lots with slopes less than 1 percent. Slopes through cul-de-sac must be at a 1 percent minimum where flow is drained through the cul-de-sac.
X		Ten-foot wide public drainage easements to be privately maintained are allowed for flow less than 20 cfs. The depth of flow entering the easement must be checked using the submerged weir calculation.
X		The limits of the flood zones and the base flood elevations (BFE) must be shown on all grading plans for all developments within a Special Flood Hazard Zone A, AO, AE, etc.
X		Minimum finish floor elevation is 6 inches above highest adjacent top of curb. Finish floor calculations must include allowances for super elevations on curves and velocity head for tee intersections.
X		Finished floor elevations for buildings adjacent to public drainage easements must be a minimum of 18 inches above the Q100 weir of submerged weir elevation, whichever is greater.

CITY OF LAS VEGAS MINIMUM DRAINAGE STUDY CRITERIA CHECKLIST

III. Local Entity Criteria - City of Las Vegas – Manual Section 1600		
Yes	No	
	N/A	Lots with "B and C Type Drainage" that drain from one lot to another through a drainage easement shall be required to install an underground nuisance drainage system or a 2-foot valley gutter. 16" x 24" minimum block wall openings are required for both options.
	N/A	Bubblers are required across 80 foot and greater ROW streets. When flows exceed 10 cfs, bubblers larger than 18 inches will be required up to a maximum of 36". Inlets must be sized to match the pipe size provided.

- Contact the Flood Control Section regarding the drainage study review fee. These fees are payable at the time of submittal.
- The Drainage Study must be conditionally approved prior to submitting improvement plans to the Civil and Planning Development of the Department of Building and Safety for review.

This document is intended as an aid in preparing Technical Drainage Studies for the City of Las Vegas. Each study submitted is reviewed for compliance with local and regional criteria. This form is not intended to be all-inclusive and does not limit the extent of the information, calculations or exhibits which may be necessary to properly evaluate the intended land use.

**TECHNICAL DRAINAGE STUDY
FOR
THE SEVENTY**

840-050

March 2016

Prepared For:

**Seventy Acres LLC, Fore Stars LTD, and 180 Land Co LLC
9775 West Charleston Boulevard
Las Vegas, NV 89117
Phone: (702) 940-6930
Fax: (702) 940-6931**

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I. INTRODUCTION

Seventy Acres LLC, Fore Stars LTD, and 180 Land Co LLC are proposing to construct The Two Fifty, a multi-family residential and single-family residential development consisting of luxury multi-family and estate lots upon the land currently operated as the Badlands golf course located south of Alta Drive, north of Charleston Road, east of Hualapai Way and west of Rampart Boulevard, in Las Vegas, Nevada. A land use exhibit provided in Appendix A shows the proposed site layout. The project improvements include: 3,020 luxury multi-family units and minimum 1 acre to 5 acre estate lots on the 253 acres of APNs 138-32-301-005 (17.49 acres), 138-32-301-006 (53.03 acres), 138-32-210-008 (2.37 acres), 138-32-202-001 (2.13 acres) 138-31-702-002 (166.99 acres) and 138-31-801-002 (11.28 acres). Onsite storm drain facilities are proposed to convey the offsite flows from the existing storm drain facilities in Hualapai Way and Charleston Boulevard to the existing dual (2) - 12-foot wide by 12-foot high reinforced concrete box culverts (RCBC) in Rampart Boulevard at the Rampart Boulevard and Alta Drive intersection. The Two Fifty development will be constructed in three phases. The 1st phase of development consists of mass grading and storm drain improvements for approximately 70 acres of APNs 138-32-301-005, 138-32-301-006, 138-32-210-008, and 138-32-202-001 (hereafter referred to as The Seventy). The 2nd phase of development includes construction of the luxury multi-family units within The Seventy. The 3rd phase of development includes construction of the estate lots within approximately 180 acres of APNs 138-31-702-002 and 138-31-801-002 (hereafter referred to as The One Eighty). The purpose of this report is to provide a conceptual drainage analysis for The Two Fifty and serve as a technical drainage study for The Seventy to determine the impacts to downstream developments and facilities to establish allowable flow rates and drainage patterns for interior development, and to recommend storm drain facilities to convey storm flow through the project site. This study also addresses the 1st phase of development which includes The Seventy mass grading and onsite storm drain improvements. The 2nd phase of development will be addressed in a future technical drainage study updates and the 3rd phase of development will be addressed in a future technical drainage study for The One Eighty. The following tasks were performed in the preparation of this report:

- ♦ Identify and review previous drainage studies for the project site and areas adjacent to the project.
- ♦ Identify the existing FEMA floodplain designation for the project site.
- ♦ Determine recommended proposed FEMA floodplain designations within the project limits.

- ◆ Identify existing and proposed regional drainage facilities within and adjacent to the project site.
- ◆ Identify existing drainage areas and storm drain facilities that affect the site.
- ◆ Perform field investigation.
- ◆ Estimate peak runoff impacting the proposed grading and storm drain improvements during the 10-year and 100-year return period storms for existing and proposed conditions.
- ◆ Recommend conceptual drainage facilities for The One Eighty to protect the proposed project and downstream properties from storm runoff.
- ◆ Prepare hydraulic analyses for The Seventy storm drain and proposed channel improvements.
- ◆ Recommend drainage facilities to protect the proposed project from storm runoff.

GCW has obtained and reviewed technical drainage studies and grading plans from the City of Las Vegas (CLV) for the site and offsite properties adjacent to the site to determine existing conditions offsite and onsite drainage patterns and discharge flows into the site. The studies reviewed include:

1. *Technical Drainage Study for Peccole Ranch Golf Course (Phase II)* (DS 1347)
2. *Technical Drainage Study for Peccole West Commercial Center* (DS 2364)
3. *Technical Drainage Study for Rampart Boulevard* (DS 2696)
4. *Technical Drainage Study Update for Peccole Ranch Golf Course Maintenance Yard* (DS 1626)
5. *Hydrology Study Update for Queensridge Fairway Homes* (DS 2307)
6. *Technical Drainage Study Peccole West Lot 9 (Phase II)* (DS 1630)
7. *Technical Drainage Study for Peccole West Lot 12* (DS 1650)
8. *Technical Drainage Study for Village 12 Hualapai Way Improvements* (DS 1853)
9. *Technical Drainage Study for Hualapai Way Rough Grading, Alta Drive to Charleston Boulevard* (DS 1758)
10. *Technical Drainage Study for Peccole West Lot 11* (DS 1753)
11. *Technical Drainage Study for Peccole Ranch Parcel 19 & 20* (DS 2172)
12. *Technical Drainage Study for San Michelle West* (DS 2226)
13. *Technical Drainage Study for Peccole – Lot 10 Parcel 18* (DS 2203)
14. *Technical Drainage Study for Windsor at Queensridge* (DS 3279)

15. *Technical Drainage Study for Club House (DS 1555)*
16. *Technical Drainage Study for the Versailles (DS 2236)*
17. *Master Drainage Study for Peccole Ranch – Phase II (DS 1140)*
18. *Technical Drainage Study for Badlands Hole 9 (DS 1974)*
19. *Technical Drainage Study for Peccole West Business Center (DS 1856)*
20. *Technical Drainage Study for Peccole West Lot 12 (Park Area) (DS 1929)*
21. *Technical Drainage Study for One Queensridge Place (Condo Towers) – Update 2 (DS 3746)*
22. *Technical Drainage Study for Apple Drive at Peccole Ranch (DS 1576)*
23. *Technical Drainage Study for Alta Drive at Peccole Ranch (DS 1588)*
24. *Technical Drainage Study for Peccole Ranch Phase II Master Plan (DS 273)*
25. *Conceptual Drainage Study for Peccole Ranch Phase II Master Plan (DS 1273)*

An exhibit showing the name and general location of the adjacent developed areas and referenced studies listed above has been included in Appendix A. In order to identify offsite drainage patterns impacting the proposed site, a field visit was performed to confirm overall existing conditions drainage patterns for the site and offsite adjacent parcels.

Hydraulic information from the following study has been referenced for the purposes of this report:

The Technical Drainage Study for Queens Borough Culvert (Reference 1, hereinafter referred to as the Queens Borough Culvert Study) was approved by the CLV on August 30, 2005. The Queens Borough Culvert Study designed the existing approximately 2,000 linear foot dual (2) - 12-foot wide by 12-foot high RCB storm drain system (CCRFGD Facility APSO 0000) downstream of the existing dual (2) - 12-foot wide by 12-foot-high RCB at the Rampart Boulevard and Alta Drive intersection. Proposed flows discharged from the site will be conveyed by the Queens Borough Culvert Study storm drain north to the Angel Park Detention Basin (CCRFGD Facility APNO 0001). Pertinent referenced material from the Queens Borough Culvert Study has been included in Appendix C. Updates to the Queens Borough Culvert Study included the following:

- *Update to the Technical Drainage Study for Queens Borough Culvert (Reference 2) – Approved by CLV on December 30, 2005.*

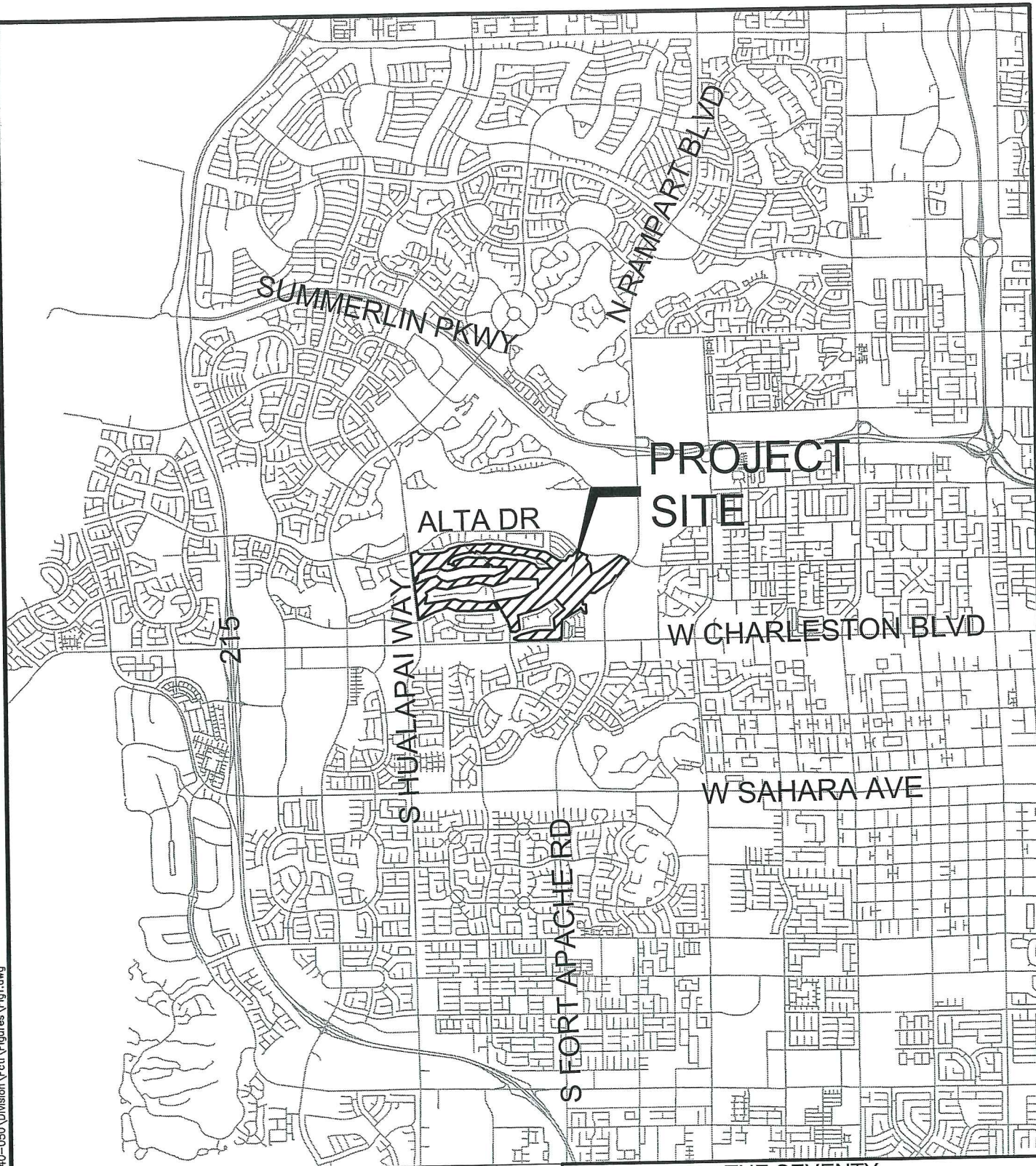
- *Update #2 to the Technical Drainage Study for Queens Borough Culvert (Reference 3, hereinafter referred to as the Queens Borough Culvert Study Update #2 Study) – Approved by CLV on April 21, 2006.*

II. LOCATION AND DESCRIPTION

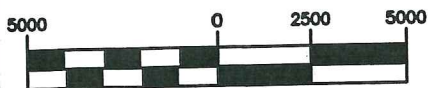
The Seventy is located on approximately 70 acres in Sections 31 and 32, Township 20 South, Range 60 East, M.D.M., in the City of Las Vegas, Nevada. Please refer to Figures 1 and 2 for the vicinity and location of the project site. The site is presently developed as a golf course with existing washes traversing the project site conveying flows from west to east. Offsite flows are conveyed to the site from the west and south through existing reinforced concrete box culverts under Hualapai Way and Charleston Boulevard. Offsite flows from residential subdivisions and commercial development adjacent to the golf course are discharged to the existing golf course as surface flow through existing storm drain and/or drainage easements. The full street improvements are in place for Alta Drive, Charleston Road, Hualapai Way and Rampart Boulevard. For this study, the proposed improvements include mass grading and onsite storm drain facilities. Grading and development of the future onsite development will include multi-family and associated open space and parking area development and will be addressed in a future technical drainage study updates.

III. FEDERAL EMERGENCY MANAGEMENT AGENCY (FEMA) FLOOD HAZARD ANALYSIS

Based on the Flood Insurance Rate Map (FIRM) Community Panel 32003C 2145 F dated November 16, 2011, and FIRM Panel 32003 C 2150 E dated September 27, 2002, and revised to reflect the Letter of Map Revision (LOMR) Case No. 06-09-B483P dated September 21, 2006, and LOMR Case No. 06-09-B486P dated October 19, 2006, the project site is crossed by a FEMA-designated Special Flood Hazard Area (SFHA). The proposed improvements will construct closed conduit facilities that will contain and convey the 100-year flow (1% annual chance flood discharge) through The Seventy. Figure 3 shows the site denoted on a portion of the aforementioned FIRM panels. A Conditional Letter of Map Revision (CLOMR) will be obtained from FEMA prior to construction of this project. A LOMR will be obtained from FEMA once construction of the onsite RCB storm drain system is substantially completed and functional.

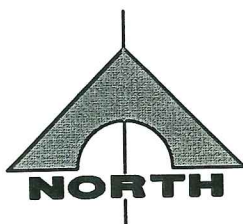


GRAPHIC SCALE



(IN FEET)

1 inch = 5000 ft.



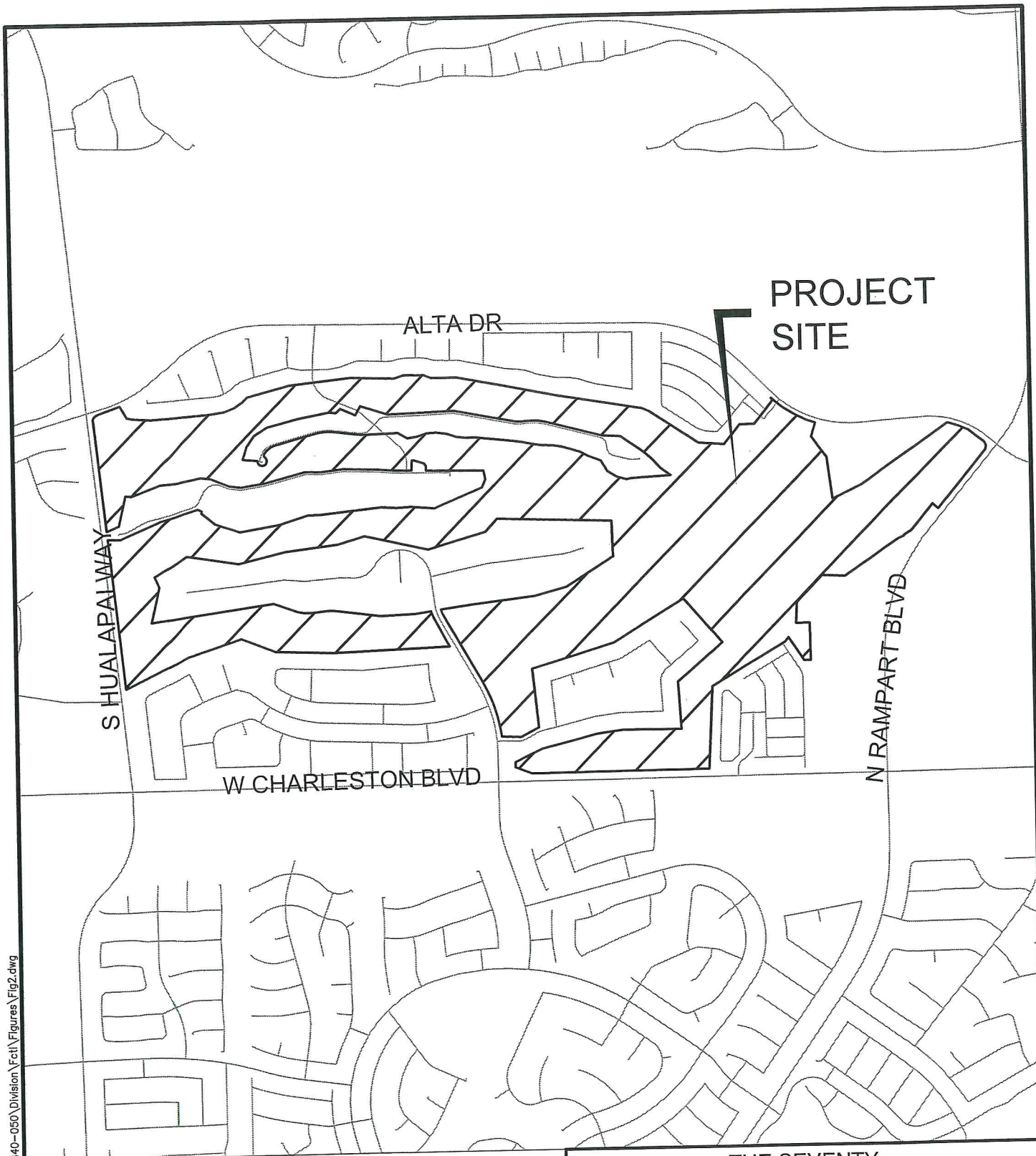
THE SEVENTY
SEVENTY ACRES LLC, FORE STARS
LTD, AND 180 LAND CO LLC

FIGURE 1

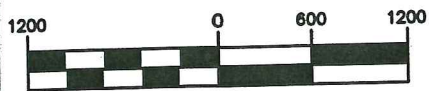
VICINITY MAP

GCV
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gcwengineering.com



GRAPHIC SCALE



(IN FEET)

1 inch = 1200 ft.



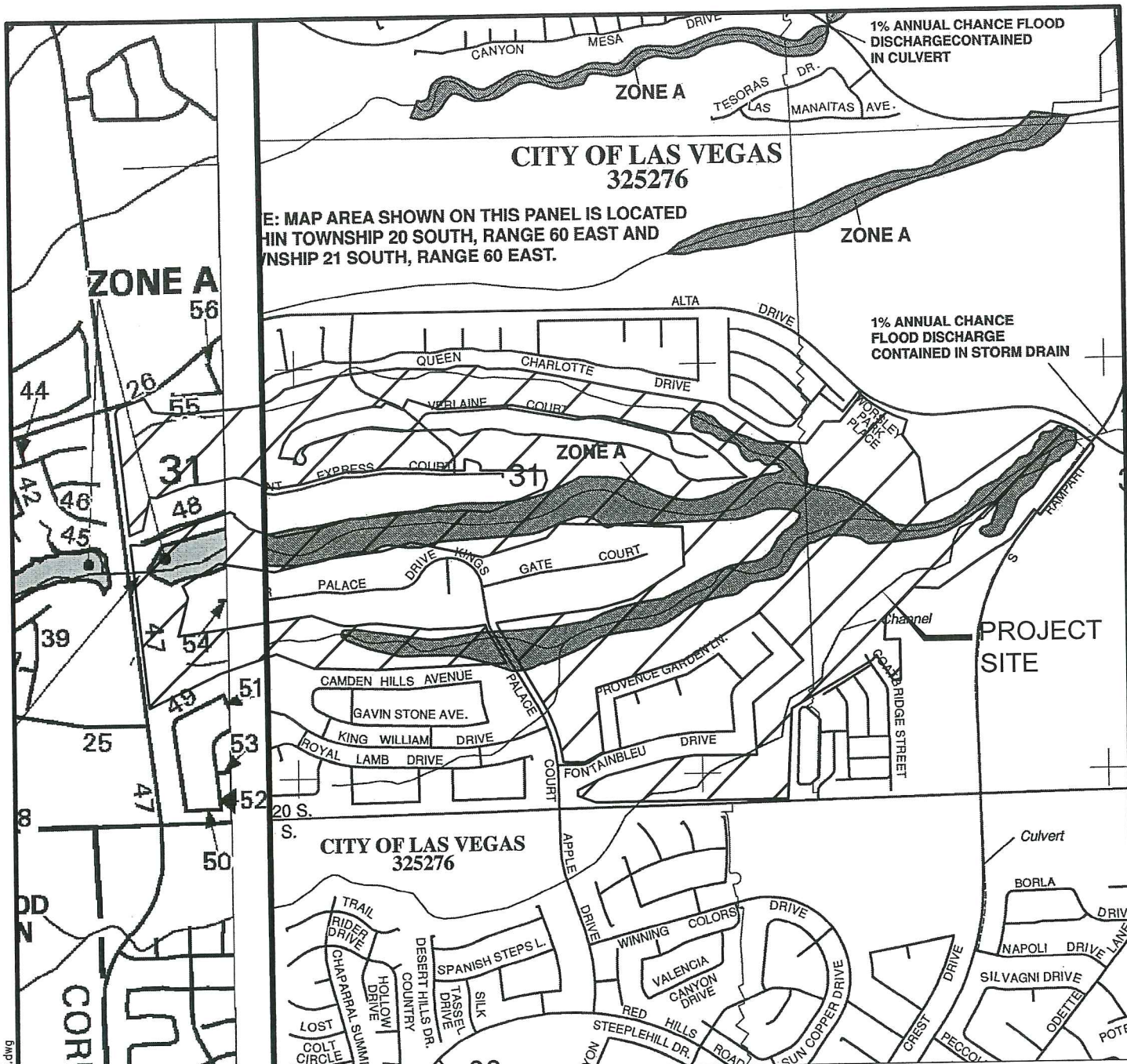
THE SEVENTY
SEVENTY ACRES LLC, FORE STARS
LTD, AND 180 LAND CO LLC

FIGURE 2

LOCATION MAP

GCV
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03-03-16 09:49:48 F:\Projects\800\840-050\Division\Fet\Figures\Fig3.dwg nbagg

NATIONAL FLOOD INSURANCE PROGRAM

PANEL 2145F

FIRM
FLOOD INSURANCE RATE MAP
CLARK COUNTY,
NEVADA
AND INCORPORATED AREAS

PANEL 2145 OF 4090
(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:	NUMBER	PANEL	SUFFIX
COMMUNITY	32032	2145	F
CLARK COUNTY	32032	2145	F
LAS VEGAS, CITY OF	32032	2145	F

Notice to User: The Map Number shown below should be used when placing map orders; the Community Number shown above should be used on insurance applications for the subject community.

MAP NUMBER
32003C2145F

MAP REVISED
NOVEMBER 16, 2011

Federal Emergency Management Agency

PANEL 2150 E

FIRM
FLOOD INSURANCE RATE MAP
CLARK COUNTY,
NEVADA AND
INCORPORATED AREAS

PANEL 2150 OF 4090
(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:	NUMBER	PANEL	SUFFIX
COMMUNITY	32032	2150	E
LAS VEGAS, CITY OF	32032	2150	E
CLARK COUNTY	32032	2150	E
UNINCORPORATED AREAS	32032	2150	E

Notice to User: The Map Number shown below should be used when placing map orders; the Community Number shown above should be used on insurance applications for the subject community.

MAP NUMBER
32003C2150 E

MAP REVISED:
SEPTEMBER 27, 2002

Federal Emergency Management Agency

GRAPHIC SCALE

1200 0 600 1200

(IN FEET)
1 inch = 1200 ft.

NORTH

**THE SEVENTY
SEVENTY ACRES LLC, FORE STARS
LTD, AND 180 LAND CO LLC**

FIGURE 3
F.I.R.M.

GCV
ENGINEERS & SURVEYORS

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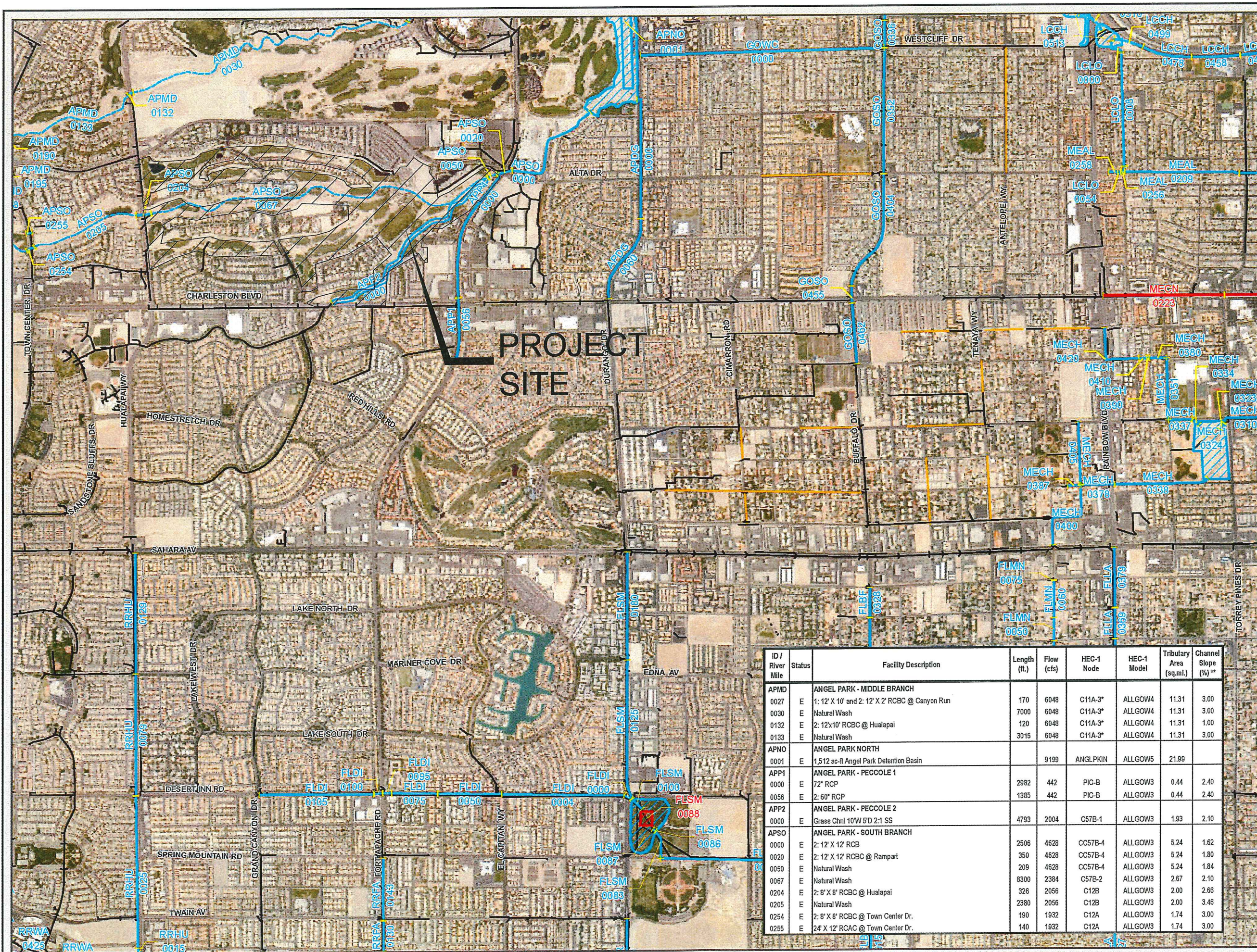
IV. CLARK COUNTY REGIONAL FLOOD CONTROL DISTRICT (CCRFCD) FACILITIES

Figure 4 is reproduced from Figures F-12 from the *2013 Las Vegas Valley Flood Control Master Plan Update* (Reference 4, hereinafter referred to as the 2013 MPU). The figure depicts the project site in relation to existing and proposed regional facilities. As shown on Figure 4, the following facilities are within or adjacent to the project site:

- ♦ Angel Park – South Branch (APSO 0000-0204)
- ♦ Angel Park – Peccole 1 (APP1 0000)
- ♦ Angel Park – Peccole 2 (APP2 0000)

The Two Fifty project site contains existing CCRFCD Facilities APSO 0050, APSO 0067, and APP2 0000. The existing CCRFCD Facilities within The Two Fifty project site are labeled as natural washes in the 2013 MPU. The One Eighty proposes approximately 4,700 linear feet of CCRFCD Facility APSO 0067 and approximately 2,300 linear feet of CCRFCD Facility APP2 0000 as future RCB storm drain. The Seventy proposes to construct CCRFCD Facility APSO 0050 and approximately 1,900 linear feet of CCRFCD Facility APSO 0067 and approximately 1,485 linear feet of CCRFCD Facility APP2 0000 as RCB storm drain.

The 2013 MPU flow rates for the proposed CCRFCD Facilities will be superseded by the project specific hydrology presented in this report. Flows conveyed through the site are discharged northeast to existing CCRFCD Facility APSO 0020 located at the Rampart Boulevard and Alta Drive intersection. CCRFCD Facility APSO 0020 is labeled as a dual (2) - 12-foot wide by 12-foot high RCB in the 2013 MPU. CCRFCD Facility APSO 0020 discharges flow east to existing CCRFCD Facility APSO 0000. CCRFCD Facility APSO 0000 is labeled as a dual (2) - 12-foot wide by 12-foot high RCB in the 2013 MPU. CCRFCD Facility APSO 0000 conveys flow northeast to the existing Angel Park Detention Basin. The hydraulic design for CCRFCD Facility APSO 0000 was presented in the Queens Borough Culvert Study. The Angel Park Detention Basin is labeled as CCRFCD Facility APNO 0001.



2013
LAS VEGAS VALLEY
FLOOD CONTROL
MASTER PLAN UPDATE

FIGURE F- 30
FLOOD CONTROL FACILITIES

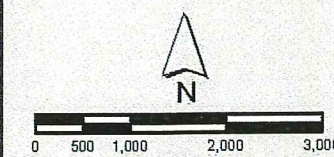
LEGEND

- Ultimate Development Boundary
- Existing Facilities
- Category A Proposed Facilities
- Category B Proposed Facilities
- Local Existing Facilities
- Local Proposed Facilities
- Detention Basin

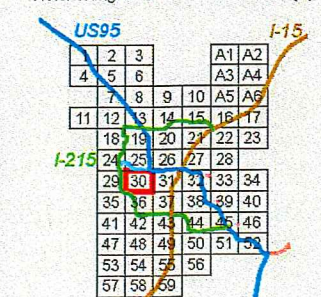
- Stormdrain
- Lined Channel
- Unlined Channel
- Levee/Dike
- Natural Wash/Floodway
- ID-Mile Separator

- Remove & Replace/Parallel Facilities**
- | Category A | Category B |
|------------|------------|
| Channel | Channel |
| Stormdrain | Stormdrain |

FIGURE 4



Scale: 1 inch = 2,000 feet
Refer to Figure G-2 for Aerial Source(s)



ID / River Mile	Status	Facility Description	Length (ft.)	Flow (cfs)	HEC-1 Node	HEC-1 Model	Tributary Area (sq.mi.)	Channel Slope (%) **
APMD 0027	E	ANGEL PARK - MIDDLE BRANCH	170	6048	C11A-3*	ALLGOW4	11.31	3.00
0030	E	1: 12' X 10' and 2: 12' X 2' RCBC @ Canyon Run	7000	6048	C11A-3*	ALLGOW4	11.31	3.00
0132	E	Natural Wash	120	6048	C11A-3*	ALLGOW4	11.31	1.00
0133	E	2: 12x10' RCBC @ Hualapai	3015	6048	C11A-3*	ALLGOW4	11.31	3.00
0133	E	Natural Wash	3015	6048	C11A-3*	ALLGOW4	11.31	3.00
APNO 0001	E	ANGEL PARK NORTH						
0001	E	1,512 ac-ft Angel Park Detention Basin		9199	ANGLPKIN	ALLGOW5	21.99	
APP1 0000	E	ANGEL PARK - PECCOLE 1						
0000	E	72" RCP	2982	442	PIC-B	ALLGOW3	0.44	2.40
0056	E	2: 60" RCP	1385	442	PIC-B	ALLGOW3	0.44	2.40
APP2 0000	E	ANGEL PARK - PECCOLE 2						
0000	E	Grass Chnl 10'W 5'D 2:1 SS	4793	2004	C57B-1	ALLGOW3	1.93	2.10
APSO 0000	E	ANGEL PARK - SOUTH BRANCH						
0000	E	2: 12' X 12' RCB	2506	4628	CC57B-4	ALLGOW3	5.24	1.62
0020	E	2: 12' X 12' RCBC @ Rampart	350	4628	CC57B-4	ALLGOW3	5.24	1.80
0050	E	Natural Wash	209	4628	CC57B-4	ALLGOW3	5.24	1.84
0067	E	Natural Wash	8300	2384	C57B-2	ALLGOW3	2.67	2.10
0204	E	2: 8' X 8' RCBC @ Hualapai	326	2056	C12B	ALLGOW3	2.00	2.66
0205	E	Natural Wash	2380	2056	C12B	ALLGOW3	2.00	3.46
0254	E	2: 8' X 8' RCBC @ Town Center Dr.	190	1932	C12A	ALLGOW3	1.74	3.00
0255	E	24' X 12' RCAC @ Town Center Dr.	140	1932	C12A	ALLGOW3	1.74	3.00

V. HYDROLOGY

The methodology presented in this study is in compliance with the *CCRFCD Hydrologic Criteria and Drainage Design Manual* (Reference 5, hereinafter referred to as the Manual).

Model Description - The drainage subbasins were modeled using the SCS Unit Hydrograph method within the U.S. Army Corps of Engineers *HEC-1 Flood Hydrograph Package* (Reference 6). Since the drainage area for each watershed within the project is less than 8 square miles, an SDN 3 design storm was selected for use in the HEC-1 computer model. The 2013 MPU ALLGOW3.dat HEC-1 model has been referenced and revised for the purposes of this report.

Precipitation – The project site and tributary drainage areas lie outside of the McCarran Rainfall Area as identified in the Manual. Rainfall depths for the project site were calculated utilizing GIS data distributed by the Clark County GISMO (Geographic Information Systems Management Office). The GIS rainfall depths were extracted from the NOAA Rainfall Atlas and have been adjusted according to the approach outlined in Section 500 of the Manual. The adjusted point precipitation values for the onsite drainage subbasins range from 2.88 inches to 3.08 inches for the 100-year storm event and 1.64 inches to 1.76 inches for the 10-year storm events. The rainfall exhibit has been included in Appendix A.

Curve Numbers (CN) – The soils information for the project watershed was referenced from the *Soil Survey of Las Vegas Valley Area, Nevada, Part of Clark County* (Reference 7). This survey delineates families of soil types and the Hydrologic Soil Group (HSG) of each family. A soils map containing the project site is included in Appendix A. The soil classification for the site has been revised since the 2013 MPU was prepared and the soil classification used for the onsite portion of the model has been revised accordingly. A copy of the *Custom Soil Resource Report for the Soil Survey of the Las Vegas Valley Area, Nevada, Part of Clark County* from the U.S. Department of Agriculture and Natural Resource Conservation Service (Reference 7) have been included in Appendix A. The report shows that the project area and offsite subbasins consist of Soil Type 152 (Cave). Soil Type 152 is classified as 100 percent Hydrologic Soil Group (HSG) Type “D”. Note that the 2013 MPU hydrology shows Soil Type 152 classified as 5 percent HSG Type “A”, 10 percent HSG Type “B”, and 85 percent HSG Type “D”. As a result of the revisions, CNs for the offsite and onsite

existing conditions subbasins are slightly higher than the CNs presented in the 2013 MPU.

The land uses or land covers used for the subbasins shown for the adjacent parcels and The One Eighty portions of the site are referenced from the 2013 MPU. Due to the size of the future estate lots (minimum 1 to 5± acres), curve numbers for the future The One Eighty subbasins will be less than or equal to the curve numbers presented in this report for existing and proposed conditions.

The land uses or land covers used for the developed The Seventy portion of the site consist of "commercial and business." Weighted curve numbers for the subbasins were calculated using GIS. The land covers used for the mass graded portion of the site in the proposed conditions model conservatively assumes "commercial and business" in lieu of "newly graded areas" since the difference in the calculated curve numbers are comparable (commercial CN 95 vs. newly graded CN 94).

Curve numbers for existing and developed conditions basins, as well as a curve number matrix of the soil type and for each land use, are included in Appendix A.

For the given soils, CN values were determined from appropriate columns of Table 602 and 602A of the Manual. Composite CN values of 82 to 95 were determined for the existing and developed conditions onsite subbasins, respectively.

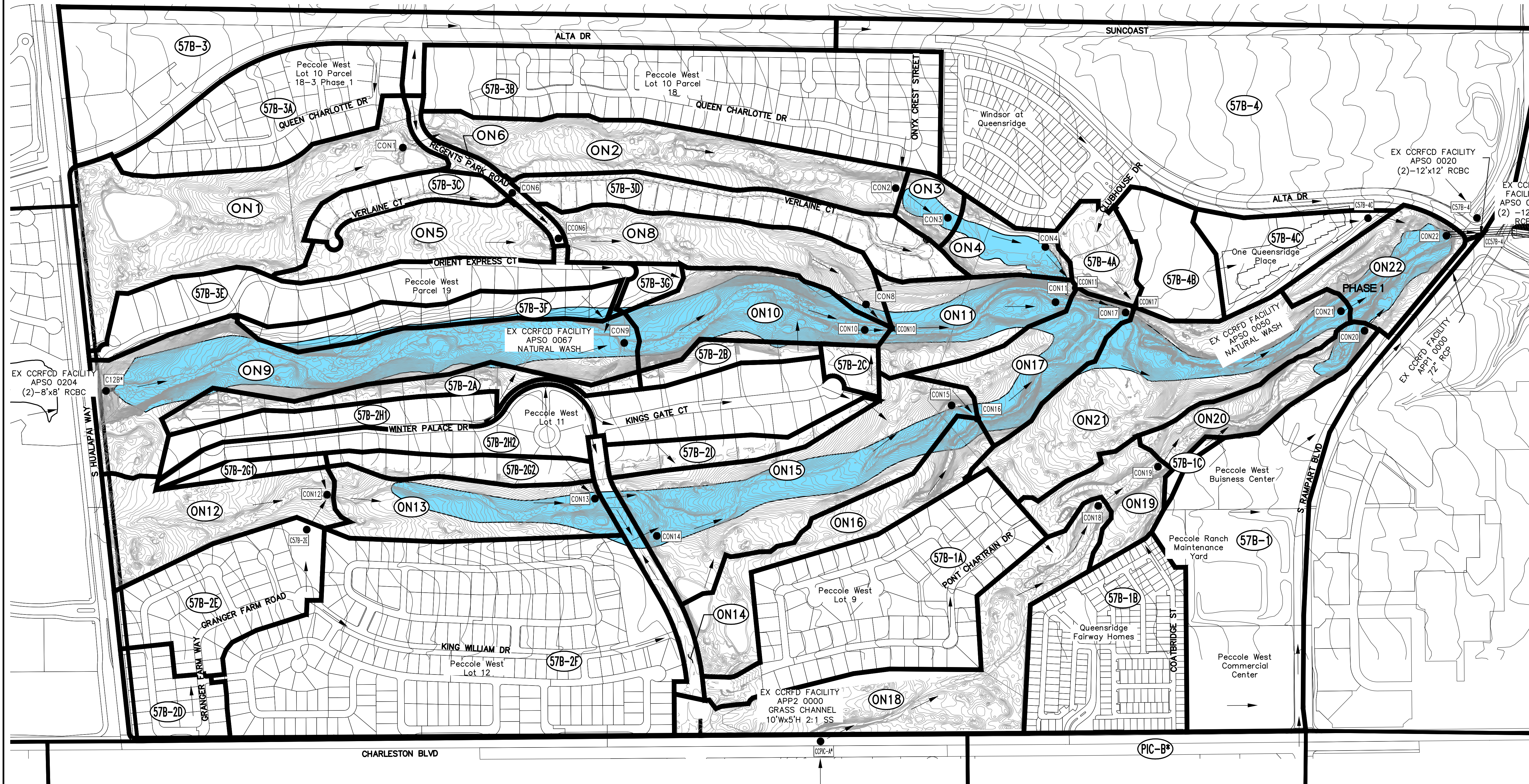
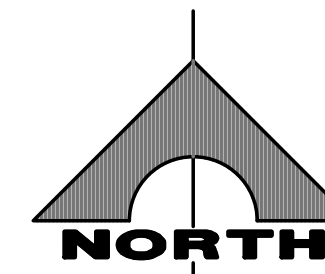
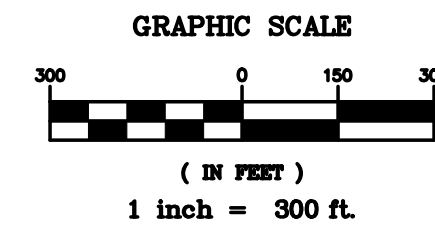
Drainage Areas and Flow Patterns - The subbasins and flow patterns used for the hydrologic modeling were determined from elevations established for the project site in a master grading digital file. Offsite hydrology was determined from research of existing drainage studies for adjacent developments.

Lag Time - The lag time (TLAG) is described as the time between the center of mass of rainfall and the time of peak discharge from a basin. Lag time can be related to time of concentration (T_c) by the following relationship: $TLAG = 0.6 (T_c)$. The time of concentration (T_c) is defined as the time required for runoff to flow from the most hydraulically distant area of the basin to the outlet of the basin or a design point. The procedure for calculating T_c is outlined in Section 602 of the Manual. Lag time calculations for the drainage subbasins have been included in Appendix A on Standard Form 4.

VI. EXISTING CONDITIONS

The site is presently developed as a golf course with existing washes traversing the project site conveying flows from west to east. A site visit was performed to confirm drainage patterns within the site and for parcels adjacent to the site. Offsite flows impact the site from the west and south. Offsite flows are conveyed to the site from the west via an existing dual (2) 8-foot wide by 8-foot high RCBC (CCRFCF Facility APSO 0204) under Hualapai Way. Additionally, offsite flows are conveyed to the site from the south via an existing RCBC under Charleston Boulevard. Offsite flows from residential subdivisions and commercial development adjacent to the golf course are discharged to the existing golf course as surface flow through existing storm drain and/or drainage easements. Flows conveyed through the site are discharged northeast to existing CCRFCF Facility APSO 0020 a dual (2) - 12-foot wide by 12-foot high RCB located at the Rampart Boulevard and Alta Drive intersection.

Figure 5 depicts the subbasins and drainage patterns used in the existing conditions hydrologic analysis. Offsite subbasins west of Hualapai Way and south of Charleston Boulevard are referenced from the 2013 MPU ALLGOW3 HEC-1 Model. The portion of the 2013 MPU tributary to 2013 MPU Concentration Point CC57B-4 located at the intersection of Alta and Rampart has been revised with this report. The model has been revised to determine onsite project specific flow rates and existing conditions flow rates discharged to CCRFCF Facilities APSO 0020 and APSO 0000. Copies of Figures H-29 and H-30 from the 2013 MPU have been included in Appendix C. The results of the Existing Conditions HEC-1 model are summarized in Table 1. A copy of the Existing Conditions HEC-1 model output is included in Appendix A.



SUMMARY OF EXISTING CONDITIONS HEC-1 MODEL			
SB OR CP	AREA (AC)	100 YR (CFS)	10 YR (CFS)
57B-1	31.1	80	40
57B-1A	28.4	54	20
57B-1B	19.3	51	25
57B-1C	0.6	2	1
57B-2A	6.3	14	6
57B-2B	3.0	8	3
57B-2C	1.7	5	2
57B-2D	5.7	16	7
57B-2E	14.5	42	19
57B-2F	57.8	147	69
57B-2G	1.6	5	2
57B-2H1	4.6	12	5
57B-2H2	10.0	21	9
57B-2I	4.6	12	5
57B-3	30.8	44	28
57B-3A	16.6	36	14
57B-3B	32.8	66	25
57B-3C	4.4	11	4
57B-3D	11.8	26	11
57B-3E	16.0	32	13
57B-3F	7.4	17	7
57B-3G	1.5	4	2
57B-4	82.7	202	101
57B-4A	4.5	8	3
57B-4B	7.1	24	13
57B-4C	7.8	23	12
C12B*	-	2134	990
C57B-2E	-	56	26
C57B-4	-	259	127
C57B-4C	-	47	25
C57B-4	-	4720	2354
CCON6	-	36	14
CCON10	-	2128	1025
CCON11	-	2227	1065
CCON17	-	2472	1171
CCPIC-A*	-	1895	900
CON1	-	86	32
CON2	-	164	55
CON3	-	189	64
CON4	-	195	66
CON6	-	18	8
CON8	-	54	19
CON9	-	2120	1012
CON10	-	2120**	1015
CON11	-	2128	1017
CON12	-	83	36
CON13	-	118	49
CON14	-	174	79
CON15	-	346	142
CON16	-	367	150
CON17	-	368	153
CON18	-	1912	906
CON19	-	1954	923
CON20	-	1944	923
CON21	-	2493	1177
CON22	-	4209	2065
ON1	25.4	50	18
ON2	17.5	31	11
ON3	2.5	6	2
ON4	4.7	9	3
ON5	9.4	18	7
ON6	2.3	8	4
ON8	12.2	27	9
ON9	25.5	41	14
ON10	11.4	24	8
ON11	10.0	19	7
ON12	11.6	23	8
ON13	12.0	23	8
ON14	3.5	6	2
ON15	22.5	42	15
ON16	11.5	23	8
ON17	9.1	20	7
ON18	20.3	31	10
ON19	6.4	12	4
ON20	6.6	12	4
ON21	22.3	34	12
ON22	8.5	19	6
PIC-B*	282.2	442	205

* Referenced Subbasin/Concentration Point from 2013 MPU
**The HEC-1 node shown identifies the controlling concentration point for the associated facility and is located upstream of this facility due to decreasing peak flow with increasing tributary area caused by storm distribution transitions, depth area reduction factors, or attenuation of flow for routing.

- LEGEND
- SUBBASIN BOUNDARY
 - DRAINAGE SUBBASIN
 - CONCENTRATION POINT
 - FLOW DIRECTION
 - ZONE A SFHA FLOODPLAIN

TABLE 1 SUMMARY OF EXISTING CONDITIONS HEC-1 MODEL			
SB OR CP*	AREA (AC)	100 YR (CFS)	10 YR (CFS)
57B-1	31.1	80	40
57B-1A	28.4	54	20
57B-1B	19.3	51	25
57B-1C	0.6	2	1
57B-2A	6.3	14	6
57B-2B	3.0	8	3
57B-2C	1.7	5	2
57B-2D	5.7	16	7
57B-2E	14.5	42	19
57B-2F	57.8	147	69
57B-2G1	1.6	5	2
57B-2G2	4.6	12	5
57B-2H1	18.6	32	13
57B-2H2	10.0	21	9
57B-2I	4.6	12	5
57B-3	30.8	44	28
57B-3A	16.6	36	14
57B-3B	32.8	66	25
57B-3C	4.4	11	4
57B-3D	11.8	26	11
57B-3E	16.0	32	13
57B-3F	7.4	17	7
57B-3G	1.5	4	2
57B-4	82.7	202	101
57B-4A	4.5	8	3
57B-4B	7.1	24	13
57B-4C	7.8	23	12
C12B*	-	2134	990
C57B-2E	-	56	26
C57B-4	-	259	127
C57B-4C	-	47	25
CC57B-4	-	4720	2354
CCON6	-	36	14
CCON10	-	2128	1025
CCON11	-	2227	1065
CCON17	-	2472	1171
CCPIC-A*	-	1895	900
CON1	-	86	32
CON2	-	164	55
CON3	-	189	64
CON4	-	195	66
CON6	-	18	8
CON8	-	54	19
CON9	-	2120	1012
CON10	-	2120**	1015
CON11	-	2128	1017

TABLE 1 SUMMARY OF EXISTING CONDITIONS HEC-1 MODEL			
SB OR CP*	AREA (AC)	100 YR (CFS)	10 YR (CFS)
CON12	-	83	36
CON13	-	118	49
CON14	-	174	79
CON15	-	346	142
CON16	-	367	150
CON17	-	368	153
CON18	-	1912	906
CON19	-	1954	923
CON20	-	1944	923
CON21	-	2493	1177
CON22	-	4209	2065
ON1	25.4	50	18
ON2	17.5	31	11
ON3	2.5	6	2
ON4	4.7	9	3
ON5	9.4	18	7
ON6	2.3	8	4
ON8	12.2	27	9
ON9	25.5	41	14
ON10	11.4	24	8
ON11	10.0	19	7
ON12	11.6	23	8
ON13	12.0	23	8
ON14	3.5	6	2
ON15	22.5	42	15
ON16	11.5	23	8
ON17	9.1	20	7
ON18	20.3	31	10
ON19	6.4	12	4
ON20	6.6	12	4
ON21	22.3	34	12
ON22	8.5	18	6
PIC-B*	282.2	442	205

*See Figure 5

**The HEC-1 node shown identifies the controlling concentration point for the associated facility and is located upstream of this facility due to decreasing peak flow with increasing tributary area caused by storm distribution transitions, depth area reduction factors, or attenuation of flow for routing.

The existing conditions flow rate of 4,720 cfs (Concentration Point CC57B-4) conveyed to the CCRFCD Facilities APSO 0020 and APSO 0000 is slightly greater (<2%) than the 2013 MPU flow rate of 4,628 cfs shown at this location. The increase in flow rate is due to the increase in the CN values as a result of the updated soils classification for the site, and project specific hydrology revisions within the area bounded by Alta Drive, Rampart Boulevard, Charleston Boulevard and Hualapai Way.

VII. PROPOSED CONDITIONS

The Seventy will be mass graded and the proposed onsite storm drain improvements will be constructed during proposed conditions. Proposed conditions drainage patterns are similar to existing conditions. Figure 6A depicts the subbasins and drainage patterns used in the proposed conditions hydrologic analysis. The results of the Proposed Conditions HEC-1 model are summarized in Table 2. A copy of the Proposed Conditions HEC-1 model output is included in Appendix A.

TABLE 2 SUMMARY OF PROPOSED CONDITIONS HEC-1 MODEL			
SB OR CP¹	AREA (AC)	100 YR (CFS)	10 YR (CFS)
57B-1	31.1	80	40
57B-1A	28.4	54	20
57B-1B	19.3	51	25
57B-1C	0.6	2	1
57B-2A	6.3	14	6
57B-2B	3.0	8	3
57B-2C	1.7	5	2
57B-2D	5.7	16	7
57B-2E	14.5	42	19
57B-2F	57.8	147	69
57B-2G1	1.6	5	2
57B-2G2	4.6	12	5
57B-2H1	18.6	32	13
57B-2H2	10.0	21	9
57B-2I	4.6	12	5
57B-3	30.8	63	28
57B-3A	16.6	36	14
57B-3B	32.8	66	25
57B-3C	4.4	11	4
57B-3D	11.8	26	11
57B-3E	16.0	32	13
57B-3F	7.4	17	7
57B-3G	1.5	4	2
57B-4	82.7	202	101
57B-4B	7.1	24	13

TABLE 2			
SUMMARY OF PROPOSED CONDITIONS HEC-1 MODEL			
SB OR CP¹	AREA (AC)	100 YR (CFS)	10 YR (CFS)
57B-4C	7.8	23	12
C12B*	-	2134	990
C57B-2E	-	56	26
C57B-4	-	259	127
C57B-4C	-	47	25
CC57B-4	-	4673	2326
CCON10	-	2128	1025
CCON6	-	36	14
CCON18R	-	1933	913
CCPIC-A*	-	1895	900
CDON2	-	2476	1169
CDON3	-	4177	2058
CDON4	-	4177**	2059
CON1	-	86	32
CON2	-	164	55
CON3R	-	191	65
CON6	-	18	8
CON8	-	54	19
CON9	-	2120	1012
CON10	-	2120**	1015
CON11R	-	2130	1026
CON12	-	83	36
CON13	-	118	49
CON14	-	174	79
CON15R	-	344	142
CON16R	-	364	149
CON18R	-	1910	905
CP19	-	1933**	920
CP20	-	1933**	920
CPPH1	-	2450	1153
DON1	10.8	34	18
DON2	19.5	60	31
DON3	21.1	65	34
DON4	17.4	44	23
ON1	25.4	50	18
ON2	17.5	31	11
ON3R	4.1	9	3
ON5	9.4	18	7
ON6	2.3	8	4
ON8	12.2	27	9
ON9	25.5	41	14
ON10	11.4	24	8
ON11R	5.1	11	4
ON12	11.6	23	8
ON13	12.0	23	8
ON14	3.5	6	2
ON15R	21.5	41	14

TABLE 2 SUMMARY OF PROPOSED CONDITIONS HEC-1 MODEL			
SB OR CP¹	AREA (AC)	100 YR (CFS)	10 YR (CFS)
ON16R	10.9	23	8
ON18R	18.5	28	10
PIC-B*	282.2	442	205

¹See Figure 6A

*Referenced Subbasin/Concentration Point from 2013 MPU

**The HEC-1 node shown identifies the controlling concentration point for the associated facility and is located upstream of this facility due to decreasing peak flow with increasing tributary area caused by storm distribution transitions, depth area reduction factors, or attenuation of flow for routing.

The proposed conditions flow rate of 4,673 cfs (Concentration Point CC57B-4) conveyed to the CCRFCD Facilities APSO 0020 and APSO 0000 is slightly lower than the existing conditions flow rate of 4,720 cfs. Additionally, the proposed conditions flow rate of 4,673 cfs is slightly greater (<1%) than the 2013 MPU flow rate of 4,628 cfs shown at this location. The increase in flow rate is due to the increase in the CN values for onsite subbasins as a result of the updated soils classification for the site and reducing the size of the onsite subbasins for project specific hydrology. The existing CCRFCD Facilities have adequate hydraulic capacity to convey proposed conditions flow rates from the site to the existing Angel Park Detention Basin.

Onsite Mass Grading

Proposed onsite drainage patterns and rough grading are depicted on Figure 6B. Subbasins impacting the proposed rough graded channels have been prorated to determine the specific flow rates to the proposed rough graded channel sections. The prorated flows are based on the total cfs per acre of tributary area. Prorated flows are summarized on Table 3.

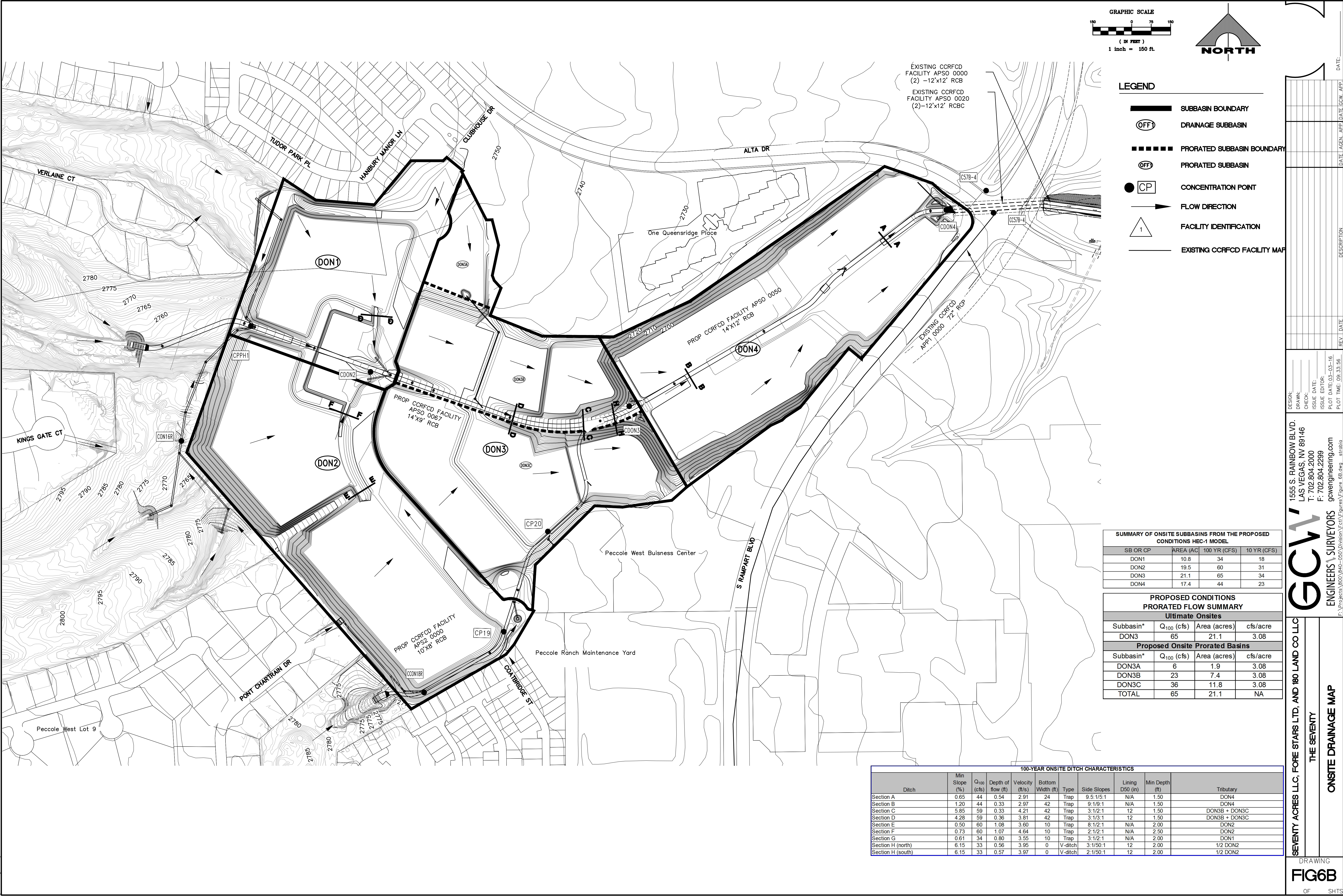
TABLE 3 PROPOSED CONDITIONS PRORATED FLOW SUMMARY			
Proposed Onsite Subbasins			
Subbasin ¹	Q ₁₀₀ (cfs)	Area (acres)	cfs/acre
DON3	65	21.1	3.08
Proposed Onsite Prorated Subbasins			
Subbasin*	Q ₁₀₀ (cfs)	Area (acres)	cfs/acre
DON3A	6	1.9	3.08
DON3B	23	7.4	3.08
DON3C	36	11.8	3.08
TOTAL	65	21.1	NA

¹See Figures 6A and 6B.

The onsite rough graded ditches are summarized in Table 4. Ditch calculations have been included in Appendix B.

TABLE 4 100-YEAR ROUGH GRADING DITCH CHARACTERISTICS										
Ditch ¹	Min Slope (%)	Q ₁₀₀ (cfs)	Depth of flow (ft)	Velocity (ft/s)	Bottom Width (ft)	Type	Side Slopes	Lining D50 (in)	Min Depth (ft)	Tributary
Section A	0.65	44	0.54	2.91	24	Trap	9.5:1/5:1	N/A	1.50	DON4
Section B	1.20	44	0.33	2.97	42	Trap	9:1/9:1	N/A	1.50	DON4
Section C	5.85	59	0.33	4.21	42	Trap	3:1/2:1	12	1.50	DON3B + DON3C
Section D	4.28	59	0.36	3.81	42	Trap	3:1/3:1	12	1.50	DON3B + DON3C
Section E	0.50	60	1.08	3.60	10	Trap	8:1/2:1	N/A	2.00	DON2
Section F	0.73	60	1.07	4.64	10	Trap	2:1/2:1	N/A	2.50	DON2
Section G	0.61	34	0.80	3.55	10	Trap	3:1/2:1	N/A	2.00	DON1
Section H (north)	6.15	33	0.56	3.95	0	V-ditch	3:1/50:1	12	2.00	1/2 DON2
Section H (south)	6.15	33	0.57	3.97	0	V-ditch	2:1/50:1	12	2.00	1/2 DON2

¹See Figures 6A and 6B.



SEVENTY ACRES LLC, FORE STARS LTD, AND 180 LAND CO LLC

THE SEVENTY

ONSITE DRAINAGE MAP

DESIGN:
DRAWN:
CHECK:
ISSUE DATE: 03-03-16
PLOT DATE: 03-03-16
PLOT TIME: 09:33:56

1555 S. RAINBOW BLVD.
LAS VEGAS, NV 89146
T: 702.804.2000
F: 702.804.2299
gcnwengineering.com

FIG6B

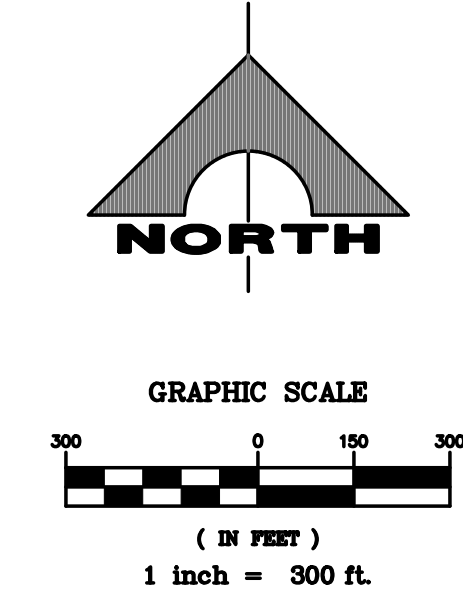
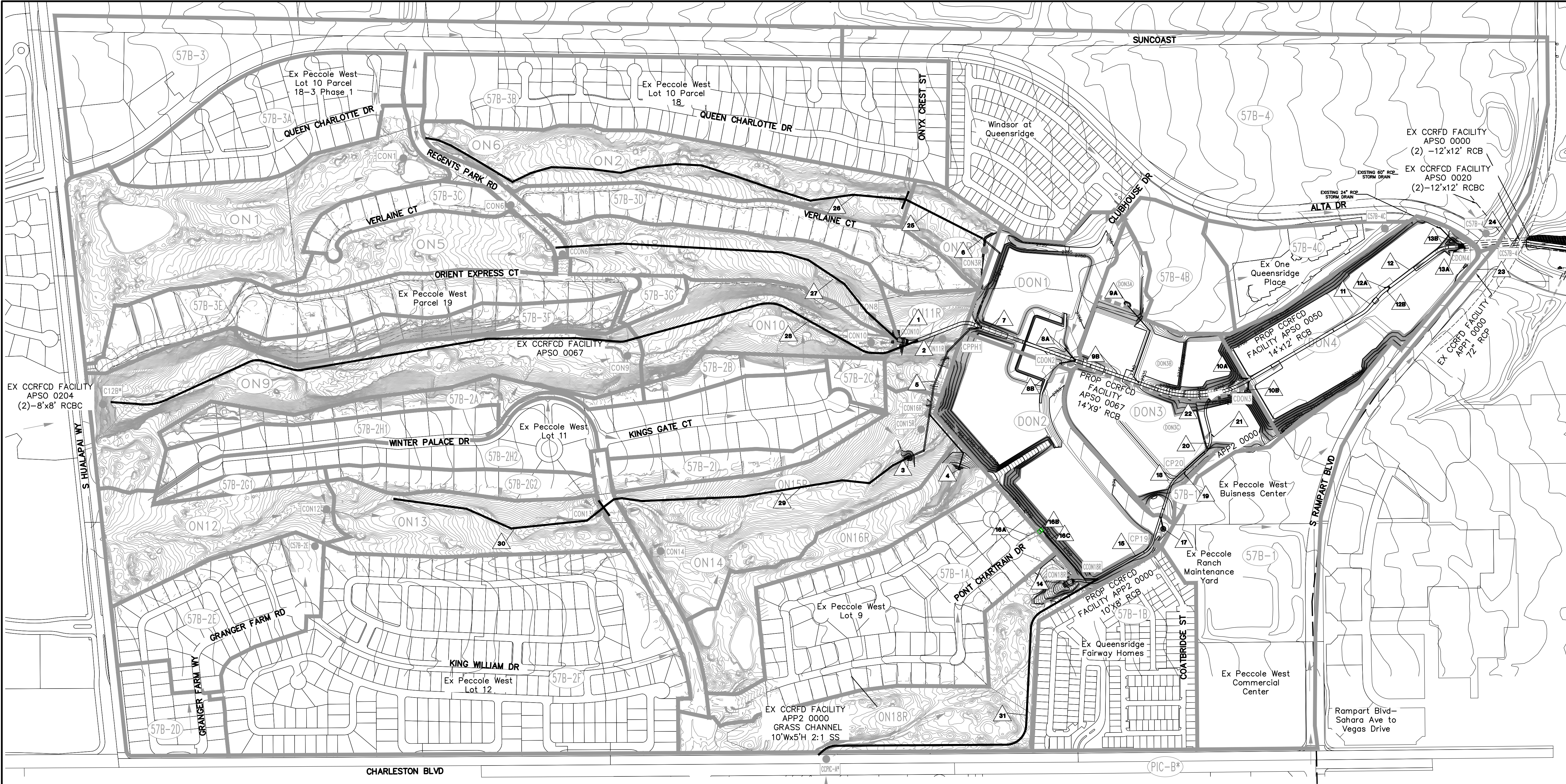
A site visit was performed to determine drainage patterns within APNs 138-32-311-002, 138-32-311-004, and 138-32-311-005. The total area tributary to site from these parcels was determined to be approximately 0.6 acres. The tributary area from these parcels is shown as Subbasin 57B-1C in the existing and proposed conditions hydrologic analyses. Subbasin 57B-1C generates 2 cfs during the 100-year storm event. The total flow is discharged at three locations along the boundary of the site. The discharge from the offsite parcel includes flow from an existing block wall opening, sheet flow from the site, and discharge from a curb opening. An NDOT Type 2 Drop Inlet and stub is proposed to intercept flow from the block wall opening. Two additional 18-inch RCP capped storm drain stubs are provided to intercept flows from these areas in the future. The future improvements for the site will safely convey flows from these adjacent parcels to the onsite storm drain system.

VIII. ULTIMATE CONDITIONS

The Two Fifty and all offsite areas are fully developed during ultimate conditions. Due to the size of the future estate lots (minimum 1 to 5± acres), curve numbers for the future One Eighty subbasins will be less than or equal to the curve numbers presented in this report for existing and proposed conditions. A separate analysis for ultimate conditions was not warranted since all offsite areas tributary to the site upstream of the overall Two Fifty development at Hualapai Way and Charleston Boulevard are already developed in proposed conditions. The proposed conditions flow rate of 4,673 cfs at CC57B-4 is considered to be the ultimate conditions flow rate conveyed to the dual (2) - 12-foot wide by 12-foot high RCB located at the Rampart Boulevard and Alta Drive intersection for the purposes of this report.

IX. STORM DRAIN FACILITIES AND PROTECTION

All proposed flood control facilities have been shown on Figure 7 and the plans included herewith. The design for the proposed facilities has been based on proposed conditions flow rates. Design of the storm drain facilities within the future One Eighty development have been based on normal depth calculations. Proposed mainline and lateral pipe sizes within the future One Eighty development were calculated using normal depth and have been upsized by 6 inches in diameter to provide for losses and future design flexibility. Proposed mainline and lateral RCB sizes include 1 foot of freeboard to account for storm



- LEGEND**
- ON1 SUBBASIN NAME
 - OFF1 PRORATED SUBBASIN NAME
 - SUBBASIN BOUNDARY
 - FLOW DIRECTION
 - FACILITY IDENTIFICATION
 - PRORATED SUBBASIN
 - FACILITY BREAKLINE
 - CP1 CONCENTRATION POINT

FLOOD PROTECTION FACILITIES

LOCATION	Q ₁₀₀ (cfs)	FACILITY	TRIBUTARY	MPU Q ₁₀₀ (cfs)	MPU FACILITY
1	2,130	20'x9' RCB; 14' DEEP MIN SUMP; D50=12";T=24"	CCON10	-	-
2	2,130	15'x9' RCB	CON11R	2384	APSP 0067
3	344	72" RCP; 11.0' DEEP MIN SUMP; D50=12";T=24"	ON15R	-	-
4	23	48" RCP; 3.0' DEEP MIN SUMP; D50=12";T=24"	ON16R	-	-
5	364	72" RCP	CON16R	-	-
6	191	72" RCP	CON3R	-	-
7	2,450	14'x9' RCB	CPPH1	2384	APSP 0067
8A	34	48" RCP; 3.5' DEEP MIN SUMP; D50=12";T=24"	DON1	-	-
8B	60	48" RCP; 4.5' DEEP MIN SUMP; D50=12";T=24"	DON2	-	-
9A	6	24" RCP; 3.5' DEEP MIN SUMP; D50=12";T=24"	DON3A	-	-

LOCATION	Q ₁₀₀ (cfs)	FACILITY	TRIBUTARY	MPU Q ₁₀₀ (cfs)	MPU FACILITY
9B	2476	14'x9' RCB	CDON2	-	-
10A	23	48" RCP; 3.5' DEEP MIN SUMP; D50=12";T=24"	DON3B	-	-
10B	36	48" RCP; 4' DEEP MIN SUMP; D50=12";T=24"	DON3C	-	-
11	4,177	14'x12' RCB	CDON3	4,628	APSO 0050
12	4,177	14'x12' RCB	CDON3	4,628	APSO 0050
12A	22	24" RCP CAPPED	N/A	-	-
12B	22	24" RCP CAPPED	N/A	-	-
13A	22	36" RCP; 3.5' DEEP MIN SUMP; D50=12";T=24"	1/2 DON4	-	-
13B	22	36" RCP; 3.5' DEEP MIN SUMP; D50=12";T=24"	1/2 DON4	-	-
14	1,910	20'x9' RCB; 12' DEEP MIN SUMP; D50=12";T=24"	CON18R	-	-

LOCATION	Q ₁₀₀ (cfs)	FACILITY	TRIBUTARY	MPU Q ₁₀₀ (cfs)	MPU FACILITY
15	1,933	10'x8' RCB	CON18R	2,004	APP2 0000
16A	54	EX. CONCRETE DRAINAGE EASEMENT	57B-1A	-	-
16B	54	PROPOSED CONCRETE FLUME	57B-1A	-	-
16C	54	48" RCP	57B-1A	-	-
17	51	42" RCP; 4.5' DEEP MIN SUMP; D50=12";T=24"	57B-1B	-	-
18	1,933	10'x8' RCB	CCON18R	2,004	APP2 0000
19	2	18" RCP; 0.5' DEEP MIN AREA DRAIN; NDOT TYPE 2A	1/2 57B-1C	-	-
20	1,933	10'x8' RCB	CP20	2,004	APP2 0000
21	2	18" RCP; STUB (PLUGGED)	N/A	-	-
22	1,933	10'x8' RCB	CP20	2,004	APP2 0000

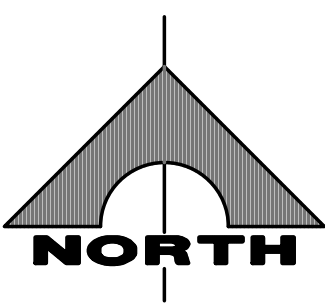
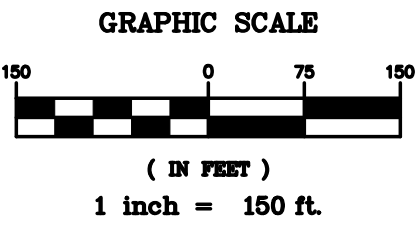
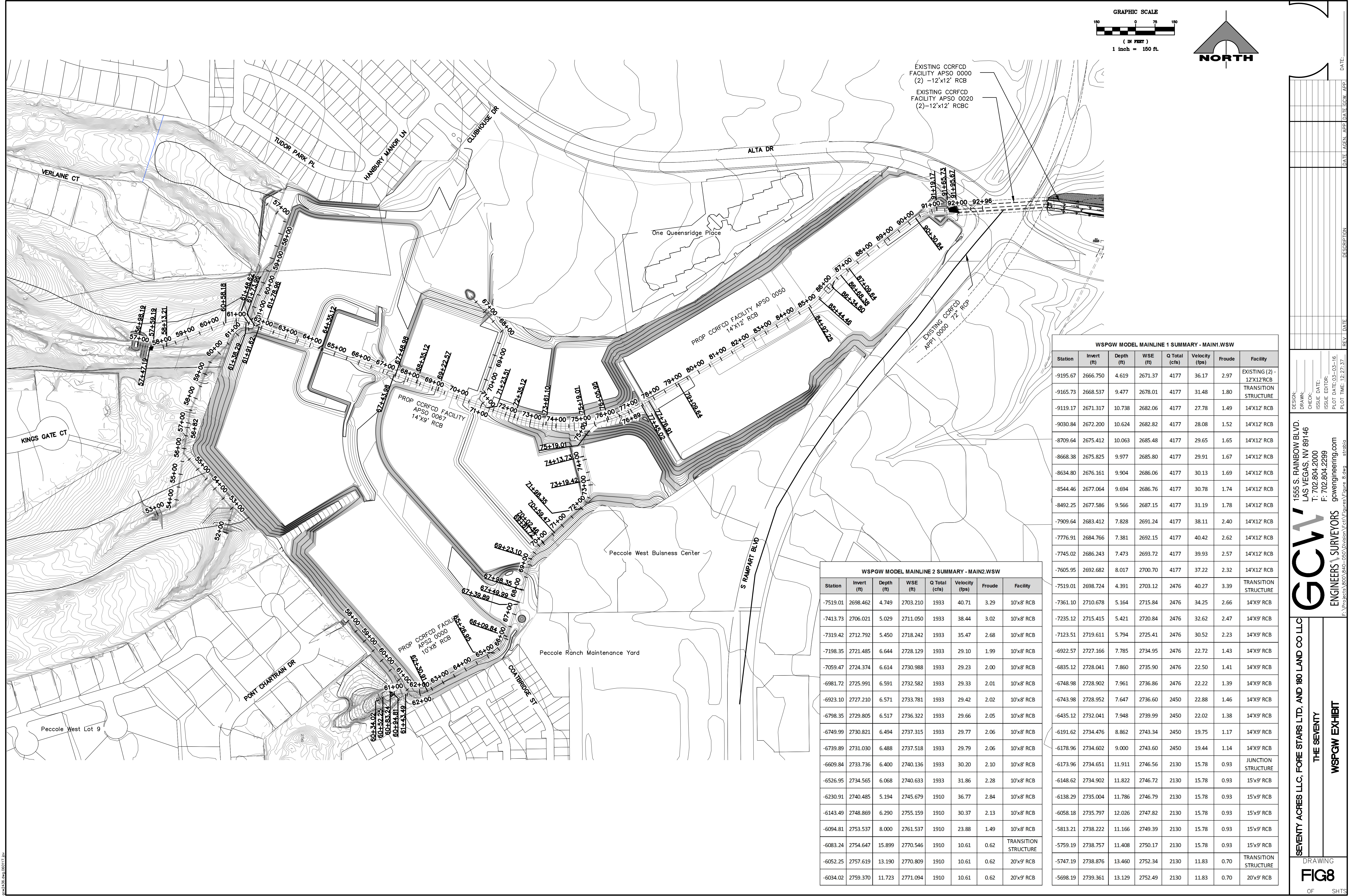
LOCATION	Q ₁₀₀ (cfs)	FACILITY	TRIBUTARY	MPU Q ₁₀₀ (cfs)	MPU FACILITY
23	-	-	-	442	APP1 0000
24	-	-	-	4,628	APSO 0020
25	191	54" RCP	CON3R	-	-
26	164	54" RCP	CON2	-	-
27	54	36" RCP	CON8	2,384	APSO 0067
28	2,128	11'x9' RCB	CCON10	-	-
29	344	66" RCP	CON15R	-	-
30	118	48" RCP	CON13	-	-
31	1,910	11'x8' RCB	CON8R	2,004	APP2 0000

drain losses. Normal depth calculations with proposed future slopes for The One Eighty recommended facilities have been included in Appendix B. Note that detailed hydraulic analysis for The One Eighty proposed facilities will be required in future technical drainage study submittals for this project. Hydraulic calculations for the recommended facilities have been included in Appendix B.

The Seventy proposed Mainline 1 RCB extends the existing CCRFCD Facility APSO 0020 dual (2) - 12-foot wide by 12-foot high RCB's in Rampart Boulevard approximately 3,500 linear feet west through the proposed site. Mainline 1 consists of an approximately 30 linear feet junction structure; 1,560 linear feet of 14-foot wide by 12-foot high RCB; an 87 linear feet junction structure; 1,345 linear feet of 14-foot wide by 9-foot high RCB; 415 linear feet of 15-foot wide by 9-foot high RCB; a 12 linear feet transition structure; and 49 linear feet of 20-foot wide by 9-foot high RCB improved inlet. Mainline 1 will collect and convey offsite flows generated west and south of the project site northeast to the existing dual (2) - 12-foot wide by 12-foot high RCB located at the Rampart Boulevard and Alta Drive intersection.

Mainline 2 consists of approximately 1,425 linear feet of 10-foot wide by 8-foot high RCB; a 12 linear feet transition structure; and 49 linear feet of 20-foot wide by 9-foot high RCB improved inlet. Mainline 2 will collect and convey offsite flows generated south of the project site north to Mainline 1.

Hydraulic modeling for the proposed RCB storm drain mainlines and RCP laterals were performed with the CIVILDESIGN Corp. WSPGW Water Surface Pressure Gradient Package (Reference 8, hereinafter referred to as WSPGW). Copies of the WSPGW models for the proposed storm drain facilities have been included in Appendix B. Electronic copies of the models have been included on CD in the Appendix. Note that the flows at the concentration points nodes from the proposed conditions HEC-1 Model were used to model the proposed storm drain mainlines. Lateral storm flows in the mainline WSPGW models were adjusted, so the 100-year storm flows in downstream reaches match the concentration point peak flows along the mainline. The WSPGW models labeled "MAIN1" and "MAIN2" are for the proposed conditions Mainline 1 and Mainline 2 storm drain mainlines, respectively. A summary of the WSPGW results have been shown on Figure 8. The results of the WSPGW Mainline 1 and 2 models are summarized in Tables 5A and 5B, respectively.



EXISTING CORFCD
FACILITY APSO 0000
(2) -12'x12' RCB

EXISTING CORFCD
FACILITY APSO 0020
(2) -12'x12' RCBC

WSPGW MODEL MAINLINE 1 SUMMARY - MAIN1.WSW						
Station	Invert (ft)	Depth (ft)	WSE (ft)	Q Total (cfs)	Velocity (fps)	Froude
-9195.67	2666.750	4.619	2671.37	4177	36.17	2.97
-9165.73	2668.537	9.477	2678.01	4177	31.48	1.80
-9119.17	2671.317	10.738	2682.06	4177	27.78	1.49
-9030.84	2672.200	10.624	2682.82	4177	28.08	1.52
-8709.64	2675.412	10.063	2685.48	4177	29.65	1.65
-8668.38	2675.825	9.977	2685.80	4177	29.91	1.67
-8634.80	2676.161	9.904	2686.06	4177	30.13	1.69
-8544.46	2677.064	9.694	2686.76	4177	30.78	1.74
-8492.25	2677.586	9.566	2687.15	4177	31.19	1.78
-7909.64	2683.412	7.828	2691.24	4177	38.11	2.40
-7776.91	2684.766	7.381	2692.15	4177	40.42	2.62
-7745.02	2686.243	7.473	2693.72	4177	39.93	2.57
-7605.95	2692.682	8.017	2700.70	4177	37.22	2.32
-7519.01	2698.724	4.391	2703.12	2476	40.27	3.39
-7361.10	2710.678	5.164	2715.84	2476	34.25	2.66
-7235.12	2715.415	5.421	2720.84	2476	32.62	2.47
-7123.51	2719.611	5.794	2725.41	2476	30.52	2.23
-6922.57	2727.166	7.785	2734.95	2476	22.72	1.43
-6835.12	2728.041	7.860	2735.90	2476	22.50	1.41
-6748.98	2728.902	7.961	2736.86	2476	22.22	1.39
-6743.98	2728.952	7.647	2736.60	2450	22.88	1.46
-6435.12	2732.041	7.948	2739.99	2450	22.02	1.38
-6191.62	2734.476	8.862	2743.34	2450	19.75	1.17
-6178.96	2734.602	9.000	2743.60	2450	19.44	1.14
-6173.96	2734.651	11.911	2746.56	2130	15.78	0.93
-6148.62	2734.902	11.822	2746.72	2130	15.78	0.93
-6138.29	2735.004	11.786	2746.79	2130	15.78	0.93
-6058.18	2735.797	12.026	2747.82	2130	15.78	0.93
-5813.21	2738.222	11.166	2749.39	2130	15.78	0.93
-5759.19	2738.757	11.408	2750.17	2130	15.78	0.93
-5747.19	2738.876	13.460	2752.34	2130	11.83	0.70
-5698.19	2739.361	13.129	2752.49	2130	11.83	0.70

WSPGW MODEL MAINLINE 2 SUMMARY - MAIN2.WSW						
Station	Invert (ft)	Depth (ft)	WSE (ft)	Q Total (cfs)	Velocity (fps)	Froude
-7519.01	2698.462	4.749	2703.210	1933	40.71	3.29
-7413.73	2706.021	5.029	2711.050	1933	38.44	3.02
-7319.42	2712.792	5.450	2718.242	1933	35.47	2.68
-7198.35	2721.485	6.644	2728.129	1933	29.10	1.99
-7059.47	2724.374	6.614	2730.988	1933	29.23	2.00
-6981.72	2725.991	6.591	2732.582	1933	29.33	2.01
-6923.10	2727.210	6.571	2733.781	1933	29.42	2.02
-6798.35	2729.805	6.517	2736.322	1933	29.66	2.05
-6749.99	2730.821	6.494	2737.315	1933	29.77	2.06
-6739.89	2731.030	6.488	2737.518	1933	29.79	2.06
-6609.84	2733.736	6.400	2740.136	1933	30.20	2.10
-6526.95	2734.565	6.068	2740.633	1933	31.86	2.28
-6230.91	2740.485	5.194	2745.679	1910	36.77	2.84
-6143.49	2748.869	6.290	2755.159	1910	30.37	2.13
-6094.81	2753.537	8.000	2761.537	1910	23.88	1.49
-6083.24	2754.647	15.899	2770.546	1910	10.61	0.62
-6052.25	2757.619	13.190	2770.809	1910	10.61	0.62
-6034.02	2759.370	11.723	2771.094	1910	10.61	0.62

SEVENTY ACRES LLC, FORE STARS LTD, AND 180 LAND CO LLC

THE SEVENTY

WSPGW EXHIBIT

DESIGN: _____

DRAWN: _____

CHECK: _____

ISSUE DATE: _____

ISSUE EDITOR: _____

PLOT DATE: 03-03-16

PLOT TIME: 12:27:37

1555 S. RAINBOW BLVD.

LAS VEGAS, NV 89146

T: 702.804.2000

F: 702.804.2299

gownengineering.com

F:\Projects\800\840-950\Division\Fcrl\Figures\Figure 8.dwg

stribila

DATE: _____

AGN: _____

APP: _____

DATE: _____

AGW: _____

APP: _____

TABLE 5A
WSPGW MODEL MAINLINE 1 SUMMARY - MAIN1.WSW

Station*	Invert (ft)	Depth (ft)	WSE (ft)	Q Total (cfs)	Velocity (fps)	Froude	Facility
-9195.67	2666.750	4.619	2671.37	4177	36.17	2.97	EXISTING (2) – 12'X12'RCB
-9165.73	2668.537	9.477	2678.01	4177	31.48	1.80	TRANSITION STRUCTURE
-9119.17	2671.317	10.738	2682.06	4177	27.78	1.49	14'X12' RCB
-9030.84	2672.200	10.624	2682.82	4177	28.08	1.52	14'X12' RCB
-8709.64	2675.412	10.063	2685.48	4177	29.65	1.65	14'X12' RCB
-8668.38	2675.825	9.977	2685.80	4177	29.91	1.67	14'X12' RCB
-8634.80	2676.161	9.904	2686.06	4177	30.13	1.69	14'X12' RCB
-8544.46	2677.064	9.694	2686.76	4177	30.78	1.74	14'X12' RCB
-8492.25	2677.586	9.566	2687.15	4177	31.19	1.78	14'X12' RCB
-7909.64	2683.412	7.828	2691.24	4177	38.11	2.40	14'X12' RCB
-7776.91	2684.766	7.381	2692.15	4177	40.42	2.62	14'X12' RCB
-7745.02	2686.243	7.473	2693.72	4177	39.93	2.57	14'X12' RCB
-7605.95	2692.682	8.017	2700.70	4177	37.22	2.32	14'X12' RCB
-7519.01	2698.724	4.391	2703.12	2476	40.27	3.39	TRANSITION STRUCTURE
-7361.10	2710.678	5.164	2715.84	2476	34.25	2.66	14'X9' RCB
-7235.12	2715.415	5.421	2720.84	2476	32.62	2.47	14'X9' RCB
-7123.51	2719.611	5.794	2725.41	2476	30.52	2.23	14'X9' RCB
-6922.57	2727.166	7.785	2734.95	2476	22.72	1.43	14'X9' RCB
-6835.12	2728.041	7.860	2735.90	2476	22.50	1.41	14'X9' RCB

TABLE 5A
WSPGW MODEL MAINLINE 1 SUMMARY - MAIN1.WSW

Station*	Invert (ft)	Depth (ft)	WSE (ft)	Q Total (cfs)	Velocity (fps)	Froude	Facility
-6748.98	2728.902	7.961	2736.86	2476	22.22	1.39	14'X9' RCB
-6743.98	2728.952	7.647	2736.60	2450	22.88	1.46	14'X9' RCB
-6435.12	2732.041	7.948	2739.99	2450	22.02	1.38	14'X9' RCB
-6191.62	2734.476	8.862	2743.34	2450	19.75	1.17	14'X9' RCB
-6178.96	2734.602	9.000	2743.60	2450	19.44	1.14	14'X9' RCB
-6173.96	2734.651	11.911	2746.56	2130	15.78	0.93	JUNCTION STRUCTURE
-6148.62	2734.902	11.822	2746.72	2130	15.78	0.93	15'x9' RCB
-6138.29	2735.004	11.786	2746.79	2130	15.78	0.93	15'x9' RCB
-6058.18	2735.797	12.026	2747.82	2130	15.78	0.93	15'x9' RCB
-5813.21	2738.222	11.166	2749.39	2130	15.78	0.93	15'x9' RCB
-5759.19	2738.757	11.408	2750.17	2130	15.78	0.93	15'x9' RCB
-5747.19	2738.876	13.460	2752.34	2130	11.83	0.70	TRANSITION STRUCTURE
-5698.19	2739.361	13.129	2752.49	2130	11.83	0.70	20'x9' RCB

*See Figure 8.

TABLE 5B
WSPGW MODEL MAINLINE 2 SUMMARY - MAIN2.WSW

Station*	Invert (ft)	Depth (ft)	WSE (ft)	Q Total (cfs)	Velocity (fps)	Froude	Facility
-7519.01	2698.462	4.749	2703.210	1933	40.71	3.29	10'x8' RCB
-7413.73	2706.021	5.029	2711.050	1933	38.44	3.02	10'x8' RCB
-7319.42	2712.792	5.450	2718.242	1933	35.47	2.68	10'x8' RCB

TABLE 5B WSPGW MODEL MAINLINE 2 SUMMARY - MAIN2.WSW							
Station*	Invert (ft)	Depth (ft)	WSE (ft)	Q Total (cfs)	Velocity (fps)	Froude	Facility
-7198.35	2721.485	6.644	2728.129	1933	29.10	1.99	10'x8' RCB
-7059.47	2724.374	6.614	2730.988	1933	29.23	2.00	10'x8' RCB
-6981.72	2725.991	6.591	2732.582	1933	29.33	2.01	10'x8' RCB
-6923.10	2727.210	6.571	2733.781	1933	29.42	2.02	10'x8' RCB
-6798.35	2729.805	6.517	2736.322	1933	29.66	2.05	10'x8' RCB
-6749.99	2730.821	6.494	2737.315	1933	29.77	2.06	10'x8' RCB
-6739.89	2731.030	6.488	2737.518	1933	29.79	2.06	10'x8' RCB
-6609.84	2733.736	6.400	2740.136	1933	30.20	2.10	10'x8' RCB
-6526.95	2734.565	6.068	2740.633	1933	31.86	2.28	10'x8' RCB
-6230.91	2740.485	5.194	2745.679	1910	36.77	2.84	10'x8' RCB
-6143.49	2748.869	6.290	2755.159	1910	30.37	2.13	10'x8' RCB
-6094.81	2753.537	8.000	2761.537	1910	23.88	1.49	10'x8' RCB
-6083.24	2754.647	15.899	2770.546	1910	10.61	0.62	TRANSITION STRUCTURE
-6052.25	2757.619	13.190	2770.809	1910	10.61	0.62	20'x9' RCB
-6034.02	2759.370	11.723	2771.094	1910	10.61	0.62	20'x9' RCB

*See Figure 8.

Mainline 1

The approved WSPGW model for the existing dual (2) - 12-foot wide by 12-foot high RCBC (CCRFGD Facility APSO 0000) storm drain downstream of the existing dual (2) - 12-foot wide by 12-foot high RCBC (CCRFGD Facility APSO 0020) at the Rampart Boulevard and Alta Drive intersection has been referenced from the Queens Borough Culvert Study. Please note that the approved Queens Borough Culvert Study referenced a design flow rate of 4,497 cfs from the 2002 MPU. As previously stated, the 2013 MPU shows a flow rate of 4,628 cfs and the proposed conditions HEC-1 model presented in this report shows a proposed 100-year flow rate of 4,672 cfs. The approved Queens Borough Culvert Study WSPGW model has been extended south with this report to include the existing CCRFGD Facility APSO 0020 and the proposed Mainline 1 storm drain. The model also includes the junction where an existing 60-inch RCP and 72-inch RCP connect to APSO 0020 in Rampart Boulevard and the proposed condition flow rates at pertinent HEC-1 nodes. Inverts used in the hydraulic calculations for the existing dual (2) - 12-foot wide by 12-foot high RCBC are based on survey and as-built information. The WSPGW Model Stations from the Queens Borough Culvert Study have been included in the Mainline 1 Model and converted to match the proposed Mainline 1 Stationing. The WSPGW Model Station Conversion has been summarized in Table 6. Pertinent referenced material from the Queens Borough Culvert Study has been included in Appendix C.

**TABLE 6
WSPGW MODEL STATION
CONVERSION SUMMARY –
MAIN1.WSW**

WSPGW Stations Referenced from Queens Borough Culvert Study	MAIN 1 WSPGW Stations*
-3625.00	-12270.67
-3550.00	-12195.67
-3500.00	-12145.67
-3401.01	-12046.68
-3350.81	-11996.48
-3325.95	-11971.62
-3315.95	-11961.62
-3225.64	-11871.31
-3223.32	-11868.99
-3152.70	-11798.37
-3135.29	-11780.96

TABLE 6 WSPGW MODEL STATION CONVERSION SUMMARY – MAIN1.WSW	
WSPGW Stations Referenced from Queens Borough Culvert Study	MAIN 1 WSPGW Stations*
-3049.99	-11695.66
-2906.52	-11552.19
-2433.63	-11079.30
-2318.22	-10963.89
-2200.00	-10845.67
-1733.86	-10379.53
-1565.00	-10210.67
-1000.00	-9645.67

*See Figure 8.

The Mainline 1 model shows the existing CCRFCD Facility APSO 0000 has adequate capacity to convey proposed conditions 100-year storm event flow rates to the existing Angel Park Detention Basin. Proposed flow depths and flow velocities within the existing dual (2) - 12-foot wide by 12-foot high RCB are comparable to the approved Queens Borough Culvert Study Design. Approximately 2,819 linear feet of the proposed Mainline 1 RCB storm drain hydraulic grade line will be more than 1-foot below the RCB soffit between the connection to the dual (2) - 12-foot wide by 12-foot high RCB and approximately 197 linear feet downstream of the junction structure with the two 72-inch RCP laterals that connect to the mainline at WSPGW Station -6176.46. The hydraulic grade line is 2.4 feet to 2.9 feet above the 15-foot wide by 9-foot high RCB mainline for approximately 417 linear feet south of the junction with the two 72-inch RCP laterals that connect to Mainline 1 at WSPGW Station -6176.46. However, the hydraulic grade line will be more than 1-foot below finished grade elevation along the storm drain mainline. The maximum flow velocity of 41.04 feet per second occurs in Mainline 1 at WSPGW Station -7519.00.

Per Section 705.7.1.2 in the Manual, all concrete lining shall have a minimum thickness of 7 inches for flow velocities 30 feet per second and greater. Additionally, the pre-cast RCB will have an additional 1-inch of cover over the rebar and a 6,000 psi concrete strength where velocities exceed 25 feet per second.

Mainline 2

Approximately 1,400 linear feet of the proposed Mainline 2 RCB hydraulic grade line will be more than 1-foot below the RCB soffit.

The maximum flow velocity of 40.71 feet per second occurs in Mainline 2 just upstream of the connection to the Mainline 1 junction structure. Per Section 705.7.1.2 in the Manual, all concrete lining shall have a minimum thickness of 7 inches for flow velocities 30 feet per second and greater. Additionally, the pre-cast RCB will have an additional 1-inch of cover over the rebar and a 6,000 psi concrete strength where velocities exceed 25 feet per second.

WSPGW models have been included for proposed laterals extending to collect flows from future onsite development and existing offsite developments. Please refer to tables on Figure 7 for facility flows and sizes.

The proposed onsite ditches will convey the existing flows with a minimum of 1-foot of freeboard. Maximum slope was selected to verify velocity. Flows from the proposed ditches will be conveyed into the proposed Mainline 1 and 2 storm drain systems. Riprap (Minimum: $d_{50} = 12$ inches, Thickness = 24 inches) has been provided at the lateral sump locations up to the ponding depth, determined by an inlet control calculation. The inlet control calculations have been provided in Appendix B.

Area drains have been provided to collect flows at some of the sump locations. Calculations for the area drains have been included in Appendix B.

X. FEMA CONDITIONAL LETTER OF MAP REVISION (CLOMR)**Hydrologic Summary**

As a part of this project development, a CLOMR and Letter of Map Revision (LOMR) will be processed with FEMA to remap the Special Flood Hazard Area (SFHA) that currently routes through the site.

Since this project re-evaluates the existing hydrologic analysis for the subject wash, the project specific existing and proposed condition hydrologic analysis was used as the

effective hydrologic model to determine peak flow rates for use in establishing the limits of the revised SFHA.

Existing Condition

See Figure 9 - Existing Conditions HEC-RAS X-Section Map. The main wash through the site labeled Main 1 represents the major conveyance corridor for the mapped Zone A SFHA overlaying the site. Several fingers of the SFHA extend out from Main 1, and will be removed from the SFHA with the CLOMR submittal connected with this study since they are either remnant washes cut-off by upstream improvements or ineffective flow areas inundated by flows in the Main 1. Please note that the existing SFHA does not impact existing development.

Main 1

100-Year Flow at Upstream End = 2,128 cfs (Concentration Point CCON10)

This reach will be the remaining conveyance corridor of the mapped SFHA upon completion of the LOMR remapping.

North Finger

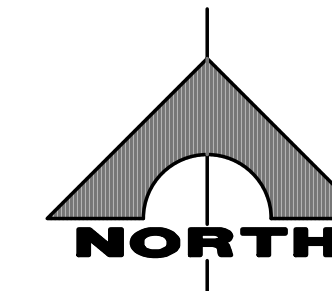
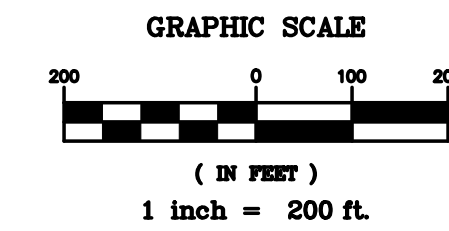
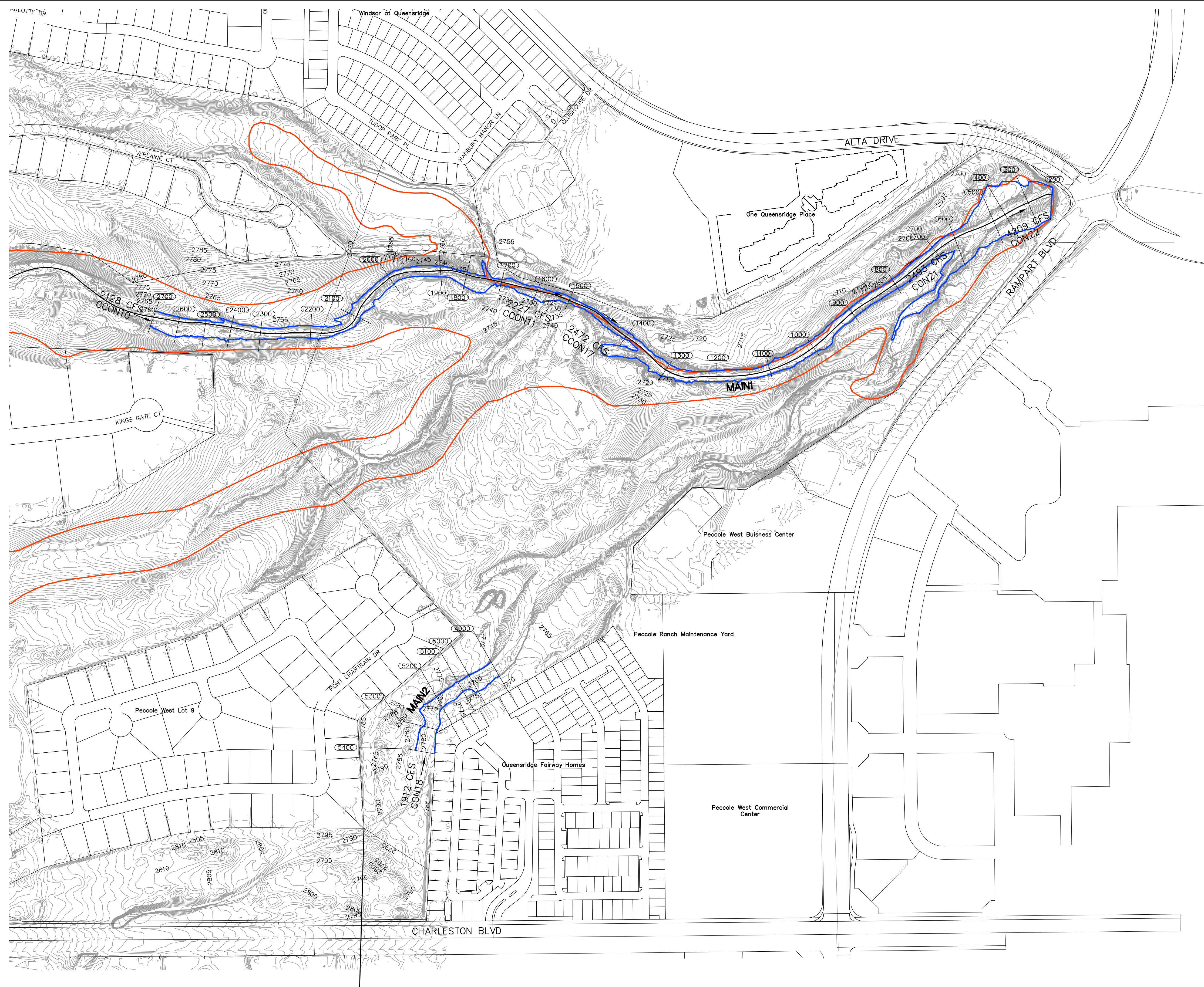
100-Year Flow = 195 cfs (Concentration Point CON4)

A finger of SFHA extends up an existing wash north of Main 1 for approximately 1,000 linear feet. Since this wash is a remnant wash, cut off by Hualapai Way and no longer conveying the historical flows originating from west of Hualapai Way, this finger will be removed from the SFHA. The wash located within an existing golf course conveys local drainage areas, and does not impact existing development.

South Finger

100-Year Flow = 368 cfs (Concentration Point CON17)

Similar to the North Finger, a finger of SFHA extends up an existing wash south of Main 1 for approximately 4,000 linear feet. This wash is also a remnant wash, cut off by Hualapai Way and no longer conveying the historical flows originating from west of Hualapai Way, and will be removed from the SFHA. The wash located within an existing golf course conveys local drainage areas, and does not impact existing development.



LEGEND

EFFECTIVE FLOODPLAIN LIMITS
 EXISTING CONDITION INUNDATION LIMITS

2147 CFS Q100 FLOW

CCON10 HEC-1 CONCENTRATION POINT

→ FLOW DIRECTION

MAIN1 HEC-RAS REACH

(2200) HEC-RAS STATION LABEL

HEC-RAS CROSS SECTION

MAIN 1 HE-RAS STATION SUMMARY TABLE									
Sta	Q (cfs)	FL Elevation (ft)	W.S. Elevation (ft)	Depth (ft)	Vel (ft/s)	Top Width (ft)	Froude #	Notes	
2700	2128	2756.00	2760.89	4.89	10.46	60.70	1.01	Existing	Wash
2600	2128	2752.00	2758.31	6.31	9.90	71.48	1.01	Existing	Wash
2500	2128	2748.00	2754.37	6.37	10.20	66.36	1.01	Existing	Wash
2400	2128	2747.00	2751.80	4.80	9.95	69.59	1.00	Existing	Wash
2300	2128	2744.00	2749.36	5.36	11.68	43.51	1.01	Existing	Wash
2200	2128	2740.00	2745.49	5.49	11.33	47.51	1.00	Existing	Wash
2100	2128	2736.00	2742.08	6.08	11.35	46.89	1.00	Existing	Wash
2000	2128	2729.00	2735.65	6.65	11.69	43.15	1.00	Existing	Wash
1900	2128	2724.00	2733.14	9.14	8.94	43.40	0.67	Existing	Wash
1800	2128	2719.00	2732.45	13.45	8	57.08	0.75	Existing	Wash
1700	2227	2716.00	2728.08	12.08	15.22	20.20	1.00	Existing	Wash
1600	2227	2711.00	2725.34	14.34	11.67	45.98	1.01	Existing	Wash
1500	2472	2707.00	2720.77	13.77	14.77	24.93	1.00	Existing	Wash
1400	2472	2702.00	2713.84	11.84	14.09	28.74	1.00	Existing	Wash
1300	2472	2699.00	2710.43	5.43	11.42	53.98	1.01	Existing	Wash
1200	2472	2695.00	2707.44	5.84	12.10	49.48	1.01	Existing	Wash
1100	2472	2691.00	2703.90	6.30	12.57	40.56	1.01	Existing	Wash
1000	2472	2687.00	2692.52	5.52	11.89	47.97	1.01	Existing	Wash
900	2472	2683.00	2689.15	6.15	12.63	39.48	1.00	Existing	Wash
800	2493	2679.00	2685.65	6.65	12.43	41.88	1.00	Existing	Wash
700	2493	2676.00	2685.62	9.62	7.03	49.85	0.46	Existing	Wash
600	2493	2674.00	2685.89	11.89	4.01	133.33	0.24	Existing	Wash
500	4209	2672.00	2685.74	13.74	4.33	143.10	0.29	Existing	Wash
400	4209	2671.00	2685.77	14.77	3.56	213.18	0.27	Existing	Wash
300	4209	2669.00	2685.77	16.77	3.04	178.22	0.19	Existing	Wash
200	4209	2668.00	2684.83	16.83	7.74	110.66	0.62	Existing	2(12)x12 RCB

MAIN 2 HEC-RAS STATION SUMMARY TABLE								
Sta	Q (cfs)	FL Elevation (ft)	W.S. Elevation (ft)	Depth (ft)	Vel (ft/s)	Total Width (ft)	Froude #	Notes
5400	1912	2780.00	2783.62	3.62	9.02	85.33	1.01	Existing Wash
5300	1912	2778.00	2781.81	3.81	10.24	67.57	1.13	Existing Wash
5200	1912	2776.00	2780.00	4.00	11.46	58.33	1.26	Existing Wash
5100	1912	2759.00	2762.99	3.99	16.44	44.34	1.79	Existing Wash
5000	1912	2758.00	2762.37	4.37	12.44	70.25	1.48	Existing Wash
4900	1912	2756.00	2760.64	4.64	10.50	63.82	1.09	Existing Wash

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EXISTING CONDITIONS HEC-RAS X-SECTION MAP

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ISSUE DATE: _____
ISSUE EDITOR: _____
PLOT DATE: 03-03-16

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REV	DATE
-----	------

DESCRIPTION

DATE	ACFN	APP	DATE	GCW	APP

DATE:

Main 2 Finger

100-Year Flow = 1,944 cfs (Concentration Point CON20)

A short finger extends south near the downstream end of the project at Rampart Boulevard for approximately 300 linear feet. This finger is located completely with the developed portion of the site and will be removed from the SFHA. The flows in this wash will be conveyed and contained in the Mainline 2 underground storm drain to Rampart Boulevard.

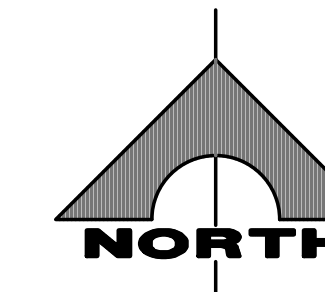
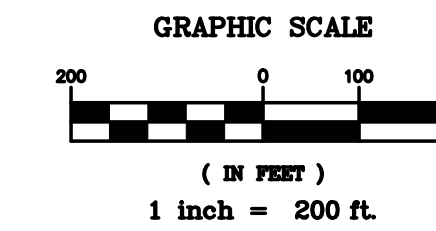
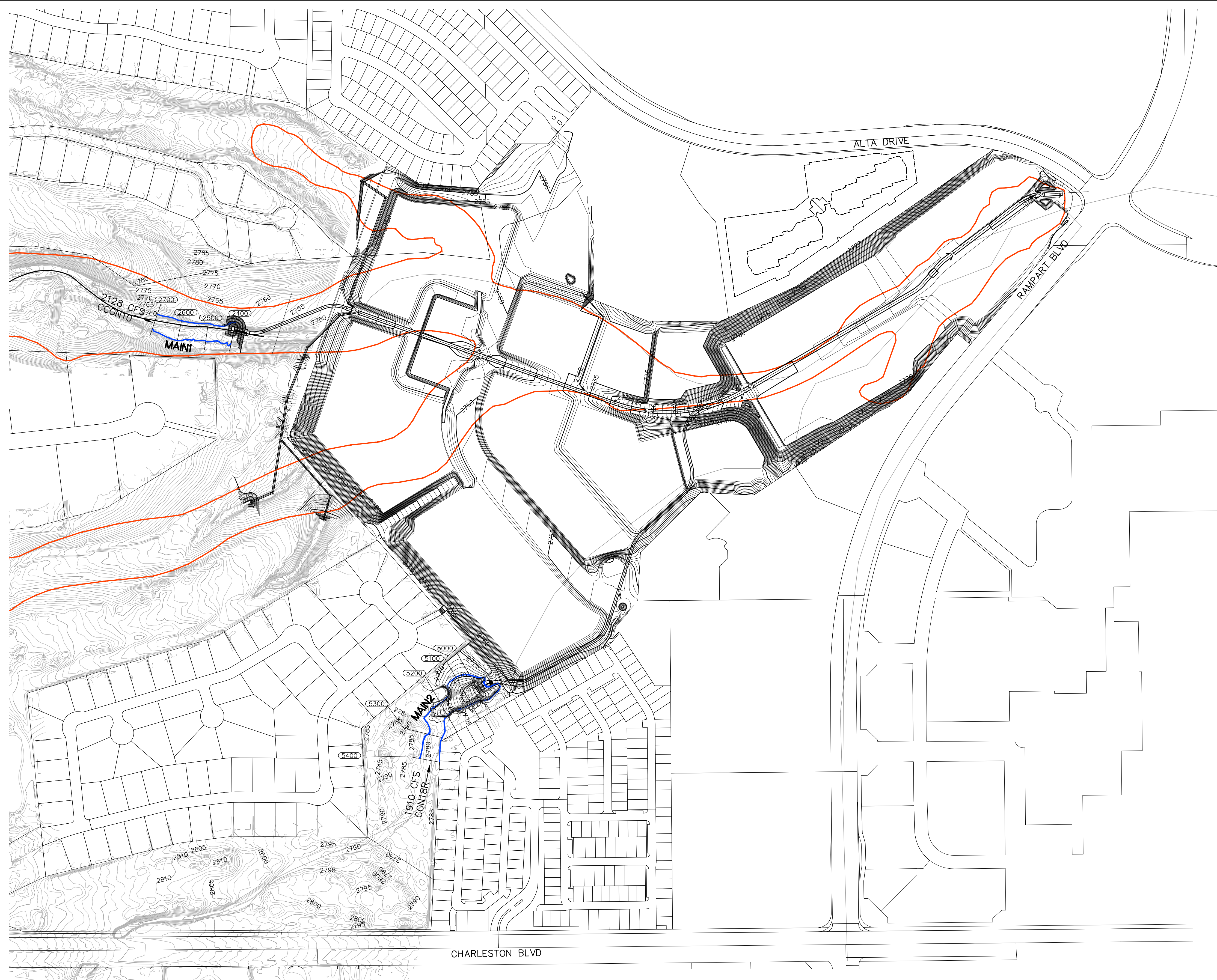
Several flow changes occur in the Main 1 wash as the above mentioned fingers combine with Main 1. Table 7 summarizes the effective flow rates used through the Main 1 wash to establish the effective water surface elevations through the Main 1 SFHA used to compare with the proposed condition water surface elevations.

TABLE 7 EFFECTIVE FLOW RATES – MAIN 1 WASH	
HEC-RAS River Station*	Effective Flow Rate (cfs)
2700	2,128
1700	2,227
1500	2,472
800	2,493
500	4,209




*See Figure 9.

Proposed Condition

See Figure 10 - Proposed Conditions HEC-RAS X-Section Map and Figure 11 - CLOMR Workmap. In the proposed condition, the portion within the project site will be contained within underground storm drain. The proposed floodplain will tie into the existing floodplain approximately 700 linear feet west of the project site as shown on the CLOMR Workmap. Table 8 summarizes the effective flow rates used through the Main 1 wash to establish the effective water surface elevations through the Main 1 SFHA used to compare to proposed condition water surface elevations.



LEGEND

- 
- Legend:
- EFFECTIVE FLOODPLAIN LIMITS
 - PROPOSED CONDITION INUNDATION LIMITS
 - 12147 CFS **Q100 FLOW**
 - CCON10 **HEC-1 CONCENTRATION POINT**
 -  **FLOW DIRECTION**
 - MAIN1** **HEC-RAS REACH**
 - 2200 **HEC-RAS STATION LABEL**
 -  **HEC-RAS CROSS SECTION**

MAIN 1 HEC-RAS STATION SUMMARY TABLE								
Sta	Q (cfs)	Fl. Elevation (ft)	W.S. Elevation (ft)	Depth (ft)	Vel (ft/s)	Top Width (ft)	Froude #	Notes
2700	2128	2756.00	2760.90	4.90	10.45	60.71	1.01	Existing Wash
2600	2128	2752.00	2758.31	6.31	9.89	71.49	1.00	Existing Wash
2500	2128	2748.00	2754.39	6.39	10.14	66.45	1.01	Existing Wash
2400	2128	2738.36	2752.49	13.13	3.16	90.29	0.20	Proposed 20x9 RCP

MAIN 2 HE-CRAN STATION SUMMARY TABLE								
Sta	Q (cfs)	FL Elevation (ft)	W.S. Elevation (ft)	Depth (ft)	Vel (ft/s)	Top Width (ft)	Froude #	Notes
5400	1910	2780.00	2783.62	3.62	9.02	85.32	1.01	Existing Wash
5300	1910	2778.00	2781.81	3.81	10.53	65.56	1.13	Existing Wash
5200	1910	2772.00	2774.34	2.34	18.71	54.29	2.40	Existing Wash
5100	1910	2764.00	2771.06	7.06	3.44	129.63	0.29	Existing Wash
5000	1910	2759.39	2771.09	11.70	2.48	127.62	0.18	Proposed 20x9 RC

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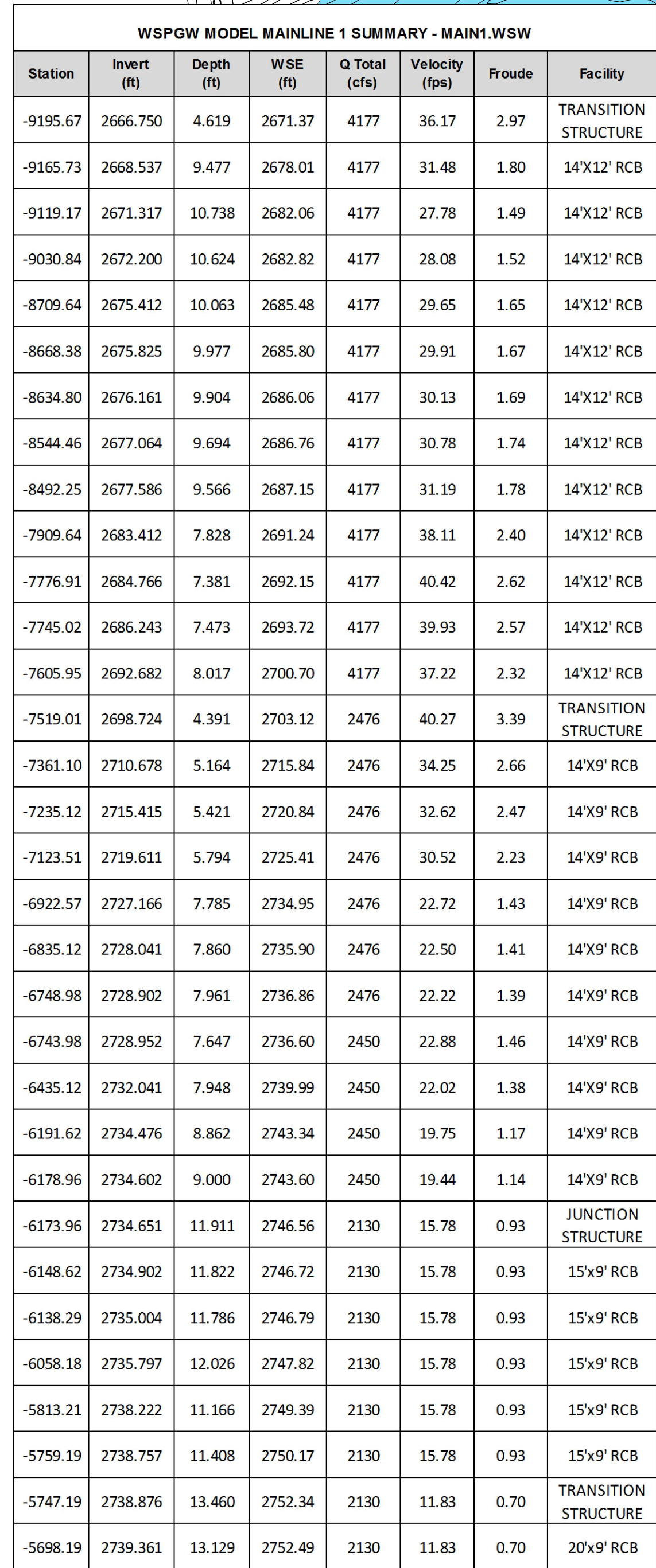
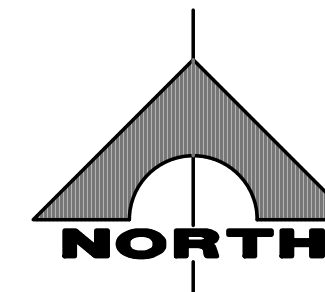
PROPOSED CONDITIONS REC-PAS X-SECTION MAP

GCV
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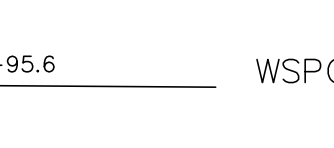
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F: 702.804.2299
gcwengineering.com

[illegible]

DRAWING
FIG10
OF SH



MAIN 1 HEC-RAS STATION SUMMARY TABLE								
Sta	Q (cfs)	R. Elevation (ft)	W.S. Elevation (ft)	Depth (ft)	Vel (ft/s)	Top Width (ft)	Froude #	Notes
2700	2128	2756.00	2760.90	4.90	10.45	60.71	1.01	Existing Wash
2600	2128	2752.00	2758.31	6.31	9.89	71.49	1.01	Existing Wash
2500	2128	2748.00	2754.39	6.39	10.14	66.45	1.01	Existing Wash
2400	2128	2739.36	2752.49	13.13	3.16	90.29	0.20	Proposed 20x9 RCB









-  HEC-RAS RIVER STATION
-  WSPGW STATION
-  ZONE A SFHA FLOODPLAIN
-  REMOVED FROM SFHA FLOODPLAIN
-  WSPGW FLOWLINE
-  HEC-RAS FLOWLINE

TABLE 8		
EFFECTIVE FLOW RATES – MAIN 1 WASH AND RCB		
HEC-RAS River Station*	WSPGW Station**	Effective Flow Rate (cfs)
2700	-	2,128
-	-5698.19	2,132
-	-6194.12	2,452
-	-6702.00	2,478
-	-7588.63	4,179

*See Figure 10.

**See Figure 11.

Hydraulic Modeling

Hydraulic modeling for the proposed channel improvements were performed within the U.S. Army Corps of Engineers HEC-RAS River Analysis System computer program version 4.1.0 (Reference 9). The HEC-RAS model outputs have been provided in Appendix B. Electronic copies of the models have been included on CD.

Existing Condition

The limits of the hydraulic modeling of Main 1 begins approximately 700 feet upstream of the western property line at Station 2700 and extend approximately 3,900 linear feet, east through an unnamed wash through an existing golf course, and terminating at the existing dual (2) - 12-foot wide by 12-foot high RCBCs at the intersection of Rampart Boulevard and Alta Drive at Station 200. This project re-evaluates the existing hydraulic analysis of the unnamed wash. The base cross section geometry used in the hydraulic modeling was determined from existing topography with 1-foot contour intervals. A “sub-critical” flow regime was analyzed for the wash. The starting water surface elevation of 2684.83 feet at Station 200 was determined based on a culvert inlet control calculation at the existing dual (2) - 12-foot wide by 12-foot high RCBCs at the intersection of Rampart Boulevard and Alta Drive ($WSE = \text{Invert of pipe} + \text{headwater depth} = 2666.75 \text{ feet} + 18.08 \text{ feet} = 2684.83 \text{ feet}$). A copy of the inlet control calculation has been included in Appendix B.

Proposed Condition

The proposed improvements along the unnamed wash extend between Main 1 Stations 200 and 2400. The improvements consist of reinforced concrete box storm drain through the length of the project and tie into the existing dual (2) - 12-foot wide by 12-foot high RCB at the intersection of Rampart Boulevard and Alta Drive.

HEC-RAS was utilized for open channel and wash portions of the analysis. WSPGW was utilized to evaluate the water surface profile through proposed storm drain. The WSPGW computer program was selected to evaluate the storm sewer system in lieu of HEC-RAS due to its more relevant modeling approach for storm drain systems. Supporting WSPGW hydraulic models are included in Appendix B.

The resulting comparison between existing and proposed condition water surface elevations through the project are summarized in Table 9.

TABLE 9 MAIN 1 WASH - WATER SURFACE ELEVATION COMPARISON TABLE							
Existing Condition				Proposed Condition			
Sta*	Q (cfs)	FL Elevation (ft)	W.S. Elevation (ft)	Q (cfs)	FL Elevation (ft)	W.S. Elevation (ft)	Rise in Water Surface Elevation Due to Development (ft)
2700	2,128	2756.00	2760.89	2,128	2756.00	2760.90	0.01
2600	2,128	2752.00	2758.31	2,128	2752.00	2758.31	0.00
2500	2,128	2748.00	2754.37	2,128	2748.00	2754.39	0.02
2400	2,128	2747.00	2751.80	2,128	2739.36	2752.49	0.69
2300	2,128	2744.00	2749.36	1% Annual Chance Flood Discharge Contained in Storm Drain			
2200	2,128	2740.00	2745.49				
2100	2,128	2736.00	2742.08				
2000	2,128	2729.00	2735.65				
1900	2,128	2724.00	2733.14				
1800	2,128	2719.00	2732.45				
1700	2,227	2716.00	2728.08				
1600	2,227	2711.00	2725.34				
1500	2,472	2707.00	2720.77				
1400	2,472	2702.00	2713.84				
1300	2,472	2699.00	2704.43				
1200	2,472	2695.00	2700.84				
1100	2,472	2691.00	2697.30				
1000	2,472	2687.00	2692.52				
900	2,472	2683.00	2689.15				
800	2,493	2679.00	2685.65				
700	2,493	2676.00	2685.62				
600	2,493	2674.00	2685.89				

TABLE 9 MAIN 1 WASH - WATER SURFACE ELEVATION COMPARISON TABLE							
Existing Condition				Proposed Condition			
Sta*	Q (cfs)	FL Elevation (ft)	W.S. Elevation (ft)	Q (cfs)	FL Elevation (ft)	W.S. Elevation (ft)	Rise in Water Surface Elevation Due to Development (ft)
500	4,209	2672.00	2685.74				
400	4,209	2671.00	2685.77				
300	4,209	2669.00	2685.77				
200	4,209	2668.00	2684.83				

*See Figures 9 and 10.

As shown in the table, the proposed improvements tie into the existing water surface elevation at the upstream end and tie into the existing storm drain facility at the downstream end that contains the 1% chance annual flood. The proposed water surface elevations do not exceed the existing water surface elevations by more than 1-foot, or are entirely contained within the proposed storm drain facility.

Mapping

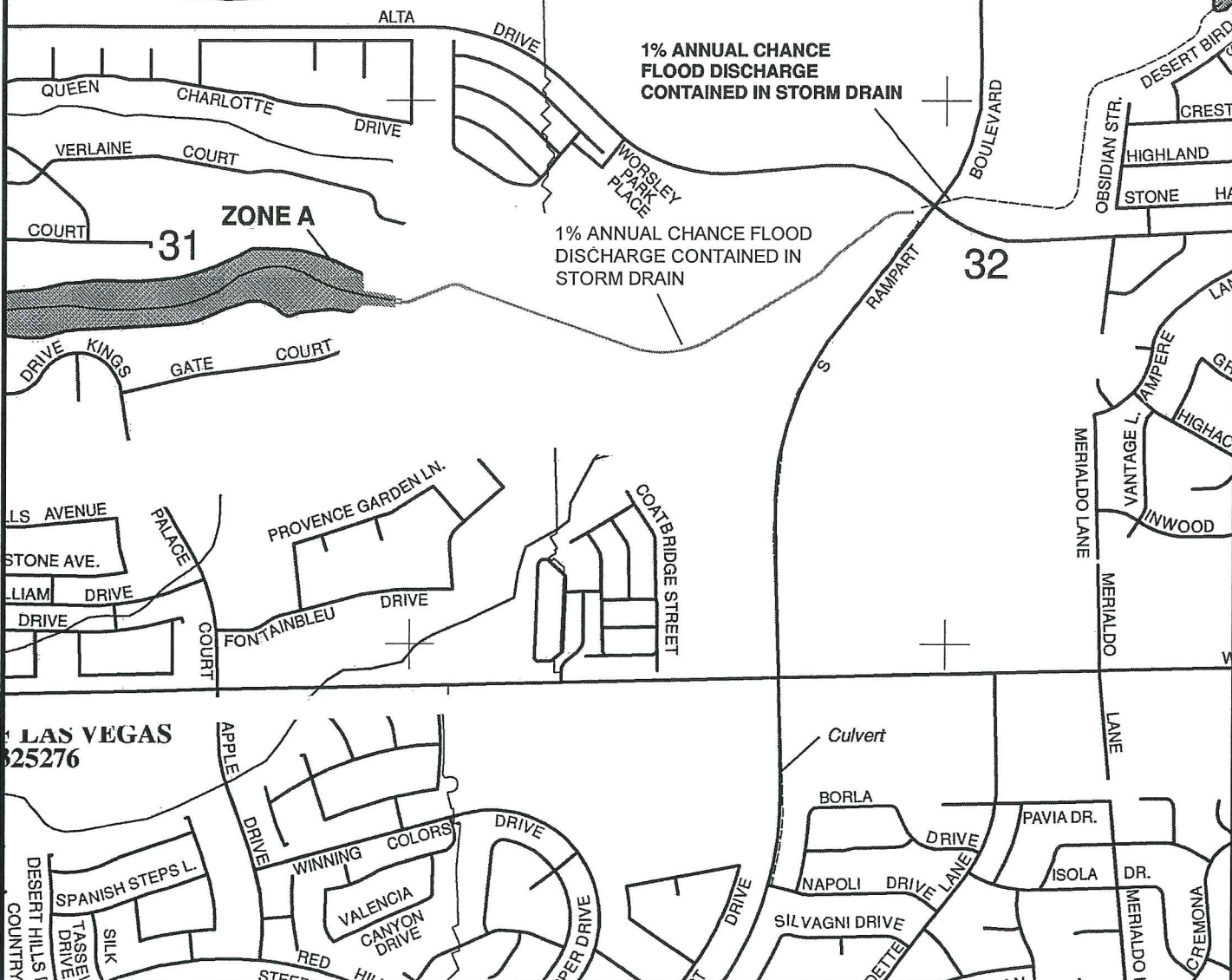
The Effective FIRM is shown on Figure 3. The proposed revisions to the Effective FIRM take into account the proposed improvements along the unnamed wash and within the project. The improvements affect the Zone A area.

The upstream tie-in to the Effective FIRM Zone A is located at Station 2700. The upstream tie-in was based on a smooth transition from the proposed floodplain width to the effective floodplain width. The downstream tie-in to the Effective FIRM Zone A is located at the existing dual (2) - 12-foot wide by 12-foot high RCBCs at the intersection of Rampart Boulevard and Alta Drive at Station 200 where the 1% annual chance flood discharge is contained in storm drain downstream of the project site. The proposed FIRM revisions and tie-in locations are shown on Figure 11 - CLOMR Workmap and Figure 12 - Annotated FIRM.

In general, the proposed site grading and storm drain improvements are in conformance with existing drainage patterns and flow values presented in the 2013 MPU and Queens Borough Culvert Study. Therefore, the proposed project will not adversely impact any downstream properties or facilities.

CITY OF LAS VEGAS
325276

HOWN ON THIS PANEL IS LOCATED
20 SOUTH, RANGE 60 EAST AND
TH, RANGE 60 EAST.



CITY OF LAS VEGAS
325276

MAP SCALE 1" = 1000'
0 500 1000 FEET
0 500 1000 METERS

PANEL 2145F

FIRM

FLOOD INSURANCE RATE MAP
CLARK COUNTY,
NEVADA
AND INCORPORATED AREAS

PANEL 2145 OF 4090

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

COMMUNITY	NUMBER	PANEL	SUFFIX
CLARK COUNTY	32003	2145	F
LAS VEGAS, CITY OF	325276	2145	F

Notes to User: The Map Number shown below should be used when placing map orders. The Community Number shown above should be used on insurance applications for the subject community.



MAP NUMBER

32003C2145F

MAP REVISED

NOVEMBER 16, 2011

Federal Emergency Management Agency

GRAPHIC SCALE



(IN FEET)

1 inch = 1000 ft.



THE SEVENTY
SEVENTY ACRES LLC, FORE STARS
LTD, AND 180 LAND CO LLC

FIGURE 12

ANNOTATED F.I.R.M.



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XI. CONCLUSIONS AND RECOMMENDATIONS

1. Methodology used in this report is in compliance with Clark County Regional Flood Control District (CCRFCD) criteria.
2. The project site is located within a FEMA-designated Special Flood Hazard Area (SFHA) Zone A. However, the 100-year flow (1% annual chance flood discharge) is contained within the proposed RCBs (Mainline 1 and Mainline 2) that transverse the site. Since the flows will be contained within the proposed RCBs, a CLOMR will be obtained from FEMA and a LOMR will be obtained from FEMA once construction of the facilities are substantially complete and functional.
3. CCRFCD Facilities to be constructed with this project include: APSO 0050, APSO 0067 and APP2 0000.
4. The proposed improvements connect to existing CCRFCD Facility APSO 0020.
5. Recommended storm drain facilities proposed with the project are shown on the attached grading plans.
6. The proposed storm drain will vary in size ranging from 18-inch RCP to 72-inch RCP and 10-foot wide by 8-foot high RCB to 14-foot wide by 12-foot high RCB connecting to the existing Rampart Boulevard dual (2) – 12-foot wide by 12-foot high RCB culverts.
7. Methods used to calculate storm runoff and size facilities are in compliance with the Manual.
8. Proposed facilities have been sized based on proposed conditions flow rates.
9. Detailed hydraulic modeling of the proposed Mainline 1 and Mainline 2 from the western boundary of the project site to the existing culverts in Rampart Boulevard shows that the design flows will be contained within the proposed RCBs. The design flows are based on the Proposed Conditions HEC-1 Model flow of 4,673 cfs. The proposed RCB will convey the Proposed Conditions flow with freeboard.
10. Flows conveyed within the onsite Mainline 1 RCB will be discharged into the existing dual (2) – 12-foot wide by 12-foot high RCBs in Rampart Boulevard located at the northeast corner of the project site.

11. Onsite storm drain laterals have been provided as part of this package to provide for future development of The Seventy and The Two Fifty.
12. Proposed onsite ditches/berms will convey onsite flows to be collected and conveyed by the proposed storm drain laterals.
13. Onsite area drains will be connected to the proposed onsite storm drain system that connects into the dual (2) - 12-foot wide by 12-foot high RCBCs.
14. All future onsite finished floors will be designed as required by CLV Criteria.
15. The emergency overflow path for the project will be Rampart Boulevard.
16. The general drainage patterns and flow rates are in general agreement with those specified in the 2013 MPU and the previous Queens Borough Culvert Study.
17. Runoff generated from, or conveyed by, the project will not adversely impact any downstream properties and facilities.

XII. REFERENCES

1. G. C. Wallace, *Technical Drainage Study for Queens Borough Culvert*, August 2005.
2. G. C. Wallace, *Update to the Technical Drainage Study for Queens Borough Culvert*, December 2005.
3. G. C. Wallace, *Update #2 to the Technical Drainage Study for Queens Borough Culvert*, April 2006.
4. *CCRFCD 2013 Las Vegas Valley Flood Control Master Plan Update*, 2013.
5. Clark County Regional Flood Control District (CCRFCD) *Hydrologic Criteria and Drainage Design Manual*. August 1999.
6. U.S. Army Corps of Engineers, *HEC-1 Flood Hydrograph Package*. June 1998.
7. U. S. Department of Agriculture & National Resource Conservation Service, *Soil Survey of Las Vegas Valley Area, Nevada, Part of Clark County*. August 2014. Version 10.
8. U. S. Army Corps of Engineers, *WSPGW Water Surface Pressure Gradient Package*. Version 12.99. 1991-2000.
9. U.S. Army Corps of Engineers, *HEC-RAS River Analysis System*. January 2010. Version 4.1.0.

THE SEVENTY APPENDIX LAYOUT

Appendix A. Hydrologic Calculations and Information

1. Figure 513 – McCarran Airport Rainfall Area
2. Figure 506 – Rainfall Depth-Duration-Frequency 100-Year, 6-Hour
3. Figure 503 – Rainfall Depth-Duration-Frequency 10-Year, 6-Hour
4. Table 501 – Precipitation Adjustment Ratios
5. Rainfall Exhibits
6. Custom Soils Resource Report
7. Table 602 – 1 of 4 from the CCRFCD Manual
8. Table 602A
9. Revised 2013 MPU Curve Number Matrix
10. Composite Curve Number Calculations
11. Land Plan Exhibit
12. Existing Conditions Standard Form 4
13. Existing Conditions HEC-1 Model
14. Proposed Conditions Standard Form 4
15. Proposed Conditions HEC-1 Model
16. Exhibit A

Appendix B. Hydraulic Calculations and Information

1. Rough Grade Ditch Calculations
2. Conceptual Storm Drain Normal Depth Calculations
3. WSPGW
 - a. Queens Borough Culvert to Main 1 WSPGW Station Conversion
 - b. Mainline 1
 - c. Mainline 1 Laterals
 - d. Mainline 2
 - e. Mainline 2 Laterals
4. HEC-RAS
 - a. Existing Conditions
 - i. Main 1
 - ii. Main 2
 - b. Proposed Conditions
 - i. Main 1
 - ii. Main 2
5. Area Drain Calculation
6. Inlet Control Calculations
7. D-Load Calculations

Appendix C. Referenced Material (On CD)

1. Referenced Studies and Grading Plans Received From CLV
2. Technical Drainage Study for Queens Borough Culvert Update 2 Supplement
 - a. City of Las Vegas Approval Letter
 - b. Supplement Letter
 - c. WSPGW Model
 - d. Improvement Plans
3. 2013 Las Vegas Valley Flood Control Master Plan Update
 - a. ALLGOW3 HEC-1 Model Excerpt

**THE SEVENTY
APPENDIX LAYOUT**

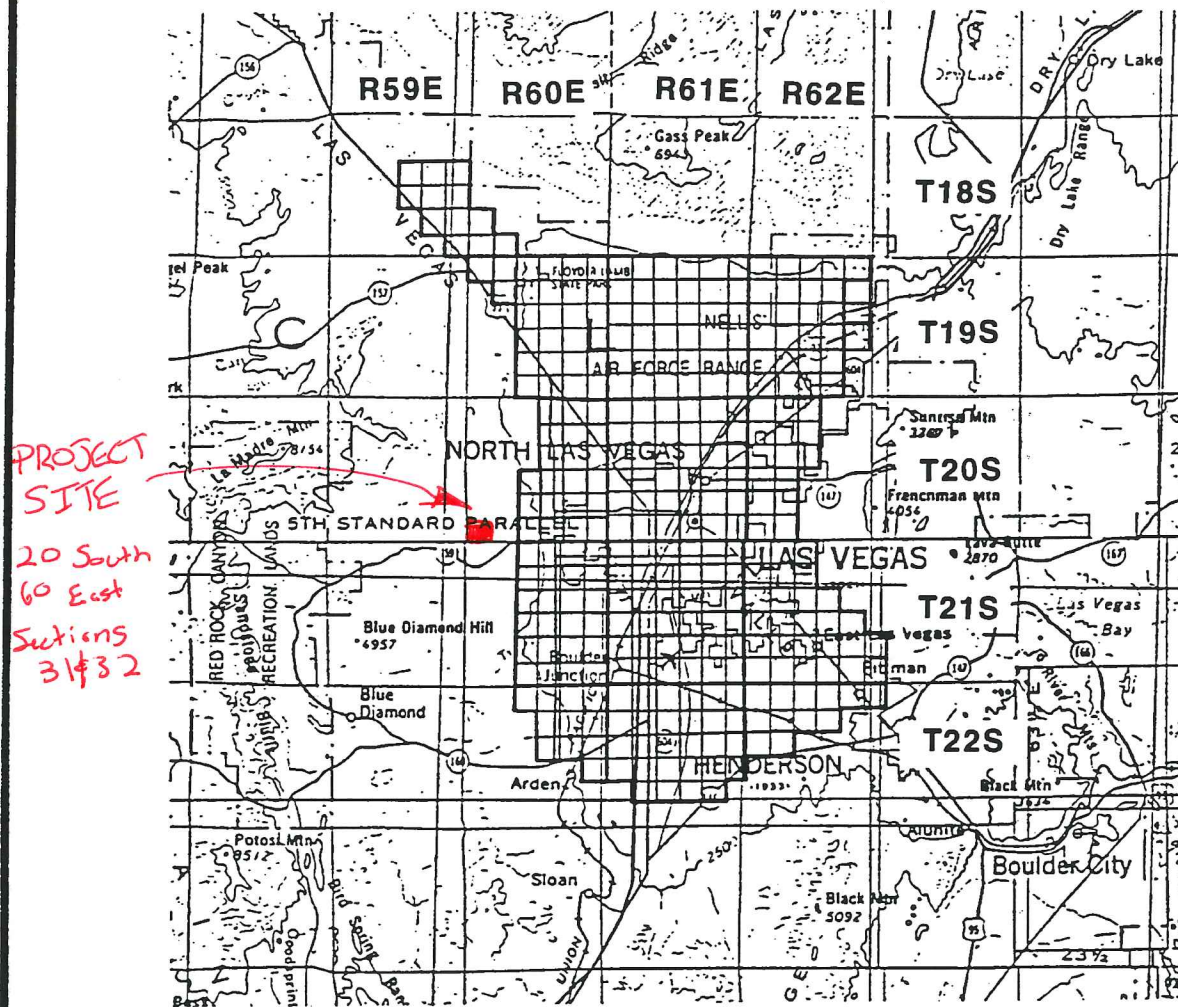
- b. Figure H-29
- c. Figure H-30
- 4. LOMR Case No. 06-09-BF86P
- 5. LOMR Case No. 06-09-B483P
- 6. Improvement Plans from One Queensridge Place (Sheet C10.03)
- 7. Improvement Plans from Rampart Boulevard (Sheet SD-5)

APPENDIX A

Hydrologic Information

HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

McCARRAN AIRPORT RAINFALL AREA



TOWNSHIP	RANGE	SECTIONS	TOWNSHIP	RANGE	SECTIONS
18 South	59 East	13-15,22-26,36	20 South	62 East	4-9,16-20,29-32
18 South	60 East	30-32	21 South	60 East	1-4,9-16,21-28,33-36
19 South	60 East	1-6,8-16,21-28,33-36	21 South	61 East	ALL SECTIONS
19 South	61 East	ALL SECTIONS	21 South	62 East	4-9,15-23, 25-36
19 South	62 East	2-11,14-23,27-34	22 South	60 East	1-4,10-15,24
20 South	60 East	1-3,10-15,21-28,33-36	22 South	61 East	1-24,26-29
20 South	61 East	ALL SECTIONS	22 South	62 East	1-10,17-18

Notes:

1. Refer to Table 505 and Figure 516 Depth-Duration-Frequency values in the McCarran Airport Rainfall Area.
2. Refer to Table 506 and Figure 517 for Time-Intensity-Frequency values on the McCarran Airport Rainfall Area.

Revision	Date

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ENGINEERING**

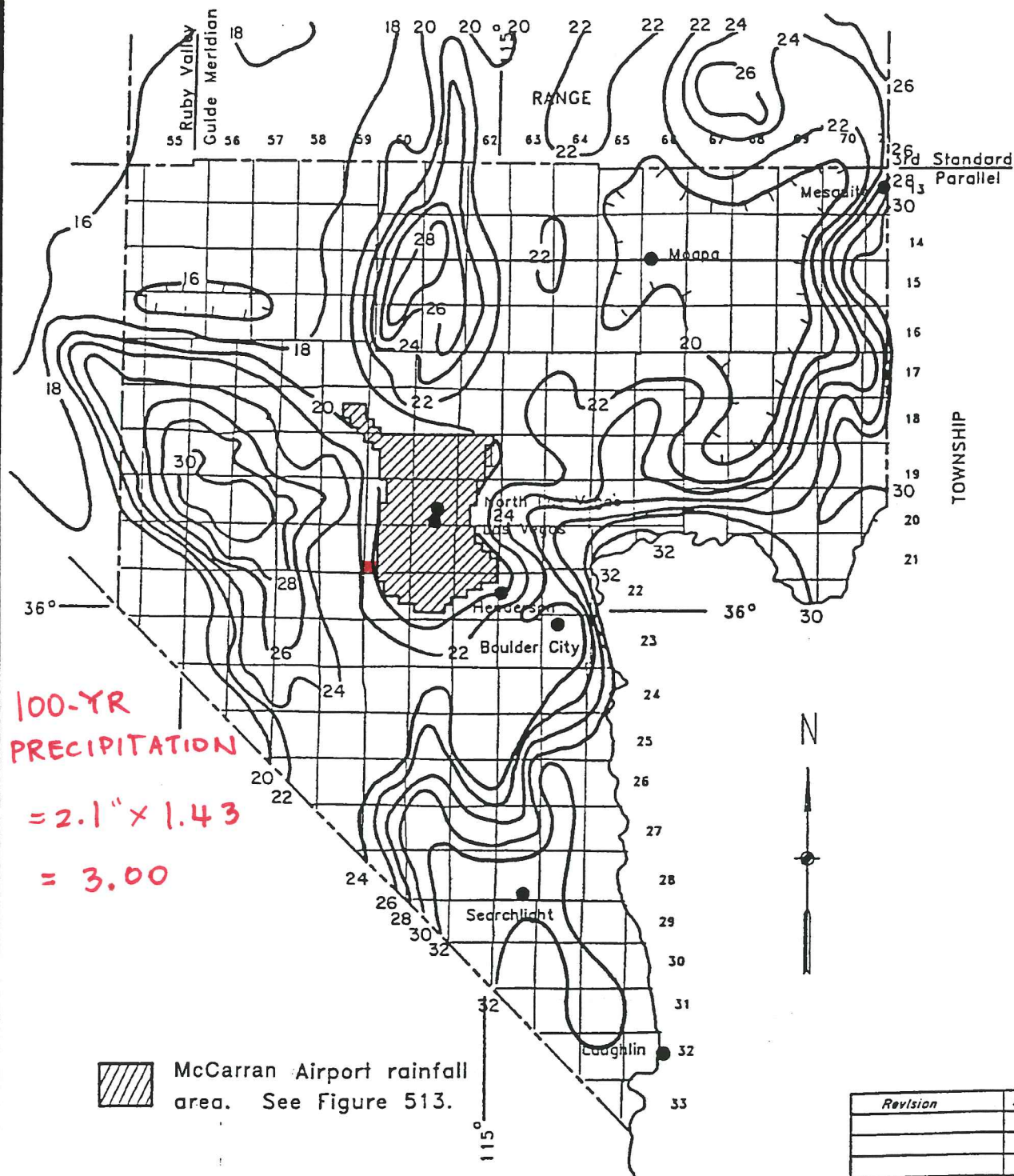
REFERENCE:

USACE, Los Angeles District, 1988

FIGURE 513

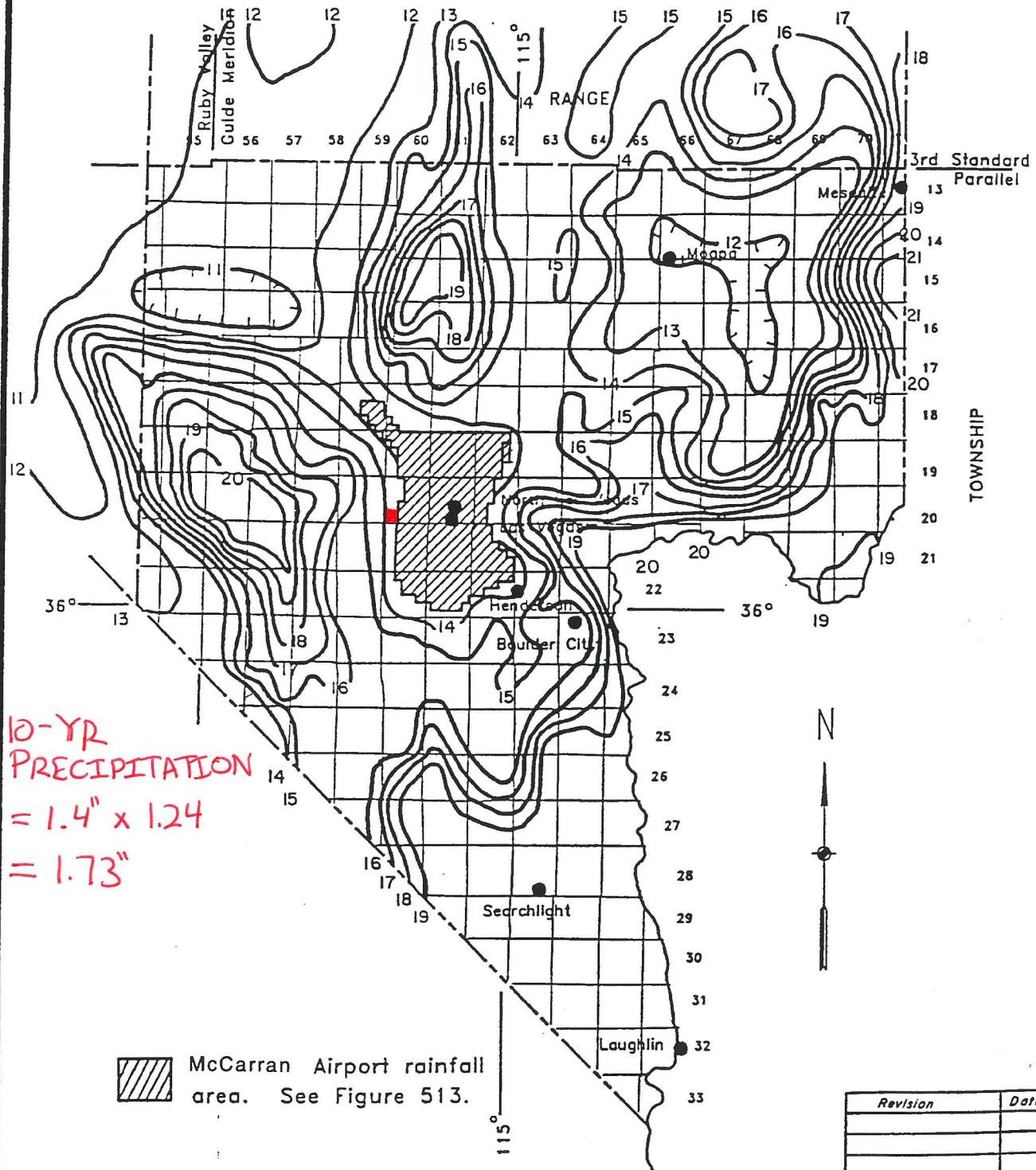
HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

RAINFALL DEPTH-DURATION-FREQUENCY 100-YEAR, 6-HOUR (DEPTHS IN TENTHS OF INCHES)



HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

RAINFALL DEPTH-DURATION-FREQUENCY 10-YEAR, 6-HOUR (DEPTHS IN TENTHS OF INCHES)



HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

PRECIPITATION ADJUSTMENT RATIOS

<u>Recurrence Interval</u>	<u>Ratio to NOAA Atlas 2</u>
2-year	1.00
5-year	1.16
10-year	1.24 $\times 1.4 = 1.73$
25-year	1.33
50-year	1.39
100-year	1.43 $\times 2.1 = 3.00$

$$\frac{1.73}{3.00} = 0.57$$

- NOTE: 1. Multiply the values obtained from the NOAA Atlas 2 by the above ratios to obtain the adjusted precipitation values.
2. NOAA Atlas 2 values for use with TR-55 shall not be adjusted by the above ratios.
3. Tables 505 and 506 require no adjustments.

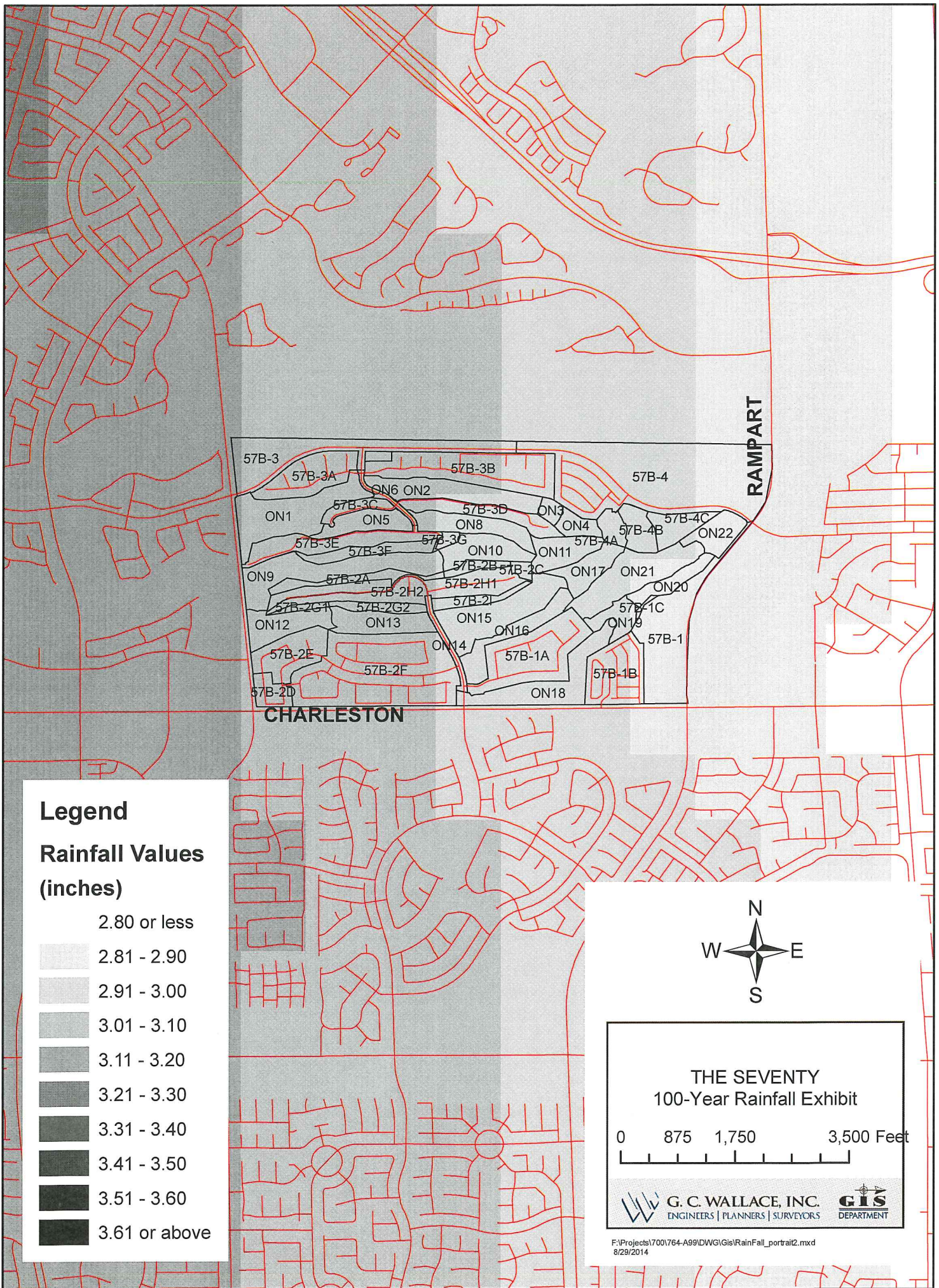
Revision	Date

**WRC
ENGINEERING**

REFERENCE:

USACE, Los Angeles District, 1988

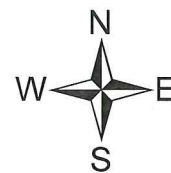
TABLE 501



Legend

Rainfall Values (inches)

	2.80 or less
	2.81 - 2.90
	2.91 - 3.00
	3.01 - 3.10
	3.11 - 3.20
	3.21 - 3.30
	3.31 - 3.40
	3.41 - 3.50
	3.51 - 3.60
	3.61 or above



THE SEVENTY 100-Year Rainfall Exhibit

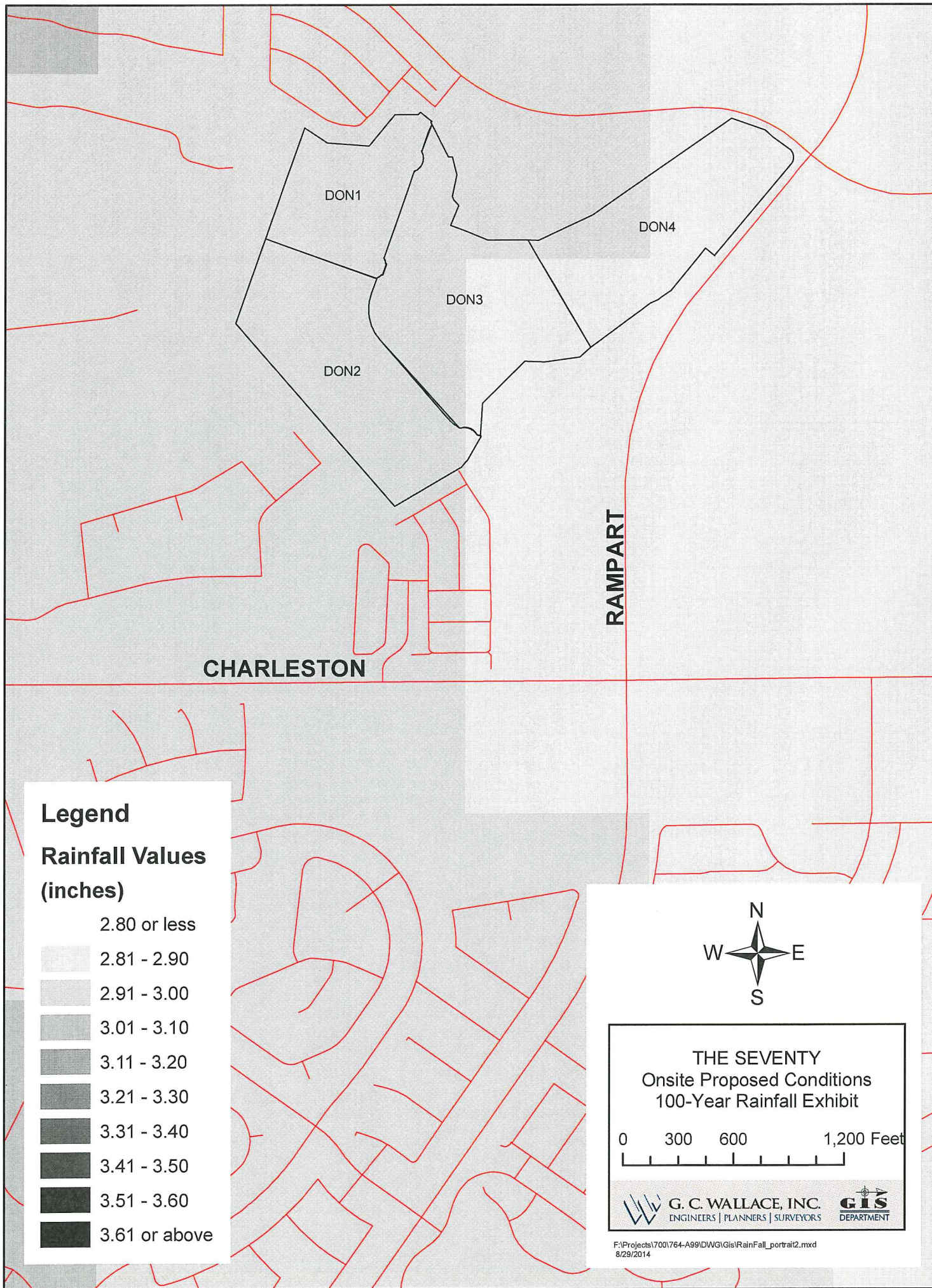
0 875 1,750 3,500 Feet



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8/29/2014





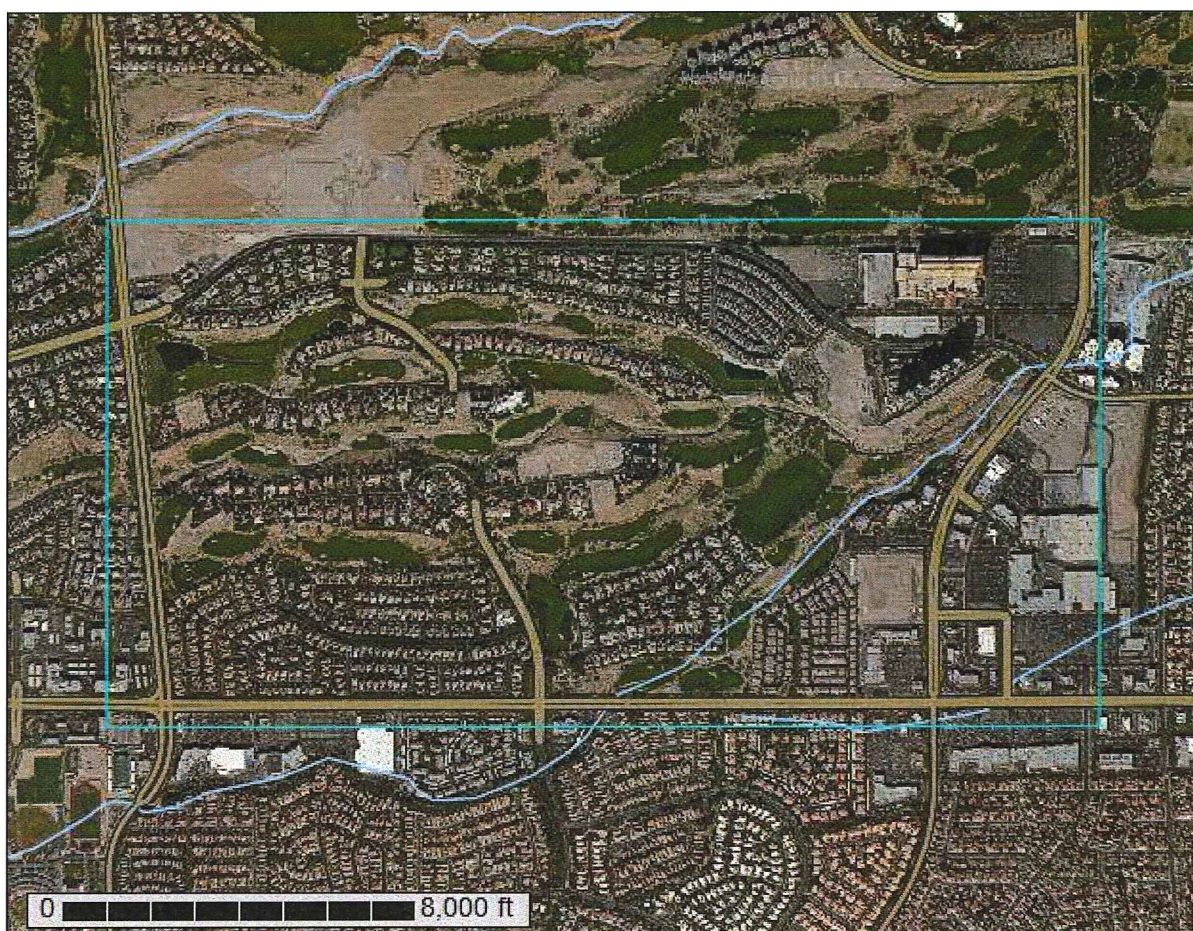
United States
Department of
Agriculture

NRCS

Natural
Resources
Conservation
Service

A product of the National
Cooperative Soil Survey,
a joint effort of the United
States Department of
Agriculture and other
Federal agencies, State
agencies including the
Agricultural Experiment
Stations, and local
participants

Custom Soil Resource Report for Las Vegas Valley Area, Nevada, Part of Clark County



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (<http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/>) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (<http://offices.sc.egov.usda.gov/locator/app?agency=nrcs>) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil scientists classified and named the soils in the survey area, they compared the

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individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.







Custom Soil Resource Report Soil Map



Map Scale: 1:14,500 if printed on A landscape (11" x 8.5") sheet.

Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 11N WGS84

MAP LEGEND

Area of Interest (AOI)		Water Features	
	Area of Interest (AOI)		Streams and Canals
Soils		Transportation	
	Soil Map Unit Polygons		Rails
	Soil Map Unit Lines		Interstate Highways
	Soil Map Unit Points		US Routes
Special Point Features			Major Roads
	Blowout		Local Roads
	Borrow Pit	Background	
	Clay Spot		Aerial Photography
	Closed Depression		
	Gravel Pit		
	Gravelly Spot		
	Landfill		
	Lava Flow		
	Marsh or swamp		
	Mine or Quarry		
	Miscellaneous Water		
	Perennial Water		
	Rock Outcrop		
	Saline Spot		
	Sandy Spot		
	Severely Eroded Spot		
	Sinkhole		
	Slide or Slip		
	Sodic Spot		

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL: <http://websoilsurvey.nrcs.usda.gov>
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Las Vegas Valley Area, Nevada, Part of Clark County
Survey Area Data: Version 10, Aug 22, 2014

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: May 7, 2011—Feb 25, 2014

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Las Vegas Valley Area, Nevada, Part of Clark County (NV788)			
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
152	Cave gravelly fine sandy loam, 0 to 4 percent slopes	867.7	100.0%
Totals for Area of Interest		867.7	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

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An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Las Vegas Valley Area, Nevada, Part of Clark County

152—Cave gravelly fine sandy loam, 0 to 4 percent slopes

Map Unit Setting

National map unit symbol: hr9v
Elevation: 2,000 to 4,800 feet
Mean annual precipitation: 4 to 12 inches
Mean annual air temperature: 57 to 70 degrees F
Frost-free period: 180 to 280 days
Farmland classification: Not prime farmland

Map Unit Composition

Cave and similar soils: 100 percent
Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Cave

Setting

Landform: Fan remnants
Down-slope shape: Linear
Across-slope shape: Convex
Parent material: Mixed alluvium

Typical profile

H1 - 0 to 12 inches: gravelly fine sandy loam
H2 - 12 to 36 inches: indurated
H3 - 36 to 60 inches: very gravelly sandy loam

Properties and qualities

Slope: 0 to 4 percent
Depth to restrictive feature: 4 to 20 inches to petrocalcic
Natural drainage class: Well drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 40 percent
Gypsum, maximum in profile: 5 percent
Salinity, maximum in profile: Nonsaline to slightly saline (0.0 to 4.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 12.0
Available water storage in profile: Very low (about 1.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7s
Hydrologic Soil Group: D
Other vegetative classification: LIMY 3-5" P.Z. (030XB019NV_3)

Soil Information for All Uses

Soil Reports

The Soil Reports section includes various formatted tabular and narrative reports (tables) containing data for each selected soil map unit and each component of each unit. No aggregation of data has occurred as is done in reports in the Soil Properties and Qualities and Suitabilities and Limitations sections.

The reports contain soil interpretive information as well as basic soil properties and qualities. A description of each report (table) is included.

Soil Physical Properties

This folder contains a collection of tabular reports that present soil physical properties. The reports (tables) include all selected map units and components for each map unit. Soil physical properties are measured or inferred from direct observations in the field or laboratory. Examples of soil physical properties include percent clay, organic matter, saturated hydraulic conductivity, available water capacity, and bulk density.

Engineering Properties (Badlands)

This table gives the engineering classifications and the range of engineering properties for the layers of each soil in the survey area.

Hydrologic soil group is a group of soils having similar runoff potential under similar storm and cover conditions. The criteria for determining Hydrologic soil group is found in the National Engineering Handbook, Chapter 7 issued May 2007(<http://directives.sc.egov.usda.gov/OpenNonWebContent.aspx?content=17757.wba>).

Listing HSGs by soil map unit component and not by soil series is a new concept for the engineers. Past engineering references contained lists of HSGs by soil series. Soil series are continually being defined and redefined, and the list of soil series names changes so frequently as to make the task of maintaining a single national list virtually impossible. Therefore, the criteria is now used to calculate the HSG using the component soil properties and no such national series lists will be maintained. All such references are obsolete and their use should be discontinued. Soil properties that influence runoff potential are those that influence the minimum rate of infiltration for a bare soil after prolonged wetting and when not frozen. These properties are depth to a seasonal high water table, saturated hydraulic conductivity after prolonged wetting, and depth to a layer with a very slow water transmission rate. Changes in soil properties caused by land management or climate changes also cause the hydrologic

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soil group to change. The influence of ground cover is treated independently. There are four hydrologic soil groups, A, B, C, and D, and three dual groups, A/D, B/D, and C/D. In the dual groups, the first letter is for drained areas and the second letter is for undrained areas.

The four hydrologic soil groups are described in the following paragraphs:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

Depth to the upper and lower boundaries of each layer is indicated.

Texture is given in the standard terms used by the U.S. Department of Agriculture. These terms are defined according to percentages of sand, silt, and clay in the fraction of the soil that is less than 2 millimeters in diameter. "Loam," for example, is soil that is 7 to 27 percent clay, 28 to 50 percent silt, and less than 52 percent sand. If the content of particles coarser than sand is 15 percent or more, an appropriate modifier is added, for example, "gravelly."

Classification of the soils is determined according to the Unified soil classification system (ASTM, 2005) and the system adopted by the American Association of State Highway and Transportation Officials (AASHTO, 2004).

The Unified system classifies soils according to properties that affect their use as construction material. Soils are classified according to particle-size distribution of the fraction less than 3 inches in diameter and according to plasticity index, liquid limit, and organic matter content. Sandy and gravelly soils are identified as GW, GP, GM, GC, SW, SP, SM, and SC; silty and clayey soils as ML, CL, OL, MH, CH, and OH; and highly organic soils as PT. Soils exhibiting engineering properties of two groups can have a dual classification, for example, CL-ML.

The AASHTO system classifies soils according to those properties that affect roadway construction and maintenance. In this system, the fraction of a mineral soil that is less than 3 inches in diameter is classified in one of seven groups from A-1 through A-7 on the basis of particle-size distribution, liquid limit, and plasticity index. Soils in group A-1 are coarse grained and low in content of fines (silt and clay). At the other extreme, soils in group A-7 are fine grained. Highly organic soils are classified in group A-8 on the basis of visual inspection.

If laboratory data are available, the A-1, A-2, and A-7 groups are further classified as A-1-a, A-1-b, A-2-4, A-2-5, A-2-6, A-2-7, A-7-5, or A-7-6. As an additional refinement, the suitability of a soil as subgrade material can be indicated by a group index number.

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Group index numbers range from 0 for the best subgrade material to 20 or higher for the poorest.

Rock fragments larger than 10 inches in diameter and 3 to 10 inches in diameter are indicated as a percentage of the total soil on a dry-weight basis. The percentages are estimates determined mainly by converting volume percentage in the field to weight percentage.

Percentage (of soil particles) passing designated sieves is the percentage of the soil fraction less than 3 inches in diameter based on an oven-dry weight. The sieves, numbers 4, 10, 40, and 200 (USA Standard Series), have openings of 4.76, 2.00, 0.420, and 0.074 millimeters, respectively. Estimates are based on laboratory tests of soils sampled in the survey area and in nearby areas and on estimates made in the field.

Liquid limit and *plasticity index* (Atterberg limits) indicate the plasticity characteristics of a soil. The estimates are based on test data from the survey area or from nearby areas and on field examination.

References:

American Association of State Highway and Transportation Officials (AASHTO). 2004. Standard specifications for transportation materials and methods of sampling and testing. 24th edition.

American Society for Testing and Materials (ASTM). 2005. Standard classification of soils for engineering purposes. ASTM Standard D2487-00.

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Absence of an entry indicates that the data were not estimated. The asterisk '*' denotes the representative texture; other possible textures follow the dash. The criteria for determining the hydrologic soil group for individual soil components is found in the National Engineering Handbook, Chapter 7 issued May 2007(<http://directives.sc.egov.usda.gov/OpenNonWebContent.aspx?content=17757.wba>).

Engineering Properties—Las Vegas Valley Area, Nevada, Part of Clark County														
Map unit symbol and soil name	Pct. of map unit	Hydrologic group	Depth	USDA texture	Classification		Fragments		Percentage passing sieve number—				Liquid limit	Plasticity index
					Unified	AASHTO	>10 inches	3-10 inches	4	10	40	200		
			<i>In</i>				<i>Pct</i>	<i>Pct</i>					<i>Pct</i>	
152—Cave gravely fine sandy loam, 0 to 4 percent slopes														
Cave	100 D		0-12	Gravelly fine sandy loam	SC-SM, SM	A-2, A-4	0-0-0	0-3-5	70-80-90	60-68-75	40-53-65	25-33-40	15-20-25	NP-3-5
			12-36	Indurated	—	—	—	—	—	—	—	—	—	—
			36-60	Gravelly loamy sand, very gravelly sandy loam	GM, GP-GM, SM, SP-SM	A-1, A-2	0-0-0	0-3-5	35-55-75	30-45-60	20-28-35	10-20-30	0-8-15	NP

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HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

RUNOFF CURVE NUMBERS (URBAN AREAS¹)

Cover description		Curve numbers for hydrologic soil group—			
Cover type and hydrologic condition	Average percent impervious area ²	A	B	C	D
<i>Fully developed urban areas (vegetation established)</i>					
Open space (lawns, parks, golf courses, cemeteries, etc.) ³ :					
Poor condition (grass cover < 50%)		68	79	86	89
Fair condition (grass cover 50% to 75%)		49	69	79	84
Good condition (grass cover > 75%)		39	61	74	80
Impervious areas:					
Paved parking lots, roofs, driveways, etc. (excluding right-of-way)		98	98	98	98
Streets and roads:					
Paved; curbs and storm sewers (excluding right-of-way)		98	98	98	98
Paved; open ditches (including right-of-way)		83	89	92	93
Gravel (including right-of-way)		76	85	89	91
Dirt (including right-of-way)		72	82	87	89
Western desert urban areas:					
Natural desert landscaping (pervious areas only) ⁴ ...		63	77	85	88
Artificial desert landscaping (impervious weed barrier, desert shrub with 1- to 2-inch sand or gravel mulch and basin borders)		96	96	96	96
Urban districts:					
Commercial and business	85	89	92	94	95
Industrial	72	81	88	91	93
Residential districts by average lot size:					

See Table 602A

Developing urban areas

Newly graded areas (pervious areas only, no vegetation) ⁵	77	86	91	94
--	----	----	----	----

1 Average runoff condition, and $I_p = 0.2S$.

2 The average percent impervious area shown was used to develop the composite CN's. Other assumptions are as follows: impervious areas are directly connected to the drainage system. Impervious areas have a CN of 98, and pervious areas are considered equivalent to open space in good hydrologic condition. CN's for other combinations of conditions may be computed using Figure 603.

3 CN's shown are equivalent to those of pasture. Composite CN's may be computed for other combinations of open space cover type.

4 Composite CN's for natural desert landscaping should be computed using Figure 603 based on the impervious area percentage (CN #98) and the pervious area CN. The pervious area CN's are assumed equivalent to desert shrub in poor hydrologic condition.

5 Composite CN's to use for the design of temporary measures during grading and construction should be computed using Figure 603 based on the degree of development (impervious area percentage) and the CN's for the newly graded pervious areas.

Revision	Date

HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

RUNOFF CURVE NUMBERS - RESIDENTIAL DISTRICTS

Average Lot Size or Usage ¹	Percent Impervious ²	Curve Number for Hydrologic Soil Groups			
		A	B	C	D
Apartments/Condos	72	81	88	91	93
Townhouses/6,000 sq ft lots or less ³	69	80	87	90	92
7,000 sq ft lots	63	76	84	89	91
8,000 sq ft lots	58	73	82	88	90
10,000 sq ft lots	38	61	75	83	87
14,000 sq ft lots	30	57	72	81	86
20,000 sq ft lots	25	54	70	80	85
40,000 sq ft lots	20	51	68	79	84
* 80,000 sq ft lots	12	46	65	77	82 *

1 Lot size should represent the size of the average lot and not the gross acreage divided by the number of lots.

2 Actual percent impervious value should be compared to selected land use type.

3 In cases where average residential lots are smaller than 6,000 sq ft, commercial/business/industrial land use should be used.

Revision	Date

REFERENCE:

TABLE 602A

Curve Number Matrix

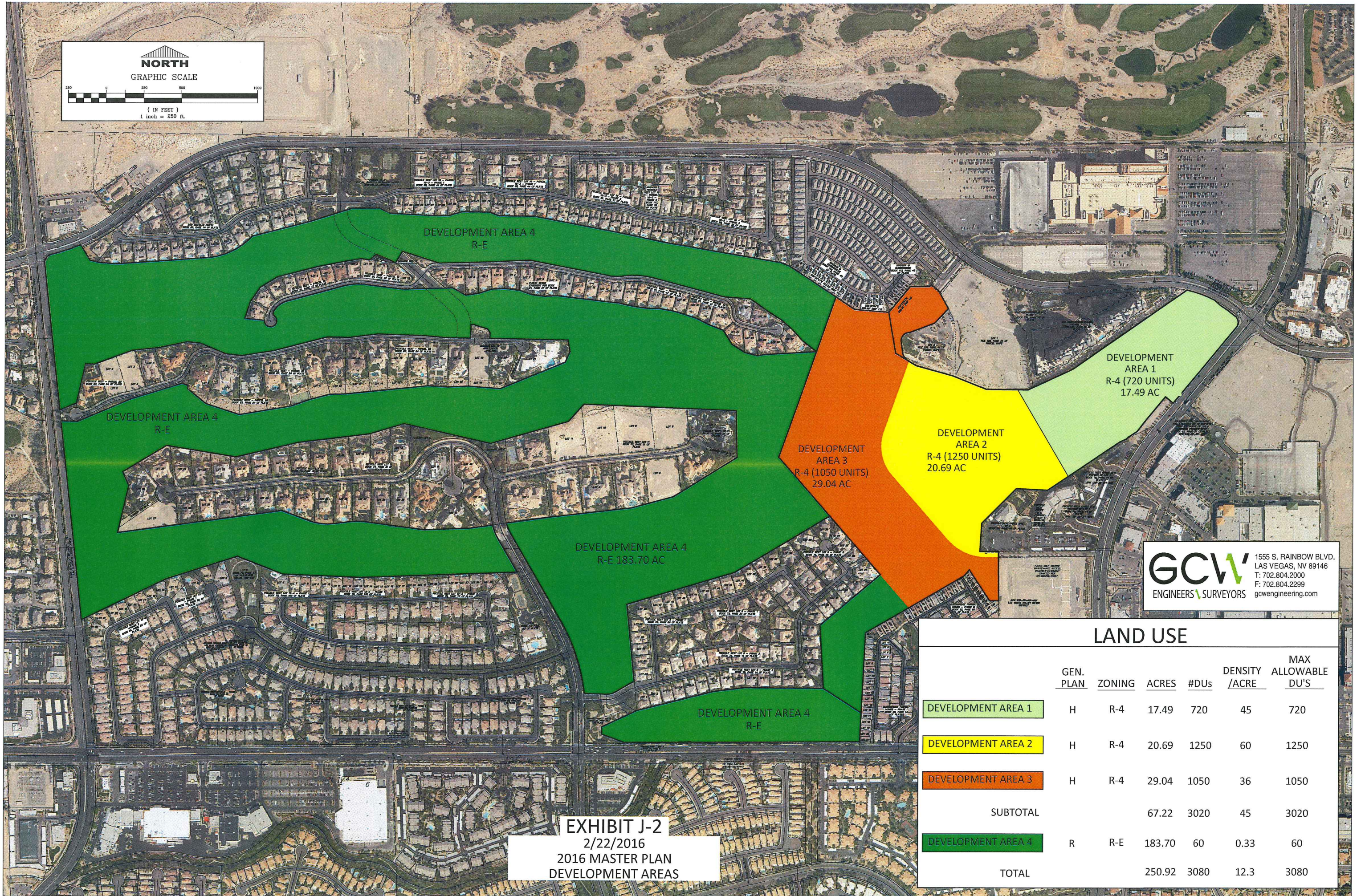
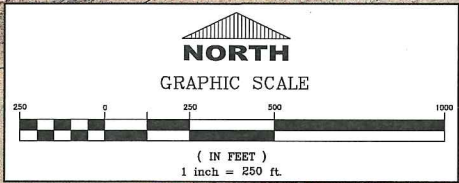
MAP #	COMPONENTS			LAND USE CLASSIFICATION INDEX NUMBER																					
	OPEN DESERT %	OPEN GOOD % ---->	% IMP	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22
				100	10	60	35	0	0	0	0	0	15	7	0	0	55	36	19	14	15	10	30	15	20
				0	85	20	40	71	38	28	15	10	15	8	50	0	20	35	19	14	0	0	0	0	30
				0	5	20	25	29	62	72	85	90	70	85	50	0	25	29	62	72	85	90	70	85	50
				SOIL TYPE COMPOSITE CN FOR LAND USE TYPE																					
	CN	CN	CN																						
152	88	80	98	88.0	82.0	88.0	87.0	85.0	91.0	93.0	95.0	96.0	94.0	96.0	89.0	30.0	89.0	88.0	93.0	94.0	97.0	97.0	95.0	97.0	91.0

* Please refer to Land use Shown on MPU H-maps

PERVIOUS AREA CURVE NUMBERS								
CONDITION 1: ----->		DESERT SHRUB POOR HYDROLOGIC CONDITION						
CONDITION 2: ----->		LANDSCAPED, LAWNS, TREES, GOOD HYDROLOGIC CONDITION						
CN VALUES								
		HYDROLOGIC SOIL GROUP						
CONDITION		A	B	C	D	ROCK		
1 ----->		63	77	85	88	90		
2 ----->		39	61	74	80	90		
							CONDITION	CONDITION
MAP		HYDROLOGIC SOIL GROUP					1	2
UNIT		%A	%B	%C	%D	%ROCK	CN	CN
</								

Orchestra (Phase 1)					
WEIGHTED CURVE NUMBERS					
Proposed Conditions					
Basin	Soil	Percent	CN	Land Use	WCN
57B-1	152	5.0%	82.0	Parks, Golf Courses	93.7
	152	54.0%	93.0	Public Facility, Residential	
	152	41.0%	96.0	Commercial, Retail, Casino, High Rise Condo	
57B-1A	152	100.0%	85.0	Medium Residential	85.0
57B-1B	152	100.0%	93.0	Public Facility, Residential	93.0
57B-1C	152	100.0%	96.0	Commercial, Retail, Casino, High Rise Condo	96.0
57B-2A	152	100.0%	87.0	Low Density Residential	87.0
57B-2B	152	100.0%	87.0	Low Density Residential	87.0
57B-2C	152	100.0%	87.0	Low Density Residential	87.0
57B-2D	152	100.0%	91.0	High Density Residential	91.0
57B-2E	152	100.0%	91.0	High Density Residential	91.0
57B-2F	152	100.0%	91.0	High Density Residential	91.0
57B-2G1	152	100.0%	87.0	Low Density Residential	87.0
57B-2G2	152	100.0%	87.0	Low Density Residential	87.0
57B-2H1	152	100.0%	87.0	Low Density Residential	87.0
57B-2H2	152	100.0%	87.0	Low Density Residential	87.0
57B-2I	152	100.0%	87.0	Low Density Residential	87.0
57B-3	152	29.2%	82.0	Parks, Golf Courses	89.3
	152	9.0%	85.0	Medium Residential	
	152	54.0%	93.0	Public Facility, Residential	
	152	7.8%	96.0	Commercial, Retail, Casino, High Rise Condo	
57B-3A	152	100.0%	85.0	Medium Residential	85.0
57B-3B	152	100.0%	85.0	Medium Residential	85.0
57B-3C	152	100.0%	87.0	Low Density Residential	87.0
57B-3D	152	100.0%	87.0	Low Density Residential	87.0
57B-3E	152	100.0%	87.0	Low Density Residential	87.0
57B-3F	152	100.0%	87.0	Low Density Residential	87.0
57B-3G	152	100.0%	87.0	Low Density Residential	87.0
57B-4	152	8.1%	82.0	Parks, Golf Courses	93.8
	152	0.3%	85.0	Medium Residential	
	152	30.2%	93.0	Public Facility, Residential	
	152	61.3%	96.0	Commercial, Retail, Casino, High Rise Condo	

57B-4B	152	100.0%	96.0	Commercial, Retail, Casino, High Rise Condo	96.0
57B-4C	152	100.0%	96.0	Commercial, Retail, Casino, High Rise Condo	96.0
ON1	152	100.0%	82.0	Parks, Golf Courses	82.0
ON2	152	100.0%	82.0	Parks, Golf Courses	82.0
ON3R	152	100.0%	82.0	Parks, Golf Courses	82.0
ON5	152	100.0%	82.0	Parks, Golf Courses	82.0
ON6	152	100.0%	93.0	Public Facility, Residential	93.0
ON8	152	100.0%	82.0	Parks, Golf Courses	82.0
ON9	152	100.0%	82.0	Parks, Golf Courses	82.0
ON10	152	100.0%	82.0	Parks, Golf Courses	82.0
ON11R	152	100.0%	82.0	Parks, Golf Courses	82.0
ON12	152	100.0%	82.0	Parks, Golf Courses	82.0
ON13	152	100.0%	82.0	Parks, Golf Courses	82.0
ON14	152	100.0%	82.0	Parks, Golf Courses	82.0
ON15R	152	100.0%	82.0	Parks, Golf Courses	82.0
ON16R	152	100.0%	82.0	Parks, Golf Courses	82.0
ON18R	152	100.0%	82.0	Parks, Golf Courses	82.0
DON1	152	100.0%	95.0	Commercial and business	95.0
DON2	152	100.0%	95.0	Commercial and business	95.0
DON3	152	100.0%	95.0	Commercial and business	95.0
DON4	152	100.0%	95.0	Commercial and business	95.0



GCV
ENGINEERS SURVEYORS
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LAS VEGAS, NV 89146
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gcvengineering.com

LAND USE						
	GEN. PLAN	ZONING	ACRES	#DUs	DENSITY /ACRE	MAX ALLOWABLE DU'S
DEVELOPMENT AREA 1	H	R-4	17.49	720	45	720
DEVELOPMENT AREA 2	H	R-4	20.69	1250	60	1250
DEVELOPMENT AREA 3	H	R-4	29.04	1050	36	1050
SUBTOTAL			67.22	3020	45	3020
DEVELOPMENT AREA 4	R	R-E	183.70	60	0.33	60
TOTAL			250.92	3080	12.3	3080

EXHIBIT J-2
2/22/2016
2016 MASTER PLAN
DEVELOPMENT AREAS

HYDROLOGIC CRITERIA AND DESIGN MANUAL

TIME OF CONCENTRATION



The Seventy
Existing Conditions

Project No: 840.050
Date: 17-Feb-16
Calculated by: MMC

DESIG:	DEV./EX. (D or E)	SUB-BASIN DATA				INITIAL / OVERLAND TIME (Ti)			TRAVEL TIME (Tt)				Tc CHECK URBANIZED BASINS			Tc	Tlag	REMARKS
		CN (16)	K (2)	AREA Ac (3)	AREA Sq Mi (4)	INITIAL LENGTH Feet (5)	SLOPE % (6)	Ti Min (7)	TRAVEL LENGTH Feet (8)	SLOPE % (9a)	V1 VELOCITY fps (9b)	V2 VELOCITY fps (10)	Tt Min (11)	TOTAL LENGTH Feet (12)	Tc = (L/180)*10 Min (13)	Min (14)	Hours (15)	
57B-1	D	93.7	0.8468	31.1	0.0485	250	2.80	5.1	3020	2.2	3.0	4.5	12.2	3270	28.2	17.3	0.173	2.89
57B-1A	D	85	0.7320	28.4	0.0443	370	2.40	9.5	2080	2.3	3.1	4.6	8.4	2450	23.6	17.9	0.179	2.96
57B-1B	D	93	0.8376	19.3	0.0301	100	1.00	4.7	1630	1.0	2.0	3.1	10.3	1730	19.6	15.0	0.150	2.91
57B-1C	D	96	0.8772	0.6	0.0009	50	1.00	2.8	490	1.2	2.2	3.4	3.7	540	13.0	6.5	0.065	2.89
57B-2A	D	87	0.7584	6.3	0.0098	186	13.40	3.5	2700	1.7	2.6	4.0	12.4	2886	26.0	15.9	0.159	3.05
57B-2B	D	87	0.7584	3.0	0.0047	50	2.00	3.5	1400	2.7	3.3	5.0	5.5	1450	18.1	8.9	0.089	2.99
57B-2C	D	87	0.7584	1.7	0.0027	100	1.00	6.1	222	6.8	5.3	8.0	0.7	322	11.8	6.9	0.069	2.96
57B-2D	D	91	0.8112	5.7	0.0088	110	1.00	5.5	1200	1.1	2.1	3.2	7.6	1310	17.3	13.0	0.130	3.09
57B-2E	D	91	0.8112	14.5	0.0227	110	1.00	5.5	1360	3.4	3.7	5.6	4.8	1470	18.2	10.2	0.102	3.08
57B-2F	D	91	0.8112	57.8	0.0902	110	1.00	5.5	3000	2.5	3.2	4.8	11.2	3110	27.3	16.7	0.167	3.03
57B-2G1	D	87	0.7584	1.6	0.0026	35	5.60	2.0	730	2.9	3.4	5.2	3.2	765	14.3	5.2	0.052	3.08
57B-2G2	D	87	0.7584	4.6	0.0073	40	2.50	2.9	1511	2.2	3.0	4.5	6.5	1551	18.6	9.4	0.094	3.03
57B-2H1	D	87	0.7584	18.6	0.0291	300	3.70	6.9	4120	1.1	2.1	3.2	22.7	4420	34.6	29.6	0.296	3.01
57B-2H2	D	87	0.7584	10.0	0.0156	300	2.30	8.1	2500	2.2	3.0	4.5	10.1	2800	25.6	18.2	0.182	3.04
57B-2I	D	87	0.7584	4.6	0.0072	80	7.50	2.8	1575	2.6	3.3	4.9	6.2	1655	19.2	9.0	0.090	2.99
57B-3	D	89.3	0.7888	30.8	0.0481	380	1.30	10.0	4170	2.4	3.1	4.7	15.6	4550	35.3	25.6	0.256	3.06
57B-3A	D	85	0.7320	16.6	0.0259	170	1.00	8.6	1360	2.0	2.9	4.3	6.2	1530	18.5	14.9	0.149	3.07
57B-3B	D	85	0.7320	32.8	0.0513	110	1.00	6.9	2500	2.4	3.1	4.7	9.7	2610	24.5	16.6	0.166	3.00
57B-3C	D	87	0.7584	4.4	0.0069	130	1.00	7.0	1140	2.5	3.2	4.8	4.8	1270	17.1	11.8	0.118	3.05
57B-3D	D	87	0.7584	11.8	0.0184	125	1.00	6.9	2500	2.7	3.3	5.0	9.1	2625	24.6	16.0	0.160	2.99
57B-3E	D	87	0.7584	16.0	0.0251	240	1.00	9.5	3200	2.5	3.2	4.8	11.9	3440	29.1	21.4	0.214	3.06
57B-3F	D	87	0.7584	7.4	0.0116	180	2.70	5.9	2170	2.5	3.2	4.9	8.3	2350	23.1	14.2	0.142	3.05
57B-3G	D	87	0.7584	1.5	0.0023	220	3.20	6.2	260	4.6	4.3	6.6	1.0	480	12.7	7.2	0.072	2.99
57B-4	D	93.8	0.8482	82.7	0.1293	35	2.00	2.1	4890	2.4	3.1	4.7	18.1	4925	37.4	20.2	0.202	2.91
57B-4A	D	82	0.6924	4.5	0.0070	274	4.70	7.3	600	2.5	3.2	4.8	3.0	874	14.9	10.2	0.102	2.93
57B-4B	D	96	0.8772	7.1	0.0110	150	2.70	3.5	860	2.9	3.4	5.2	3.6	1010	15.6	7.1	0.071	2.91
57B-4C	D	96	0.8772	7.8	0.0122	100	1.00	4.0	1560	1.6	2.6	3.9	7.8	1660	19.2	11.8	0.118	2.90
ON1	D	82	0.6924	25.4	0.0397	165	4.20	5.8	2040	3.0	3.5	5.3	7.2	2205	22.3	13.1	0.131	3.08
ON2	D	82	0.6924	17.5	0.0273	180	5.00	5.8	2700	2.5	3.2	4.8	10.2	2880	26.0	15.9	0.159	3.00
ON3	D	82	0.6924	2.5	0.0040	135	12.00	3.7	300	1.7	2.6	4.0	1.9	435	12.4	5.6	0.056	2.96
ON4	D	82	0.6924	4.7	0.0073	150	9.30	4.3	530	1.0	2.0	3.1	4.3	680	13.8	8.6	0.086	2.94
ON5	D	82	0.6924	9.4	0.0147	125	4.00	5.2	1420	2.9	3.4	5.2	5.4	1545	18.6	10.5	0.105	3.05

ON6	D	93	0.8376	2.3	0.0035	20	4.00	1.3	785	1.7	2.6	4.0	4.4	805	14.5	5.7	0.057	3.04						
ON8	D	82	0.6924	12.2	0.0190	65	6.20	3.2	1950	8.7	6.0	9.0	4.1	2015	21.2	7.3	0.073	2.99						
ON9	D	82	0.6924	25.5	0.0399	290	15.50	5.0	3085	1.0	2.0	3.1	18.2	3375	28.8	23.2	0.232	3.06						
ON10	D	82	0.6924	11.4	0.0177	100	29.00	2.4	1460	2.9	3.4	5.2	5.5	1560	18.7	7.9	0.079	2.98						
ON11	D	82	0.6924	10.0	0.0157	270	13.70	5.0	1040	1.6	2.6	3.9	5.6	1310	17.3	10.6	0.106	2.95						
ON12	D	82	0.6924	11.6	0.0182	225	3.50	7.2	1300	3.1	3.6	5.4	4.8	1525	18.5	12.1	0.121	3.08						
ON13	D	82	0.6924	12.0	0.0187	210	7.10	5.5	1540	3.6	3.8	5.8	5.2	1750	19.7	10.7	0.107	3.04						
ON14	D	82	0.6924	3.5	0.0054	100	1.00	7.3	1575	0.5	1.4	2.2	14.1	1675	19.3	21.5	0.193	3.00						
ON15	D	82	0.6924	22.5	0.0351	120	7.50	4.1	2160	3.3	3.7	5.6	7.2	2280	22.7	11.4	0.114	2.98						
ON16	D	82	0.6924	11.5	0.0180	45	45.00	1.4	2200	3.3	3.7	5.6	7.4	2245	22.5	8.8	0.088	2.97						
ON17	D	82	0.6924	9.1	0.0143	41	7.30	2.4	1160	3.4	3.7	5.6	4.2	1201	16.7	6.6	0.066	2.93						
ON18	D	82	0.6924	20.3	0.0317	175	0.60	11.5	2930	2.5	3.2	4.9	10.9	3105	27.3	22.4	0.224	2.95						
ON19	D	82	0.6924	6.4	0.0100	112	1.80	6.4	785	4.2	4.1	6.3	2.8	897	15.0	9.2	0.092	2.92						
ON20	D	82	0.6924	6.6	0.0104	200	9.00	5.0	1415	2.0	2.9	4.3	6.4	1615	19.0	11.4	0.114	2.89						
ON21	D	82	0.6924	22.3	0.0348	270	1.10	11.7	2222	3.0	3.5	5.3	7.8	2492	23.8	19.5	0.195	2.91						
ON22	D	82	0.6924	8.5	0.0133	65	3.10	4.1	970	4.9	4.5	6.8	3.0	1035	15.8	7.1	0.071	2.88						
Tc = Ti + Tt Ti = 1.8 (1.1 - K) L ^{1/2} / S ^{1/3} K = 0.0132 (CN) - 0.39																			For the travel time (Tt) calculations, V1 applies to the first 500 feet of travel distance; V2 applies to the remaining travel distance.		Existing: V1 = 14.8*(S/100) ^{1/2} V2 = 29.4*(S/100) ^{1/2}		Developed: V1 = 20.2*(S/100) ^{1/2} V2 = 30.6*(S/100) ^{1/2}	
REFERENCE: CN values referenced from MPU																							STANDARD FORM 4	


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1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   JUN 1998
*   VERSION 4.1
*
* RUN DATE 03MAR16 TIME 10:06:06
*
*****
EXISTING.OUT
*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*** FREE ***
*DIAGRAM
ID *****
ID *
ID *
ID * THE SEVENTY
ID *
ID * EXISTING CONDITIONS
ID *
ID * RETURN PERIOD 100 & 10 -YEAR
ID * DISTRIBUTION 6-HOUR SDN3
ID * PROJECT NO 840.050
ID * FILENAME EXISTING.H1
ID * DATE MODELED 2/22/16
ID * MODELED BY JAM, MMC, RRD, SHT
ID *
ID *****
ID
ID REFERENCED HYDROLOGIC MODELS:
ID 2013 LAS VEGAS VALLEY FLOOD CONTROL MASTER PLAN UPDATE
ID CITY OF LAS VEGAS CITY WIDE HYDROLOGY ANALYSIS (PBS&J 1997)
ID CLARK COUNTY REGIONAL FLOOD CONTROL DISTRICT 2008 MASTER PLAN UPDATE
ID GOWAN WATERSHED (ALL)
ID RECOMMENDED DRAINAGE SYSTEM WITH ULTIMATE DEVELOPMENT
ID INPUT FILE = ALLGOW3.DAT
ID INPUT FILE DATE = MAY 5, 2008
ID DESIGN STORM = 100-YEAR 6-HR STORM
ID STORM DISTRIBUTION = SDN #3
ID MODELED BY PBS&J (MICHELE L. D'ALESSANDRO, E.I., CFM)
ID CHECKED BY PBS&J (HARSHAL B. DESAI, P.E., CFM)
ID STORM CENTERING = FULL WATERSHED
ID JR CARDS CONTAIN DARFS BASED ON THE FOLLOWING VALUES:
ID
ID AREA DARF
ID SQ. MI.
ID 0-0.5 0.99
ID 0.5-1 0.975
ID 1-2 0.95
ID 2-3 0.925
ID 3-4 0.915
ID 4-5 0.908
ID 5-6 0.903
ID 6-7 0.895
ID 10yr 0.570
ID
ID JR CARD RATIOS REPRESENT DEPTH-AREA REDUCTION FACTORS (DARF'S)
ID
ID 100-YEAR, 6-HOUR STORM, SDN3
ID
ID IT 5 0 0 650
ID IO 5 0 0
ID IN 5 0 0
ID JR PREC 0.99 0.975 0.95 0.925 0.915 0.908 0.903 0.895 0.570
ID *

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1 HEC-1 INPUT PAGE 2

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
54 KK ON1
55 KM OFFSITE BASIN ON1
56 PB 3.08
57 BA 0.0397
58 PC 0 0.02 0.057 0.07 0.087 0.108 0.124 0.13 0.13 0.13
59 PC 0.13 0.13 0.13 0.133 0.14 0.142 0.148 0.158 0.172 0.181
60 PC 0.19 0.197 0.199 0.2 0.201 0.204 0.214 0.229 0.241 0.249
61 PC 0.251 0.256 0.27 0.278 0.281 0.283 0.295 0.322 0.352 0.409
62 PC 0.499 0.59 0.71 0.744 0.781 0.812 0.819 0.835 0.851 0.856
63 PC 0.86 0.868 0.876 0.888 0.91 0.926 0.937 0.95 0.97 0.976
64 PC 0.982 0.985 0.987 0.989 0.99 0.993 0.993 0.994 0.995 0.998
65 PC 0.998 0.999 1
66 LS 0 82

```


EXISTING.OUT

67 UD .131
 *
 68 KK 57B-3A
 69 KM ONSITE BASIN 57B-3A
 70 PB 3.07
 71 BA 0.0259
 72 LS 0 85
 73 UD .149
 *
 74 KK CON1
 75 KM COMBINE 57B-3A AND ON1
 76 HC 2
 *
 77 KK RCON1
 78 KM ROUTE CON1 TO CON2
 79 KM LENGTH SLOPE n-VALUE 0 SHAPE WIDTH S-SLOPE
 80 RD 3020 .027 .040 0 TRAP 50 3
 *
 81 KK 57B-3B
 82 KM OFFSITE BASIN 57B-3B
 83 PB 3.00
 84 BA 0.0513
 85 LS 0 85
 86 UD .166
 *
 87 KK ON2
 88 KM OFFSITE BASIN ON2
 89 PB 3.00
 90 BA 0.0273
 91 LS 0 82
 92 UD .159
 *

HEC-1 INPUT

PAGE 3

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

93 KK CON2
 94 KM COMBINE CON1, 57B-3B AND ON2
 95 HC 3
 *
 96 KK 57B-3D
 97 KM OFFSITE BASIN 57B-3D
 98 PB 2.99
 99 BA 0.0184
 100 LS 0 87
 101 UD .160
 *
 102 KK ON3
 103 KM ONSITE BASIN ON3
 104 PB 2.96
 105 BA 0.0040
 106 LS 0 82
 107 UD .056
 *
 108 KK CON3
 109 KM COMBINE CON2, 57B-3D AND ON3
 110 HC 3
 *
 111 KK ON4
 112 KM OFFSITE BASIN ON4
 113 PB 2.94
 114 BA 0.0073
 115 LS 0 82
 116 UD .086
 *
 117 KK CON4
 118 KM COMBINE CON3 AND ON4
 119 HC 2
 *
 120 KK ON5
 121 KM OFFSITE BASIN ON5
 122 PB 3.05
 123 BA 0.0147
 124 LS 0 82
 125 UD .105
 *
 126 KK 57B-3C
 127 KM OFFSITE BASIN 57B-3C
 128 PB 3.05
 129 BA 0.0069
 130 LS 0 87
 131 UD .118
 *

HEC-1 INPUT

PAGE 4

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

132 KK ON6
 133 KM OFFSITE BASIN ON6
 134 PB 3.04
 135 BA 0.0035
 136 LS 0 93
 137 UD .057
 *
 138 KK CON6
 139 KM COMBINE 57B-3C AND ON6
 140 HC 2

EXISTING.OUT

*
 141 KK CCON6
 142 KM COMBINE ON5 AND CON6
 143 HC 2
 *
 144 KK RCON6
 145 KM ROUTE CCON6 TO CON8
 146 KM LENGTH SLOPE n-VALUE
 147 RD 2015 .037 .040 0 SHAPE WIDTH S-SLOPE
 * TRAP 20 2
 *
 148 KK ON8
 149 KM ONSITE BASIN ON8
 150 PB 2.99
 151 BA 0.0190
 152 LS 0 82
 153 UD .073
 *
 154 KK CON8
 155 KM COMBINE CCON6 AND ON8
 156 HC 2
 *
 157 KK SW11
 158 BA 0.589
 159 PB 3.34
 160 LS 0 87.8
 161 UD 0.311
 *
 162 KK RSW11
 163 KM ROUTE SW11 TO CSW17
 164 KM FACILITY = ANGEL PARK - CHARLESTON BOULEVARD
 165 KM FACILITY # = APCB 0064, 0080
 166 KM LINING = RCB
 167 RD 2338 0.0167 0.015 0 TRAP 7 0
 *

HEC-1 INPUT

PAGE 5

1 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

168 KK SW17
 169 BA 0.356
 170 PB 3.30
 171 LS 0 87.8
 172 UD 0.271
 *
 173 KK CSW17
 174 KM COMBINE RSW11 AND SW17
 175 HC 2
 *
 176 KK RCSW17
 177 KM ROUTE CSW17 TO CSW18
 178 KM FACILITY = ANGEL PARK - CHARLESTON BOULEVARD
 179 KM FACILITY # = APCB 0000,0001,0019,0050
 180 KM LINING = RCB
 181 RD 3600 0.014 0.015 0 TRAP 11 0
 *
 182 KK SW18
 183 BA 0.405
 184 PB 3.27
 185 LS 0 86.8
 186 UD 0.271
 *
 187 KK CSW18
 188 KM COMBINE RCSW17 AND SW18
 189 HC 2
 *
 190 KK RCSW18
 191 KM ROUTE CSW18 TO C12A
 192 KM FACILITY = ANGEL PARK SOUTH
 193 KM FACILITY # = APSO 0254,0255,0258,0345,0346; APCB 0000
 194 KM NATURAL WASH
 195 KM LENGTH = 5,200
 196 KM SLOPE = 1.4%
 197 KM N = 0.040
 198 KM HYDRAULIC RADIUS = 1.5
 199 KM VELOCITY = 9.2
 200 RM 2 0.157 0.15
 *

201 KK 12A
 202 BA 0.392
 203 PB 3.20
 204 LS 0 91.2
 205 UD 0.264
 *

HEC-1 INPUT

PAGE 6

1 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

206 KK C12A
 207 KM COMBINE 12A AND RCSW18
 208 HC 2
 *
 209 KK RC12A
 210 KM ROUTE THRU 12B
 211 KM FACILITY = ANGEL PARK SOUTH
 212 KM FACILITY # = APSO 0204, 0205
 213 KM NATURAL WASH
 214 KM LENGTH = 2,600

EXISTING.OUT

215 KM SLOPE = 3.5%
 216 KM N = 0.040
 217 KM HYDRAULIC RADIUS = 1.5
 218 KM VELOCITY = 14.5
 219 RM 1 0.05 0.15
 *

220 KK 12B
 221 BA 0.260
 222 PB 3.13
 223 LS 0 91.0
 224 UD 0.233
 *

225 KK C12B
 226 KM COMBINE 12B AND RC12A
 227 HC 2
 *

228 KK 57B-2A
 229 KM OFFSITE BASIN 57B-2A
 230 PB 3.05
 231 BA 0.0098
 232 LS 0 87
 233 UD .159
 *

234 KK 57B-3F
 235 KM OFFSITE BASIN 57B-3F
 236 PB 3.05
 237 BA 0.0116
 238 LS 0 87
 239 UD .142
 *

240 KK 57B-3E
 241 KM OFFSITE BASIN 57B-3E
 242 PB 3.06
 243 BA 0.0251
 244 LS 0 87
 245 UD .214
 *

HEC-1 INPUT

PAGE 7

1 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

246 KK ON9
 247 KM ONSITE BASIN ON9
 248 PB 3.06
 249 BA 0.0399
 250 LS 0 82
 251 UD .232
 *

252 KK CON9
 253 KM COMBINE C12B, 57B-2A, 57B-3F, 57B-3E AND ON9
 254 HC 5
 *

255 KK RCON9
 256 KM ROUTE CON9 TO CON10
 257 RD LENGTH SLOPE n-VALUE 0 SHAPE WIDTH S-SLOPE
 258 1540 .030 .040 0 TRAP 50 2
 *

259 KK 57B-3G
 260 KM OFFSITE BASIN 57B-3G
 261 PB 2.99
 262 BA 0.0023
 263 LS 0 87
 264 UD .072
 *

265 KK 57B-2B
 266 KM OFFSITE BASIN 57B-2B
 267 PB 2.99
 268 BA 0.0047
 269 LS 0 87
 270 UD .089
 *

271 KK 57B-2C
 272 KM OFFSITE BASIN 57B-2C
 273 PB 2.96
 274 BA 0.0027
 275 LS 0 87
 276 UD .069
 *

277 KK ON10
 278 KM ONSITE BASIN ON10
 279 PB 2.98
 280 BA 0.0177
 281 LS 0 82
 282 UD .079
 *

HEC-1 INPUT

PAGE 8

1 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

283 KK CON10
 284 KM COMBINE C57B-2A, 57B-3G, 57B-2B, 57B-2C AND ON10
 285 HC 5
 *

286 KK CCON10
 287 KM COMBINE CON8 AND CON10
 288 HC 2
 *

		EXISTING.OUT					
289	KK	RCON10					
290	KM	ROUTE CCON10 TO CON11					
291	KM	LENGTH	SLOPE	n-VALUE	0	SHAPE	WIDTH
292	RD	1040	.014	.040		TRAP	20
	*						S-SLOPE
							2
293	KK	ON11					
294	KM	ONSITE BASIN ON11					
295	PB	2.95					
296	BA	0.0157					
297	LS	0	82				
298	UD	.106					
	*						
299	KK	CON11					
300	KM	COMBINE CCON10 AND ON11					
301	HC	2					
	*						
302	KK	CCON11					
303	KM	COMBINE CON4 AND CON11					
304	HC	2					
	*						
305	KK	57B-2D					
306	KM	OFFSITE BASIN 57B-2D					
307	PB	3.09					
308	BA	0.0088					
309	LS	0	91				
310	UD	.130					
	*						
311	KK	57B-2E					
312	KM	OFFSITE BASIN 57B-2E					
313	PB	3.08					
314	BA	0.0227					
315	LS	0	91				
316	UD	.102					
	*						

HEC-1 INPUT

PAGE 9

1

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
317	KK C57B-2E
318	KM COMBINE 57B-2D AND 57B-2E
319	HC 2
	*
320	KK 57B-2G1
321	KM OFFSITE BASIN 57B-2G1
322	PB 3.08
323	BA 0.0026
324	LS 0
325	UD .052
	*
326	KK ON12
327	KM ONSITE BASIN ON12
328	PB 3.08
329	BA 0.0182
330	LS 0
331	UD .121
	*
332	KK CON12
333	KM COMBINE C57B-2E, 57B-2G1 AND ON12
334	HC 3
	*
335	KK 57B-2G2
336	KM OFFSITE BASIN 57B-2G2
337	PB 3.03
338	BA 0.0073
339	LS 0
340	UD .094
	*
341	KK ON13
342	KM ONSITE BASIN ON13
343	PB 3.04
344	BA 0.0187
345	LS 0
346	UD .107
	*
347	KK CON13
348	KM COMBINE CON12, 57B-2G2 AND ON13
349	HC 3
	*
350	KK 57B-2F
351	KM OFFSITE BASIN 57B-2F
352	PB 3.03
353	BA 0.0902
354	LS 0
355	UD .167
	*

HEC-1 INPUT

PAGE 10

1

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
356	KK 57B-2H2
357	KM OFFSITE BASIN 57B-2H2
358	PB 3.04
359	BA 0.0156
360	LS 0
361	UD .182
	*
362	KK ON14

EXISTING.OUT

```

363      KM  ONSITE BASIN ON14
364      PB      3.00
365      BA  0.0054
366      LS      0      82
367      UD  .193
      *

368      KK  CON14
369      KM  COMBINE C57B-2F, 57B-2H2 AND ON14
370      HC      3
      *

371      KK  RCON14
372      KM  ROUTE CON14 TO CON15
373      KM  LENGTH  SLOPE  n-VALUE
374      RD  2160    .032    .040      0  SHAPE  WIDTH  S-SLOPE
      *                TRAP      20      2

375      KK  57B-2I
376      KM  OFFSITE BASIN 57B-2I
377      PB      2.99
378      BA  0.0072
379      LS      0      87
380      UD  .090
      *

381      KK  57B-2H1
382      KM  OFFSITE BASIN 57B-2H1
383      PB      3.01
384      BA  0.0291
385      LS      0      87
386      UD  .296
      *

387      KK  ON15
388      KM  ONSITE BASIN ON15
389      PB      2.98
390      BA  0.0351
391      LS      0      82
392      UD  .114
      *

```

1

HEC-1 INPUT

PAGE 11

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

393      KK  CON15
394      KM  COMBINE CON13, CON14, 57B-21, 57B-2H1 AND ON15
395      HC      5
      *

396      KK  ON16
397      KM  ONSITE BASIN ON16
398      PB      2.97
399      BA  0.0180
400      LS      0      82
401      UD  .088
      *

402      KK  CON16
403      KM  COMBINE CON15 AND ON16
404      HC      2
      *

405      KK  RCON16
406      KM  ROUTE CON16 TO CON17
407      KM  LENGTH  SLOPE  n-VALUE
408      RD  1050    .036    .040      0  SHAPE  WIDTH  S-SLOPE
      *                TRAP      20      2

409      KK  ON17
410      KM  ONSITE BASIN ON17
411      PB      2.93
412      BA  0.0143
413      LS      0      82
414      UD  .066
      *

415      KK  CON17
416      KM  COMBINE CON16 AND ON17
417      HC      2
      *

418      KK  RCON17
419      KM  ROUTE CON17 TO CON21
420      KM  LENGTH  SLOPE  n-VALUE
421      RD  1160    .027    .040      0  SHAPE  WIDTH  S-SLOPE
      *                TRAP      30      2

422      KK  57B-4A
423      KM  OFFSITE BASIN 57B-4A
424      PB      2.93
425      BA  0.0070
426      LS      0      82
427      UD  .102
      *

```

1

HEC-1 INPUT

PAGE 12

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

428      KK  CCON17
429      KM  COMBINE CCON11, CON17 AND 57B-4A
430      HC      3
      *

431      KK  ON21
432      KM  ONSITE BASIN ON21
433      PB      2.91
434      BA  0.0348
435      LS      0      82
436      UD  .195
      *

```


EXISTING.OUT

```

*
437 KK CON21
438 KM COMBINE CCON17 AND ON21
439 HC 2
*

440 KK 13B-1
441 BA 0.249
442 PB 3.19
443 LS 0 91.6
444 UD 0.284
*

445 KK RC13B-1
446 KM ROUTE 13B-1 TO C13B-2
447 KM GRIFFITH PARK DRIVE AND HUALAPAI WAY
448 RD 3000 0.018 0.016 0 TRAP 0 50
*

449 KK 13B-2
450 BA 0.216
451 PB 3.14
452 LS 0 89.7
453 UD 0.231
*

454 KK C13B-2
455 KM COMBINE 13B-2 AND RC13B-1
456 KM HUALAPAI WAY AND LOCAL FACILITY
457 HC 2
*

458 KK RC13B-2
459 KM ROUTE C13B-2 TO CCPIC-A
460 KM LINING = GRASS
461 RD 4900 0.021 0.03 0 TRAP 40 6
*

```

HEC-1 INPUT

PAGE 13

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

462 KK 19A
463 BA 0.253
464 PB 3.25
465 LS 0 89.9
466 UD 0.351
*

467 KK R19A
468 KM ROUTE 19A TO C13A-1
469 KM UNNAMED ROAD
470 RD 4300 0.021 0.016 0 TRAP 0 50
*

471 KK 13A-1
472 BA 0.224
473 PB 3.19
474 LS 0 91.4
475 UD 0.302
*

476 KK C13A-1
477 KM COMBINE 13A-1 AND R19A
478 KM TOWN CENTER DRIVE AND SWALE
479 HC 2
*

480 KK RC13A-1
481 KM ROUTE C13A-1 TO C13A-2
482 KM NATURAL WASH
483 KM TRAVEL LENGTH = 2,800
484 KM SLOPE = 2.1%
485 KM N = 0.040
486 KM HYDRAULIC RADIUS = 1.5
487 KM VELOCITY = 11.4
488 RM 1 0.068 0.15
*

489 KK 13A-2
490 BA 0.188
491 PB 3.15
492 LS 0 90.0
493 UD 0.236
*

494 KK C13A-2
495 KM COMBINE 13A-2 AND RC13A-1
496 HC 2
*

```

HEC-1 INPUT

PAGE 14

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

497 KK RC13A-2
498 KM ROUTE C13A-2 TO CPIC-C
499 KM LINING = GRASS
500 RD 5200 0.015 0.03 0 TRAP 40 4
*

501 KK PIC-C
502 BA 0.243
503 PB 3.08
504 LS 0 90.4
505 UD 0.373
*

506 KK CPIC-C
507 KM COMBINE PIC-C AND RC13A-2
508 HC 2

```


EXISTING.OUT

509 KK RCPIC-C
 510 KM ROUTE CPIC-C TO CPIC-A
 511 KM LINING = GRASS
 512 RD 2200 0.025 0.03 0 TRAP 40 4
 *

513 KK PIC-A
 514 BA 0.359
 515 PB 3.03
 516 LS 0 91.1
 517 UD 0.499
 *

518 KK CPIC-A
 519 KM COMBINE RCPIC-C AND PIC-A
 520 HC 2
 *

521 KK CCPIC-A
 522 KM COMBINE CPIC-A AND RC13B-2
 523 HC 2
 *

524 KK ON18
 525 KM ONSITE BASIN ON18
 526 PB 2.95
 527 BA 0.0317
 528 LS 0 82
 529 UD .224
 *

HEC-1 INPUT

PAGE 15

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

530 KK CON18
 531 KM COMBINE CCPIC-A AND ON18
 532 HC 2
 *

533 KK 57B-1A
 534 KM OFFSITE BASIN 57B-1A
 535 PB 2.96
 536 BA 0.0443
 537 LS 0 85
 538 UD .179
 *

539 KK 57B-1B
 540 KM OFFSITE BASIN 57B-1B
 541 PB 2.91
 542 BA 0.0301
 543 LS 0 93
 544 UD .150
 *

545 KK ON19
 546 KM ONSITE BASIN ON19
 547 PB 2.92
 548 BA 0.0100
 549 LS 0 82
 550 UD .092
 *

551 KK CON19
 552 KM COMBINE CON18, 57B-1A, 57B-1B AND ON19
 553 HC 4
 *

554 KK RCON19
 555 KM ROUTE CON19 TO CON20
 556 KM LENGTH SLOPE n-VALUE
 557 RD 1480 .024 .040 0 SHAPE TRAP WIDTH 50 S-SLOPE 2
 *

558 KK 57B-1C
 559 KM OFFSITE BASIN 57B-1C
 560 PB 2.89
 561 BA 0.0009
 562 LS 0 96
 563 UD .065
 *

564 KK ON20
 565 KM ONSITE BASIN ON20
 566 PB 2.89
 567 BA 0.0104
 568 LS 0 82
 569 UD .114
 *

HEC-1 INPUT

PAGE 16

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

570 KK CON20
 571 KM COMBINE CON19, 57B-1C AND ON20
 572 HC 3
 *

573 KK RCON20
 574 KM ROUTE CON20 TO CON22
 575 KM LENGTH SLOPE n-VALUE
 576 RD 700 .063 .040 0 SHAPE TRAP WIDTH 30 S-SLOPE 2
 *

577 KK 57B-4B
 578 KM OFFSITE BASIN 57B-4B
 579 PB 2.91
 580 BA 0.0110

EXISTING.OUT

581	LS	0	96
582	UD	.071	
	*		
583	KK	57B-4C	
584	KM	OFFSITE BASIN 57B-4C	
585	PB	2.90	
586	BA	0.0122	
587	LS	0	96
588	UD	.118	
	*		
589	KK	C57B-4C	
590	KM	COMBINE 57B-4B AND 57B-4C	
591	HC	2	
	*		
592	KK	ON22	
593	KM	ONSITE BASIN ON22	
594	PB	2.88	
595	BA	0.0133	
596	LS	0	82
597	UD	.071	
	*		
598	KK	CON22	
599	KM	COMBINE CON21, CON20, C57B-4C AND ON22	
600	HC	4	
	*		
601	KK	57B-1	
602	KM	OFFSITE BASIN 57B-1	
603	BA	0.0485	
604	PB	2.89	
605	LS	0	93.7
606	UD	0.173	
	*		

HEC-1 INPUT

PAGE 17

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
607	KK 57B-3
608	KM OFFSITE BASIN 57B-3
609	BA 0.0481
610	PB 3.06
611	LS 0 89.3
612	UD 0.256
	*
613	KK 57B-4
614	KM OFFSITE BASIN 57B-4
615	BA 0.1293
616	PB 2.91
617	LS 0 93.8
618	UD 0.202
	*
619	KK C57B-4
620	KM COMBINE 57B-3 AND 57B-4
621	HC 2
	*
622	KK PIC-B
623	BA 0.441
624	PB 2.98
625	LS 0 91.1
626	UD 0.471
	*
627	KK RPIC-B
628	KM ROUTE PIC-B TO CC57B-4
629	KM FACILITY = ANGEL PARK - PECCOLE 1
630	KM FACILITY # = APP1 0000
631	KM LINING = RCP
632	RD 2982 0.024 0.013 0 CIRC 6
	*
633	KK CC57B-4
634	KM COMBINE CON22, C57B-1, RPIC-B, AND C57B-4
635	HC 4
	*
636	ZZ

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

```

54  ON1
    .
68  . 57B-3A
    .
74  CON1.....
    V
77  RCON1
    .
81  . 57B-3B
    .
87  . ON2
    .
93  CON2.....
    .
96  . 57B-3D
  
```

EXISTING.OUT

102				ON3	
108	CON3				
111		ON4			
117	CON4				
120		ON5			
126			57B-3C		
132				ON6	
138			CON6		
141		CCON6			
144		V			
148		RCCON6			
154			ON8		
157			CON8		
162			SW11		
168			V		
173			RSW11		
176				SW17	
182					
187			CSW17		
190			V		
201			RCSW17		
206				SW18	
209			CSW18		
220			V		
225			RCSW18		
228				12A	
234					
240			C12A		
246			V		
252			RC12A		
255				12B	
259			C12B		
265				57B-2A	
271					
277				57B-3F	
283					
286				57B-3E	
					ON9
			CON9		
			V		
			RCON9		
				57B-3G	
				57B-2B	
				57B-2C	
					ON10
			CON10		
			CCON10		
			V		

EXISTING.OUT

289	.	.	V		
	.	.	RCON10		
293	.	.	.	ON11	
	
299	.	.	CON11.....	.	
	
302	.	.	CCON11.....	.	
	
305	.	.	57B-2D	.	
	
311	.	.	.	57B-2E	
	
317	.	.	C57B-2E.....	.	
	
320	.	.	.	57B-2G1	
	
326	ON12

332	.	.	CON12.....	.	
	
335	.	.	.	57B-2G2	
	
341	ON13

347	.	.	CON13.....	.	
	
350	.	.	.	57B-2F	
	
356	57B-2H2

362	ON14

368	.	.	CON14.....	.	
	
	.	.	.	V	
	.	.	.	V	
371	.	.	RCON14	.	
	
375	.	.	.	57B-2I	
	
381	57B-2H1

387	ON15

393	.	.	CON15.....	.	
	
396	.	.	.	ON16	
	
402	.	.	CON16.....	.	
	
	.	.	.	V	
	.	.	.	V	
405	.	.	RCON16	.	
	
409	.	.	.	ON17	
	
415	.	.	CON17.....	.	
	
	.	.	.	V	
	.	.	.	V	
418	.	.	RCON17	.	
	
422	.	.	.	57B-4A	
	
428	.	.	CCON17.....	.	
	
431	.	.	.	ON21	
	
437	.	.	CON21.....	.	
	
440	.	.	.	13B-1	
	
	.	.	.	V	
445	.	.	RC13B-1	.	
	
449	.	.	.	13B-2	
	
454	.	.	C13B-2.....	.	
	
	.	.	.	V	
	.	.	.	V	
458	.	.	RC13B-2	.	
	

EXISTING.OUT

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462      .      .      19A
      .      .      V
467      .      .      R19A
      .      .      .
471      .      .      .      13A-1
      .      .      .      .
476      .      .      C13A-1.....
      .      .      .      V
480      .      .      RC13A-1
      .      .      .
489      .      .      .      13A-2
      .      .      .      .
494      .      .      C13A-2.....
      .      .      .      V
497      .      .      RC13A-2
      .      .      .
501      .      .      .      PIC-C
      .      .      .      .
506      .      .      CPIC-C.....
      .      .      .      V
509      .      .      RCPIC-C
      .      .      .
513      .      .      .      PIC-A
      .      .      .      .
518      .      .      CPIC-A.....
      .      .      .
521      .      .      CCPIC-A.....
      .      .      .
524      .      .      .      ON18
      .      .      .      .
530      .      .      CON18.....
      .      .      .
533      .      .      .      57B-1A
      .      .      .      .
539      .      .      .      .      57B-1B
      .      .      .      .
545      .      .      .      .      ON19
      .      .      .      .
551      .      .      CON19.....
      .      .      .      V
554      .      .      RCON19
      .      .      .
558      .      .      .      57B-1C
      .      .      .      .
564      .      .      .      .      ON20
      .      .      .      .
570      .      .      CON20.....
      .      .      .      V
573      .      .      RCON20
      .      .      .
577      .      .      .      57B-4B
      .      .      .      .
583      .      .      .      .      57B-4C
      .      .      .      .
589      .      .      .      C57B-4C.....
      .      .      .      .
592      .      .      .      .      ON22
      .      .      .      .
598      .      .      CON22.....
      .      .      .
601      .      .      .      57B-1
      .      .      .      .
607      .      .      .      .      57B-3
      .      .      .      .
613      .      .      .      .      57B-4
      .      .      .      .
619      .      .      .      C57B-4.....
      .      .      .      .
622      .      .      .      .      PIC-B
      .      .      .      .      V
627      .      .      .      .      RPIC-B
      .      .      .      .
633      .      .      .      .      CC57B-4.....

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION
 1*****

* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
 * JUN 1998 *
 * VERSION 4.1 *
 * RUN DATE 03MAR16 TIME 10:06:06 *

EXISTING.OUT

* U.S. ARMY CORPS OF ENGINEERS *
 * HYDROLOGIC ENGINEERING CENTER *
 * 609 SECOND STREET *
 * DAVIS, CALIFORNIA 95616 *
 * (916) 756-1104 *

 * THE SEVENTY *
 * EXISTING CONDITIONS *
 * RETURN PERIOD 100 & 10 -YEAR *
 * DISTRIBUTION 6-HOUR SDN3 *
 * PROJECT NO. 840.050 *
 * FILENAME EXISTING.H1 *
 * DATE MODELED 2/22/16 *
 * MODELED BY JAM, MMC, RRD, SHT *

REFERENCED HYDROLOGIC MODELS:
 2013 LAS VEGAS VALLEY FLOOD CONTROL MASTER PLAN UPDATE
 CITY OF LAS VEGAS CITY WIDE HYDROLOGY ANALYSIS (PBS&J 1997)
 CLARK COUNTY REGIONAL FLOOD CONTROL DISTRICT 2008 MASTER PLAN UPDATE
 GOWAN WATERSHED (ALL)
 RECOMMENDED DRAINAGE SYSTEM WITH ULTIMATE DEVELOPMENT
 INPUT FILE = ALLGOW3.DAT
 INPUT FILE DATE = MAY 5, 2008
 DESIGN STORM = 100-YEAR 6-HR STORM
 STORM DISTRIBUTION = SDN #3
 MODELED BY PBS&J (MICHELE L. D'ALESSANDRO, E.I., CFM)
 CHECKED BY PBS&J (HARSHAL B. DESAI, P.E., CFM)
 STORM CENTERING = FULL WATERSHED
 JR CARDS CONTAIN DARFS BASED ON THE FOLLOWING VALUES:

AREA SQ. MI.	DARF
0-0.5	0.99
0.5-1	0.975
1-2	0.95
2-3	0.925
3-4	0.915
4-5	0.908
5-6	0.903
6-7	0.895
10yr	0.570

JR CARD RATIOS REPRESENT DEPTH-AREA REDUCTION FACTORS (DARF'S)
 100-YEAR, 6-HOUR STORM, SDN3

51 IO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IT HYDROGRAPH TIME DATA
 NMIN 5 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 650 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 3 0 ENDING DATE
 NDTIME 0605 ENDING TIME
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS
 TOTAL TIME BASE 54.08 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-Feet
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .99 .98 .95 .93 .92 .91 .90 .89 .57

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION								
				RATIO 1 .99	RATIO 2 .98	RATIO 3 .95	RATIO 4 .93	RATIO 5 .92	RATIO 6 .91	RATIO 7 .90	RATIO 8 .89	RATIO 9 .57
HYDROGRAPH AT	ON1	.04	1	50. 3.58	49.	47.	45.	44.	43.	43.	42.	18.
HYDROGRAPH AT	57B-3A	.03	1	36.	35.	34.	32.	32.	31.	31.	31.	14.

				TIME	3.58	EXISTING. OUT 3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58
2 COMBINED AT	CON1	.07	1	FLOW TIME	86. 3.58	84. 3.58	80. 3.58	77. 3.58	76. 3.58	75. 3.58	74. 3.58	73. 3.58	32. 3.58
ROUTED TO	RCON1	.07	1	FLOW TIME	86. 3.75	84. 3.75	80. 3.75	77. 3.75	76. 3.75	75. 3.75	74. 3.75	73. 3.75	30. 3.83
HYDROGRAPH AT	57B-3B	.05	1	FLOW TIME	66. 3.58	65. 3.58	62. 3.58	59. 3.58	58. 3.58	58. 3.58	57. 3.58	56. 3.58	25. 3.58
HYDROGRAPH AT	ON2	.03	1	FLOW TIME	31. 3.58	30. 3.58	29. 3.58	28. 3.58	27. 3.58	27. 3.58	27. 3.58	26. 3.58	11. 3.58
3 COMBINED AT	CON2	.14	1	FLOW TIME	164. 3.67	160. 3.67	153. 3.67	145. 3.67	143. 3.67	141. 3.67	139. 3.67	137. 3.67	55. 3.75
HYDROGRAPH AT	57B-3D	.02	1	FLOW TIME	26. 3.58	25. 3.58	24. 3.58	23. 3.58	23. 3.58	23. 3.58	23. 3.58	22. 3.58	11. 3.58
HYDROGRAPH AT	ON3	.00	1	FLOW TIME	6. 3.50	6. 3.50	6. 3.50	5. 3.50	5. 3.50	5. 3.50	5. 3.50	5. 3.50	2. 3.50
3 COMBINED AT	CON3	.17	1	FLOW TIME	189. 3.67	185. 3.67	177. 3.67	169. 3.67	165. 3.67	163. 3.67	161. 3.67	159. 3.67	64. 3.75
HYDROGRAPH AT	ON4	.01	1	FLOW TIME	9. 3.50	9. 3.50	9. 3.50	8. 3.50	8. 3.50	8. 3.50	8. 3.50	8. 3.50	3. 3.50
2 COMBINED AT	CON4	.17	1	FLOW TIME	195. 3.67	190. 3.67	182. 3.67	173. 3.67	170. 3.67	168. 3.67	166. 3.67	164. 3.67	66. 3.75
HYDROGRAPH AT	ON5	.01	1	FLOW TIME	18. 3.50	18. 3.58	17. 3.58	16. 3.58	16. 3.58	16. 3.58	16. 3.58	16. 3.58	7. 3.58
HYDROGRAPH AT	57B-3C	.01	1	FLOW TIME	11. 3.58	10. 3.58	10. 3.58	10. 3.58	9. 3.58	9. 3.58	9. 3.58	9. 3.58	4. 3.58
HYDROGRAPH AT	ON6	.00	1	FLOW TIME	8. 3.50	8. 3.50	8. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	4. 3.50
2 COMBINED AT	CON6	.01	1	FLOW TIME	18. 3.50	18. 3.50	17. 3.50	16. 3.50	16. 3.50	16. 3.50	16. 3.50	16. 3.50	8. 3.50
2 COMBINED AT	CCON6	.03	1	FLOW TIME	36. 3.50	36. 3.50	34. 3.50	33. 3.50	32. 3.50	32. 3.50	32. 3.50	31. 3.50	14. 3.50
ROUTED TO	RCCON6	.03	1	FLOW TIME	34. 3.67	33. 3.67	32. 3.67	31. 3.67	30. 3.67	30. 3.67	30. 3.67	29. 3.67	14. 3.67
HYDROGRAPH AT	ON8	.02	1	FLOW TIME	27. 3.50	26. 3.50	25. 3.50	24. 3.50	23. 3.50	23. 3.50	23. 3.50	22. 3.50	9. 3.50
2 COMBINED AT	CON8	.04	1	FLOW TIME	54. 3.58	53. 3.58	50. 3.58	48. 3.58	47. 3.58	47. 3.58	46. 3.58	46. 3.58	19. 3.67
HYDROGRAPH AT	SW11	.59	1	FLOW TIME	759. 3.75	743. 3.75	717. 3.75	691. 3.75	680. 3.75	673. 3.75	668. 3.75	660. 3.75	330. 3.75
ROUTED TO	RSW11	.59	1	FLOW TIME	754. 3.75	738. 3.75	712. 3.75	686. 3.75	676. 3.75	668. 3.75	663. 3.75	655. 3.75	325. 3.75
HYDROGRAPH AT	SW17	.36	1	FLOW TIME	479. 3.67	469. 3.67	452. 3.67	436. 3.67	429. 3.67	424. 3.67	421. 3.67	416. 3.67	205. 3.67
2 COMBINED AT	CSW17	.94	1	FLOW TIME	1221. 3.75	1196. 3.75	1153. 3.75	1111. 3.75	1095. 3.75	1083. 3.75	1075. 3.75	1061. 3.75	530. 3.75
ROUTED TO	RCSW17	.94	1	FLOW TIME	1211. 3.75	1186. 3.75	1143. 3.75	1101. 3.75	1083. 3.75	1073. 3.75	1063. 3.75	1051. 3.75	521. 3.75
HYDROGRAPH AT	SW18	.41	1	FLOW TIME	519. 3.67	507. 3.67	489. 3.67	470. 3.67	463. 3.67	457. 3.67	454. 3.67	448. 3.67	215. 3.75
2 COMBINED AT	CSW18	1.35	1	FLOW TIME	1718. 3.75	1682. 3.75	1622. 3.75	1562. 3.75	1537. 3.75	1521. 3.75	1508. 3.75	1490. 3.75	736. 3.75
ROUTED TO	RCSW18	1.35	1	FLOW TIME	1610. 3.92	1576. 3.92	1520. 3.92	1464. 3.92	1441. 3.92	1426. 3.92	1414. 3.92	1397. 3.92	690. 3.92
HYDROGRAPH AT	12A	.39	1	FLOW TIME	576. 3.67	565. 3.67	547. 3.67	529. 3.67	521. 3.67	516. 3.67	513. 3.67	507. 3.67	272. 3.67
2 COMBINED AT	C12A	1.74	1	FLOW	2046.	2003.	1932.	1861.	1832.	1813.	1798.	1776.	881.

				TIME	3.83	EXISTING.OUT 3.83	3.83	3.83	3.83	3.83	3.83	3.83	3.83
ROUTED TO +	RC12A	1.74	1	FLOW TIME	2025. 3.92	1983. 3.92	1913. 3.92	1843. 3.92	1815. 3.92	1796. 3.92	1782. 3.92	1760. 3.92	880. 3.92
HYDROGRAPH AT +	12B	.26	1	FLOW TIME	387. 3.67	380. 3.67	367. 3.67	355. 3.67	350. 3.67	347. 3.67	344. 3.67	340. 3.67	182. 3.67
2 COMBINED AT +	C12B	2.00	1	FLOW TIME	2259. 3.83	2212. 3.83	2134. 3.83	2056. 3.83	2024. 3.83	2002. 3.83	1987. 3.83	1962. 3.83	990. 3.92
HYDROGRAPH AT +	57B-2A	.01	1	FLOW TIME	14. 3.58	14. 3.58	13. 3.58	13. 3.58	13. 3.58	13. 3.58	12. 3.58	12. 3.58	6. 3.58
HYDROGRAPH AT +	57B-3F	.01	1	FLOW TIME	17. 3.58	17. 3.58	16. 3.58	16. 3.58	15. 3.58	15. 3.58	15. 3.58	15. 3.58	7. 3.58
HYDROGRAPH AT +	57B-3E	.03	1	FLOW TIME	32. 3.67	31. 3.67	30. 3.67	29. 3.67	29. 3.67	28. 3.67	28. 3.67	28. 3.67	13. 3.67
HYDROGRAPH AT +	ON9	.04	1	FLOW TIME	41. 3.67	40. 3.67	38. 3.67	36. 3.67	36. 3.67	35. 3.67	35. 3.67	34. 3.67	14. 3.67
5 COMBINED AT +	CON9	2.09	1	FLOW TIME	2330. 3.83	2281. 3.83	2200. 3.83	2120. 3.83	2087. 3.83	2064. 3.83	2048. 3.83	2023. 3.83	1012. 3.92
ROUTED TO +	RCON9	2.09	1	FLOW TIME	2307. 3.92	2259. 3.92	2181. 3.92	2103. 3.92	2071. 3.92	2048. 3.92	2032. 3.92	2007. 3.92	1012. 3.92
HYDROGRAPH AT +	57B-3G	.00	1	FLOW TIME	4. 3.50	4. 3.50	4. 3.50	4. 3.50	4. 3.50	4. 3.50	3. 3.50	3. 3.50	2. 3.50
HYDROGRAPH AT +	57B-2B	.00	1	FLOW TIME	8. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	3. 3.50
HYDROGRAPH AT +	57B-2C	.00	1	FLOW TIME	5. 3.50	5. 3.50	4. 3.50	4. 3.50	4. 3.50	4. 3.50	4. 3.50	4. 3.50	2. 3.50
HYDROGRAPH AT +	ON10	.02	1	FLOW TIME	24. 3.50	23. 3.50	22. 3.50	21. 3.50	21. 3.50	21. 3.50	21. 3.50	20. 3.50	8. 3.50
5 COMBINED AT +	CON10	2.12	1	FLOW TIME	2314. 3.92	2266. 3.92	2188. 3.92	2110. 3.92	2077. 3.92	2055. 3.92	2039. 3.92	2014. 3.92	1015. 3.92
2 COMBINED AT +	CCON10	2.16	1	FLOW TIME	2335. 3.92	2286. 3.92	2208. 3.92	2128. 3.92	2096. 3.92	2073. 3.92	2057. 3.92	2032. 3.92	1025. 3.92
ROUTED TO +	RCCON10	2.16	1	FLOW TIME	2331. 3.92	2283. 3.92	2206. 3.92	2124. 3.92	2092. 3.92	2069. 3.92	2052. 3.92	2028. 3.92	1015. 3.92
HYDROGRAPH AT +	ON11	.02	1	FLOW TIME	19. 3.58	18. 3.58	17. 3.58	17. 3.58	16. 3.58	16. 3.58	16. 3.58	16. 3.58	7. 3.58
2 COMBINED AT +	CON11	2.18	1	FLOW TIME	2336. 3.92	2288. 3.92	2210. 3.92	2128. 3.92	2096. 3.92	2074. 3.92	2056. 3.92	2032. 3.92	1017. 3.92
2 COMBINED AT +	CCON11	2.35	1	FLOW TIME	2443. 3.92	2393. 3.92	2312. 3.92	2227. 3.92	2193. 3.92	2170. 3.92	2152. 3.92	2126. 3.92	1065. 3.92
HYDROGRAPH AT +	57B-2D	.01	1	FLOW TIME	16. 3.58	15. 3.58	15. 3.58	14. 3.58	14. 3.58	14. 3.58	14. 3.58	14. 3.58	3.58
HYDROGRAPH AT +	57B-2E	.02	1	FLOW TIME	42. 3.50	41. 3.50	40. 3.50	38. 3.50	38. 3.50	37. 3.50	37. 3.50	37. 3.50	19. 3.50
2 COMBINED AT +	C57B-2E	.03	1	FLOW TIME	56. 3.50	55. 3.50	53. 3.50	52. 3.50	51. 3.50	50. 3.50	50. 3.50	49. 3.50	26. 3.50
HYDROGRAPH AT +	57B-2G1	.00	1	FLOW TIME	5. 3.50	5. 3.50	5. 3.50	5. 3.50	5. 3.50	4. 3.50	4. 3.50	4. 3.50	2. 3.50
HYDROGRAPH AT +	ON12	.02	1	FLOW TIME	23. 3.58	23. 3.58	22. 3.58	21. 3.58	20. 3.58	20. 3.58	20. 3.58	20. 3.58	8. 3.58
3 COMBINED AT +	CON12	.05	1	FLOW TIME	83. 3.50	81. 3.50	78. 3.50	75. 3.50	74. 3.50	73. 3.50	73. 3.50	72. 3.50	36. 3.58
HYDROGRAPH AT +	57B-2G2	.01	1	FLOW TIME	12. 3.50	11. 3.50	11. 3.50	11. 3.50	10. 3.50	10. 3.50	10. 3.50	10. 3.50	5. 3.50
HYDROGRAPH AT +	ON13	.02	1	FLOW TIME	23. 3.58	23. 3.58	22. 3.58	21. 3.58	21. 3.58	20. 3.58	20. 3.58	20. 3.58	8. 3.58
3 COMBINED AT +	CON13	.08	1	FLOW	118. Page 15	115.	111.	107.	105.	104.	103.	101.	49.

				TIME	3.50	EXISTING. OUT 3.50	3.50	3.50	3.50	3.50	3.50	3.50	3.58
HYDROGRAPH AT	57B-2F	.09	1	FLOW TIME	147. 3.58	145. 3.58	140. 3.58	135. 3.58	133. 3.58	132. 3.58	131. 3.58	129. 3.58	69. 3.58
HYDROGRAPH AT	57B-2H2	.02	1	FLOW TIME	21. 3.58	21. 3.58	20. 3.58	19. 3.58	19. 3.58	19. 3.58	19. 3.58	18. 3.58	9. 3.58
HYDROGRAPH AT	ON14	.01	1	FLOW TIME	6. 3.58	5. 3.58	5. 3.58	5. 3.58	5. 3.58	5. 3.58	5. 3.58	5. 3.58	2. 3.67
3 COMBINED AT	CON14	.11	1	FLOW TIME	174. 3.58	171. 3.58	165. 3.58	159. 3.58	157. 3.58	155. 3.58	154. 3.58	152. 3.58	79. 3.58
ROUTED TO	RCON14	.11	1	FLOW TIME	166. 3.67	163. 3.67	158. 3.67	156. 3.67	153. 3.67	152. 3.67	151. 3.67	146. 3.67	79. 3.67
HYDROGRAPH AT	57B-2I	.01	1	FLOW TIME	12. 3.50	11. 3.50	11. 3.50	10. 3.50	10. 3.50	10. 3.50	10. 3.50	10. 3.50	5. 3.50
HYDROGRAPH AT	57B-2H1	.03	1	FLOW TIME	32. 3.75	31. 3.75	30. 3.75	29. 3.75	29. 3.75	28. 3.75	28. 3.75	28. 3.75	13. 3.75
HYDROGRAPH AT	ON15	.04	1	FLOW TIME	42. 3.58	41. 3.58	40. 3.58	38. 3.58	37. 3.58	37. 3.58	36. 3.58	36. 3.58	15. 3.58
5 COMBINED AT	CON15	.26	1	FLOW TIME	346. 3.58	338. 3.58	326. 3.58	314. 3.58	309. 3.58	306. 3.58	303. 3.58	298. 3.58	142. 3.58
HYDROGRAPH AT	ON16	.02	1	FLOW TIME	23. 3.50	23. 3.50	22. 3.50	21. 3.50	20. 3.50	20. 3.50	20. 3.50	20. 3.50	8. 3.50
2 COMBINED AT	CON16	.28	1	FLOW TIME	367. 3.58	359. 3.58	345. 3.58	333. 3.58	327. 3.58	324. 3.58	321. 3.58	316. 3.58	150. 3.58
ROUTED TO	RCON16	.28	1	FLOW TIME	354. 3.58	346. 3.58	333. 3.58	320. 3.58	315. 3.58	311. 3.58	309. 3.58	303. 3.58	149. 3.67
HYDROGRAPH AT	ON17	.01	1	FLOW TIME	20. 3.50	20. 3.50	19. 3.50	18. 3.50	18. 3.50	17. 3.50	17. 3.50	17. 3.50	7. 3.50
2 COMBINED AT	CON17	.29	1	FLOW TIME	368. 3.58	360. 3.58	347. 3.58	333. 3.58	328. 3.58	323. 3.58	321. 3.58	316. 3.58	153. 3.67
ROUTED TO	RCON17	.29	1	FLOW TIME	356. 3.67	350. 3.67	337. 3.67	328. 3.67	321. 3.67	319. 3.67	318. 3.67	309. 3.67	149. 3.67
HYDROGRAPH AT	57B-4A	.01	1	FLOW TIME	8. 3.50	8. 3.50	8. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	3. 3.58
3 COMBINED AT	CCON17	2.65	1	FLOW TIME	2716. 3.83	2660. 3.83	2567. 3.83	2472. 3.83	2434. 3.83	2407. 3.83	2388. 3.83	2359. 3.83	1171. 3.92
HYDROGRAPH AT	ON21	.03	1	FLOW TIME	34. 3.58	33. 3.58	32. 3.67	30. 3.67	30. 3.67	29. 3.67	29. 3.67	29. 3.67	12. 3.67
2 COMBINED AT	CON21	2.68	1	FLOW TIME	2740. 3.83	2683. 3.83	2589. 3.83	2493. 3.83	2455. 3.83	2427. 3.83	2408. 3.83	2378. 3.83	1177. 3.92
HYDROGRAPH AT	13B-1	.25	1	FLOW TIME	354. 3.67	347. 3.67	336. 3.67	325. 3.67	321. 3.67	318. 3.67	315. 3.67	312. 3.67	169. 3.75
ROUTED TO	RC13B-1	.25	1	FLOW TIME	354. 3.75	347. 3.75	336. 3.75	324. 3.75	320. 3.75	317. 3.75	314. 3.83	311. 3.83	171. 3.83
HYDROGRAPH AT	13B-2	.22	1	FLOW TIME	310. 3.67	304. 3.67	294. 3.67	283. 3.67	279. 3.67	277. 3.67	274. 3.67	271. 3.67	140. 3.67
2 COMBINED AT	C13B-2	.47	1	FLOW TIME	634. 3.75	622. 3.75	602. 3.75	581. 3.75	573. 3.75	567. 3.75	563. 3.75	557. 3.75	294. 3.75
ROUTED TO	RC13B-2	.47	1	FLOW TIME	641. 3.83	628. 3.83	607. 3.83	586. 3.83	578. 3.83	572. 3.83	568. 3.83	561. 3.83	295. 3.92
HYDROGRAPH AT	19A	.25	1	FLOW TIME	318. 3.75	312. 3.75	301. 3.75	291. 3.75	287. 3.75	284. 3.75	282. 3.75	278. 3.75	144. 3.75
ROUTED TO	R19A	.25	1	FLOW TIME	319. 3.92	313. 3.92	302. 3.92	292. 3.92	288. 3.92	285. 3.92	283. 3.92	280. 3.92	146. 3.92
HYDROGRAPH AT	13A-1	.22	1	FLOW TIME	308. 3.75	303. 3.75	293. 3.75	283. 3.75	279. 3.75	277. 3.75	275. 3.75	272. 3.75	147. 3.75
2 COMBINED AT	C13A-1	.48	1	FLOW	595. 3.75	583. 3.75	564. 3.75	545. 3.75	537. 3.75	532. 3.75	528. 3.75	522. 3.75	273. 3.75

				TIME	3.83	EXISTING.OUT 3.83		3.83	3.83	3.83	3.83	3.83	3.83	3.83
ROUTED TO +	RC13A-1	.48	1	FLOW TIME	581. 3.92	569. 3.92	551. 3.92	532. 3.92	524. 3.92	519. 3.92	515. 3.92	509. 3.92	268. 3.92	
HYDROGRAPH AT +	13A-2	.19	1	FLOW TIME	272. 3.67	267. 3.67	258. 3.67	249. 3.67	246. 3.67	243. 3.67	241. 3.67	238. 3.67	124. 3.67	
2 COMBINED AT +	C13A-2	.66	1	FLOW TIME	782. 3.83	766. 3.83	740. 3.83	715. 3.83	704. 3.83	697. 3.83	692. 3.83	684. 3.83	354. 3.83	
ROUTED TO +	RC13A-2	.66	1	FLOW TIME	781. 3.92	765. 3.92	738. 3.92	712. 3.92	702. 3.92	694. 3.92	689. 3.92	681. 3.92	354. 4.00	
HYDROGRAPH AT +	PIC-C	.24	1	FLOW TIME	280. 3.83	274. 3.83	265. 3.83	256. 3.83	252. 3.83	250. 3.83	248. 3.83	245. 3.83	129. 3.83	
2 COMBINED AT +	CPIC-C	.91	1	FLOW TIME	1041. 3.92	1020. 3.92	985. 3.92	951. 3.92	937. 3.92	927. 3.92	920. 3.92	909. 3.92	462. 3.92	
ROUTED TO +	RCPIC-C	.91	1	FLOW TIME	1030. 3.92	1009. 3.92	975. 3.92	940. 3.92	922. 3.92	915. 3.92	908. 3.92	896. 3.92	461. 4.00	
HYDROGRAPH AT +	PIC-A	.36	1	FLOW TIME	356. 3.92	349. 3.92	338. 3.92	326. 3.92	322. 3.92	318. 3.92	316. 3.92	312. 3.92	165. 3.92	
2 COMBINED AT +	CPIC-A	1.27	1	FLOW TIME	1386. 3.92	1359. 3.92	1313. 3.92	1266. 3.92	1243. 3.92	1233. 3.92	1224. 3.92	1208. 3.92	625. 4.00	
2 COMBINED AT +	CCPIC-A	1.73	1	FLOW TIME	1997. 3.92	1959. 3.92	1895. 3.92	1830. 3.92	1800. 3.92	1785. 3.92	1772. 3.92	1750. 3.92	900. 4.00	
HYDROGRAPH AT +	ON18	.03	1	FLOW TIME	31. 3.67	30. 3.67	29. 3.67	27. 3.67	27. 3.67	26. 3.67	26. 3.67	26. 3.67	10. 3.67	
2 COMBINED AT +	CON18	1.76	1	FLOW TIME	2015. 3.92	1977. 3.92	1912. 3.92	1846. 3.92	1816. 3.92	1801. 3.92	1788. 3.92	1765. 3.92	906. 4.00	
HYDROGRAPH AT +	57B-1A	.04	1	FLOW TIME	54. 3.58	53. 3.58	51. 3.58	48. 3.58	48. 3.58	47. 3.58	47. 3.58	46. 3.58	20. 3.58	
HYDROGRAPH AT +	57B-1B	.03	1	FLOW TIME	51. 3.58	50. 3.58	49. 3.58	47. 3.58	47. 3.58	46. 3.58	46. 3.58	45. 3.58	25. 3.58	
HYDROGRAPH AT +	ON19	.01	1	FLOW TIME	12. 3.50	12. 3.50	12. 3.50	11. 3.50	11. 3.50	11. 3.50	11. 3.50	10. 3.50	4. 3.50	
4 COMBINED AT +	CON19	1.85	1	FLOW TIME	2059. 3.92	2020. 3.92	1954. 3.92	1886. 3.92	1856. 3.92	1840. 3.92	1826. 3.92	1804. 3.92	923. 3.92	
ROUTED TO +	RCON19	1.85	1	FLOW TIME	2045. 3.92	2006. 3.92	1941. 3.92	1871. 3.92	1840. 3.92	1824. 3.92	1811. 3.92	1788. 3.92	922. 4.00	
HYDROGRAPH AT +	57B-1C	.00	1	FLOW TIME	2. 3.50	2. 3.50	2. 3.50	2. 3.50	2. 3.50	2. 3.50	2. 3.50	2. 3.50	1. 3.50	
HYDROGRAPH AT +	ON20	.01	1	FLOW TIME	12. 3.58	12. 3.58	11. 3.58	11. 3.58	10. 3.58	10. 3.58	10. 3.58	10. 3.58	4. 3.58	
3 COMBINED AT +	CON20	1.86	1	FLOW TIME	2048. 3.92	2009. 3.92	1944. 3.92	1874. 3.92	1843. 3.92	1827. 3.92	1814. 3.92	1791. 3.92	923. 4.00	
ROUTED TO +	RCON20	1.86	1	FLOW TIME	2040. 3.92	2001. 3.92	1935. 3.92	1865. 3.92	1834. 3.92	1818. 3.92	1805. 3.92	1781. 3.92	920. 4.00	
HYDROGRAPH AT +	57B-4B	.01	1	FLOW TIME	24. 3.50	24. 3.50	23. 3.50	22. 3.50	22. 3.50	22. 3.50	22. 3.50	22. 3.50	13. 3.50	
HYDROGRAPH AT +	57B-4C	.01	1	FLOW TIME	23. 3.50	22. 3.50	22. 3.50	21. 3.50	21. 3.50	21. 3.50	21. 3.50	20. 3.50	12. 3.58	
2 COMBINED AT +	C57B-4C	.02	1	FLOW TIME	47. 3.50	46. 3.50	45. 3.50	43. 3.50	43. 3.50	43. 3.50	42. 3.50	42. 3.50	25. 3.50	
HYDROGRAPH AT +	ON22	.01	1	FLOW TIME	18. 3.50	17. 3.50	16. 3.50	16. 3.50	15. 3.50	15. 3.50	15. 3.50	15. 3.50	6. 3.50	
4 COMBINED AT +	CON22	4.58	1	FLOW TIME	4729. 3.92	4636. 3.92	4481. 3.92	4318. 3.92	4251. 3.92	4209. 3.92	4177. 3.92	4125. 3.92	2065. 3.92	
HYDROGRAPH AT +	57B-1	.05	1	FLOW TIME	80. 3.58	79. 3.58	76. 3.58	74. 3.58	73. 3.58	72. 3.58	72. 3.58	71. 3.58	40. 3.58	
HYDROGRAPH AT +	57B-3	.05	1	FLOW	63. 3.58	62. 3.58	60. 3.58	58. 3.58	57. 3.58	56. 3.58	56. 3.58	55. 3.58	28. 3.58	

				TIME	3.67	EXISTING.OUT 3.67	3.67	3.67	3.67	3.67	3.67	3.67	3.67	3.67
HYDROGRAPH AT														
+	57B-4	.13	1	FLOW TIME	202. 3.58	198. 3.58	192. 3.58	186. 3.58	184. 3.58	182. 3.58	181. 3.58	179. 3.58	101. 3.58	
2 COMBINED AT														
+	C57B-4	.18	1	FLOW TIME	259. 3.58	254. 3.58	246. 3.67	238. 3.67	235. 3.67	233. 3.67	232. 3.67	229. 3.67	127. 3.67	
HYDROGRAPH AT														
+	PIC-B	.44	1	FLOW TIME	442. 3.92	433. 3.92	419. 3.92	405. 3.92	399. 3.92	395. 3.92	392. 3.92	388. 3.92	205. 3.92	
ROUTED TO														
+	RPIC-B	.44	1	FLOW TIME	439. 3.92	431. 3.92	416. 3.92	402. 3.92	396. 3.92	392. 3.92	390. 3.92	385. 3.92	202. 3.92	
4 COMBINED AT														
+	CC57B-4	5.25	1	FLOW TIME	5339. 3.92	5234. 3.92	5060. 3.92	4878. 3.92	4803. 3.92	4756. 3.92	4720. 3.92	4662. 3.92	2354. 3.92	

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING (FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)										
ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL PEAK TIME TO PEAK		VOLUME	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)	
FOR PLAN = 1	RATIO=	.00								
RCON1	MANE	5.00	85.62	225.00	1.50	5.00	85.62	225.00	1.50	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5242E+01 EXCESS= .0000E+00 OUTFLOW= .5262E+01 BASIN STORAGE= .6505E-02 PERCENT ERROR= -.5										
FOR PLAN = 1	RATIO=	.00								
RCON1	MANE	5.00	83.65	225.00	1.47	5.00	83.65	225.00	1.47	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5111E+01 EXCESS= .0000E+00 OUTFLOW= .5131E+01 BASIN STORAGE= .6457E-02 PERCENT ERROR= -.5										
FOR PLAN = 1	RATIO=	.00								
RCON1	MANE	5.00	80.35	225.00	1.40	5.00	80.35	225.00	1.40	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4894E+01 EXCESS= .0000E+00 OUTFLOW= .4914E+01 BASIN STORAGE= .6374E-02 PERCENT ERROR= -.5										
FOR PLAN = 1	RATIO=	.00								
RCON1	MANE	5.00	77.02	225.00	1.34	5.00	77.02	225.00	1.34	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4680E+01 EXCESS= .0000E+00 OUTFLOW= .4699E+01 BASIN STORAGE= .6290E-02 PERCENT ERROR= -.5										
FOR PLAN = 1	RATIO=	.00								
RCON1	MANE	5.00	75.69	225.00	1.32	5.00	75.69	225.00	1.32	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4594E+01 EXCESS= .0000E+00 OUTFLOW= .4613E+01 BASIN STORAGE= .6256E-02 PERCENT ERROR= -.5										
FOR PLAN = 1	RATIO=	.00								
RCON1	MANE	5.00	74.75	225.00	1.30	5.00	74.75	225.00	1.30	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4535E+01 EXCESS= .0000E+00 OUTFLOW= .4553E+01 BASIN STORAGE= .6232E-02 PERCENT ERROR= -.5										
FOR PLAN = 1	RATIO=	.00								
RCON1	MANE	5.00	74.08	225.00	1.29	5.00	74.08	225.00	1.29	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4492E+01 EXCESS= .0000E+00 OUTFLOW= .4511E+01 BASIN STORAGE= .6038E-02 PERCENT ERROR= -.5										
FOR PLAN = 1	RATIO=	.00								
RCON1	MANE	5.00	73.00	225.00	1.27	5.00	73.00	225.00	1.27	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4425E+01 EXCESS= .0000E+00 OUTFLOW= .4442E+01 BASIN STORAGE= .6011E-02 PERCENT ERROR= -.5										
FOR PLAN = 1	RATIO=	.00								
RCON1	MANE	4.00	31.17	228.00	.55	5.00	30.06	230.00	.54	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1896E+01 EXCESS= .0000E+00 OUTFLOW= .1909E+01 BASIN STORAGE= .5556E-02 PERCENT ERROR= -1.0										
FOR PLAN = 1	RATIO=	.00								
RCON6	MANE	4.25	34.85	216.75	1.61	5.00	33.88	220.00	1.61	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2157E+01 EXCESS= .0000E+00 OUTFLOW= .2162E+01 BASIN STORAGE= .2734E-02 PERCENT ERROR= -.3										
FOR PLAN = 1	RATIO=	.00								
RCON6	MANE	4.25	34.03	216.75	1.58	5.00	33.16	220.00	1.57	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2106E+01 EXCESS= .0000E+00 OUTFLOW= .2111E+01 BASIN STORAGE= .2708E-02 PERCENT ERROR= -.3										
FOR PLAN = 1	RATIO=	.00								
RCON6	MANE	4.25	32.67	216.75	1.51	5.00	31.96	220.00	1.51	

					EXISTING	OUT														
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.2022E+01	EXCESS=	.0000E+00	OUTFLOW=	.2026E+01	BASIN STORAGE=	.2664E-02	PERCENT ERROR=	- .3											
FOR PLAN = 1	RATIO=	.00																		
RCCON6	MANE	4.25	31.31	216.75	1.45	5.00	30.75	220.00	1.45											
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.1938E+01	EXCESS=	.0000E+00	OUTFLOW=	.1942E+01	BASIN STORAGE=	.2619E-02	PERCENT ERROR=	- .4											
FOR PLAN = 1	RATIO=	.00																		
RCCON6	MANE	4.25	30.77	216.75	1.43	5.00	30.27	220.00	1.42											
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.1905E+01	EXCESS=	.0000E+00	OUTFLOW=	.1909E+01	BASIN STORAGE=	.2601E-02	PERCENT ERROR=	- .4											
FOR PLAN = 1	RATIO=	.00																		
RCCON6	MANE	4.25	30.39	216.75	1.41	5.00	29.93	220.00	1.41											
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.1881E+01	EXCESS=	.0000E+00	OUTFLOW=	.1886E+01	BASIN STORAGE=	.2588E-02	PERCENT ERROR=	- .4											
FOR PLAN = 1	RATIO=	.00																		
RCCON6	MANE	4.25	30.11	216.75	1.40	5.00	29.69	220.00	1.39											
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.1865E+01	EXCESS=	.0000E+00	OUTFLOW=	.1869E+01	BASIN STORAGE=	.2579E-02	PERCENT ERROR=	- .4											
FOR PLAN = 1	RATIO=	.00																		
RCCON6	MANE	4.25	29.68	216.75	1.38	5.00	29.30	220.00	1.37											
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.1838E+01	EXCESS=	.0000E+00	OUTFLOW=	.1842E+01	BASIN STORAGE=	.2564E-02	PERCENT ERROR=	- .4											
FOR PLAN = 1	RATIO=	.00																		
RCCON6	MANE	3.75	14.36	221.25	.63	5.00	14.02	220.00	.63											
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.8405E+00	EXCESS=	.0000E+00	OUTFLOW=	.8424E+00	BASIN STORAGE=	.2039E-02	PERCENT ERROR=	- .5											
FOR PLAN = 1	RATIO=	.00																		
RSW11	MANE	1.02	755.16	226.24	2.08	5.00	753.82	225.00	2.08											
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.6522E+02	EXCESS=	.0000E+00	OUTFLOW=	.6522E+02	BASIN STORAGE=	.1654E-02	PERCENT ERROR=	.0											
FOR PLAN = 1	RATIO=	.00																		
RSW11	MANE	1.03	740.95	226.07	2.03	5.00	738.42	225.00	2.03											
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.6380E+02	EXCESS=	.0000E+00	OUTFLOW=	.6381E+02	BASIN STORAGE=	.1696E-02	PERCENT ERROR=	.0											
FOR PLAN = 1	RATIO=	.00																		
RSW11	MANE	1.05	714.15	226.19	1.96	5.00	712.14	225.00	1.96											
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.6145E+02	EXCESS=	.0000E+00	OUTFLOW=	.6145E+02	BASIN STORAGE=	.1622E-02	PERCENT ERROR=	.0											
FOR PLAN = 1	RATIO=	.00																		
RSW11	MANE	1.06	686.99	226.38	1.88	5.00	685.95	225.00	1.88											
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.5911E+02	EXCESS=	.0000E+00	OUTFLOW=	.5911E+02	BASIN STORAGE=	.1763E-02	PERCENT ERROR=	.0											
FOR PLAN = 1	RATIO=	.00																		
RSW11	MANE	1.07	677.33	225.62	1.85	5.00	675.73	225.00	1.85											
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.5818E+02	EXCESS=	.0000E+00	OUTFLOW=	.5818E+02	BASIN STORAGE=	.1832E-02	PERCENT ERROR=	.0											
FOR PLAN = 1	RATIO=	.00																		
RSW11	MANE	1.07	669.72	225.52	1.83	5.00	668.38	225.00	1.83											
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.5752E+02	EXCESS=	.0000E+00	OUTFLOW=	.5752E+02	BASIN STORAGE=	.1613E-02	PERCENT ERROR=	.0											
FOR PLAN = 1	RATIO=	.00																		
RSW11	MANE	1.08	665.29	226.22	1.82	5.00	663.31	225.00	1.82											
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.5706E+02	EXCESS=	.0000E+00	OUTFLOW=	.5706E+02	BASIN STORAGE=	.1791E-02	PERCENT ERROR=	.0											
FOR PLAN = 1	RATIO=	.00																		
RSW11	MANE	1.08	656.69	226.27	1.79	5.00	654.91	225.00	1.79											
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.5631E+02	EXCESS=	.0000E+00	OUTFLOW=	.5632E+02	BASIN STORAGE=	.1761E-02	PERCENT ERROR=	.0											
FOR PLAN = 1	RATIO=	.00																		
RSW11	MANE	1.43	328.10	225.73	.88	5.00	324.89	225.00	.88											
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.2754E+02	EXCESS=	.0000E+00	OUTFLOW=	.2754E+02	BASIN STORAGE=	.1787E-02	PERCENT ERROR=	.0											
FOR PLAN = 1	RATIO=	.00																		
RCSW17	MANE	1.65	1211.98	225.57	2.06	5.00	1210.68	225.00	2.06											

				EXISTING	OUT						
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.1040E+03	EXCESS=	.0000E+00	OUTFLOW=	.1040E+03	BASIN STORAGE=	.3928E-02	PERCENT ERROR=	.0	
FOR PLAN	= 1	RATIO=	.00								
RCSW17	MANE		1.66	1187.90	225.78	2.02	5.00	1185.71	225.00	2.02	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.1018E+03	EXCESS=	.0000E+00	OUTFLOW=	.1018E+03	BASIN STORAGE=	.3507E-02	PERCENT ERROR=	.0	
FOR PLAN	= 1	RATIO=	.00								
RCSW17	MANE		1.68	1144.91	225.68	1.94	5.00	1143.40	225.00	1.94	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9799E+02	EXCESS=	.0000E+00	OUTFLOW=	.9800E+02	BASIN STORAGE=	.3522E-02	PERCENT ERROR=	.0	
FOR PLAN	= 1	RATIO=	.00								
RCSW17	MANE		1.71	1102.37	225.64	1.87	5.00	1101.22	225.00	1.87	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9424E+02	EXCESS=	.0000E+00	OUTFLOW=	.9424E+02	BASIN STORAGE=	.3477E-02	PERCENT ERROR=	.0	
FOR PLAN	= 1	RATIO=	.00								
RCSW17	MANE		1.72	1087.77	227.00	1.84	5.00	1083.30	225.00	1.84	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9278E+02	EXCESS=	.0000E+00	OUTFLOW=	.9279E+02	BASIN STORAGE=	.3927E-02	PERCENT ERROR=	.0	
FOR PLAN	= 1	RATIO=	.00								
RCSW17	MANE		1.73	1077.08	226.26	1.82	5.00	1072.79	225.00	1.82	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9172E+02	EXCESS=	.0000E+00	OUTFLOW=	.9173E+02	BASIN STORAGE=	.3817E-02	PERCENT ERROR=	.0	
FOR PLAN	= 1	RATIO=	.00								
RCSW17	MANE		1.73	1069.06	226.95	1.81	5.00	1062.80	225.00	1.81	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9100E+02	EXCESS=	.0000E+00	OUTFLOW=	.9101E+02	BASIN STORAGE=	.3937E-02	PERCENT ERROR=	.0	
FOR PLAN	= 1	RATIO=	.00								
RCSW17	MANE		1.74	1055.75	226.36	1.78	5.00	1050.97	225.00	1.78	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.8979E+02	EXCESS=	.0000E+00	OUTFLOW=	.8980E+02	BASIN STORAGE=	.3511E-02	PERCENT ERROR=	.0	
FOR PLAN	= 1	RATIO=	.00								
RCSW17	MANE		2.30	524.06	227.64	.87	5.00	520.91	225.00	.87	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.4386E+02	EXCESS=	.0000E+00	OUTFLOW=	.4387E+02	BASIN STORAGE=	.3897E-02	PERCENT ERROR=	.0	
FOR PLAN	= 1	RATIO=	.00								
RCON9	MANE		1.67	2325.51	231.44	2.07	5.00	2306.80	235.00	2.07	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2301E+03	EXCESS=	.0000E+00	OUTFLOW=	.2301E+03	BASIN STORAGE=	.3123E-02	PERCENT ERROR=	.0	
FOR PLAN	= 1	RATIO=	.00								
RCON9	MANE		1.68	2279.65	231.56	2.02	5.00	2258.94	235.00	2.02	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2252E+03	EXCESS=	.0000E+00	OUTFLOW=	.2252E+03	BASIN STORAGE=	.2858E-02	PERCENT ERROR=	.0	
FOR PLAN	= 1	RATIO=	.00								
RCON9	MANE		1.70	2197.90	232.94	1.95	5.00	2181.01	235.00	1.95	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2170E+03	EXCESS=	.0000E+00	OUTFLOW=	.2170E+03	BASIN STORAGE=	.2984E-02	PERCENT ERROR=	.0	
FOR PLAN	= 1	RATIO=	.00								
RCON9	MANE		1.72	2118.94	232.70	1.87	5.00	2102.63	235.00	1.88	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2088E+03	EXCESS=	.0000E+00	OUTFLOW=	.2088E+03	BASIN STORAGE=	.3195E-02	PERCENT ERROR=	.0	
FOR PLAN	= 1	RATIO=	.00								
RCON9	MANE		1.73	2088.03	232.28	1.85	5.00	2070.54	235.00	1.85	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2056E+03	EXCESS=	.0000E+00	OUTFLOW=	.2056E+03	BASIN STORAGE=	.2784E-02	PERCENT ERROR=	.0	
FOR PLAN	= 1	RATIO=	.00								
RCON9	MANE		1.74	2062.77	233.22	1.83	5.00	2047.86	235.00	1.83	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2033E+03	EXCESS=	.0000E+00	OUTFLOW=	.2033E+03	BASIN STORAGE=	.2736E-02	PERCENT ERROR=	.0	
FOR PLAN	= 1	RATIO=	.00								
RCON9	MANE		1.75	2050.03	232.14	1.81	5.00	2032.41	235.00	1.81	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2017E+03	EXCESS=	.0000E+00	OUTFLOW=	.2017E+03	BASIN STORAGE=	.2832E-02	PERCENT ERROR=	.0	
FOR PLAN	= 1	RATIO=	.00								
RCON9	MANE		1.75	2021.32	233.22	1.79	5.00	2006.95	235.00	1.79	

										EXISTING.OUT	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1991E+03 EXCESS= .0000E+00										OUTFLOW= .1991E+03	BASIN STORAGE= .2680E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON9 MANE										RATIO= .00 2.26	1012.15 235.03 .89 5.00 1012.06 235.00 .89
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9869E+02 EXCESS= .0000E+00										OUTFLOW= .9869E+02	BASIN STORAGE= .3005E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON10 MANE										RATIO= .00 1.23	2331.18 234.30 2.05 5.00 2330.90 235.00 2.05
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2358E+03 EXCESS= .0000E+00										OUTFLOW= .2358E+03	BASIN STORAGE= .1329E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON10 MANE										RATIO= .00 1.24	2284.11 234.71 2.00 5.00 2283.17 235.00 2.00
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2307E+03 EXCESS= .0000E+00										OUTFLOW= .2307E+03	BASIN STORAGE= .1356E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON10 MANE										RATIO= .00 1.26	2205.80 234.98 1.93 5.00 2205.72 235.00 1.93
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2223E+03 EXCESS= .0000E+00										OUTFLOW= .2223E+03	BASIN STORAGE= .1456E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON10 MANE										RATIO= .00 1.27	2124.92 235.34 1.86 5.00 2124.05 235.00 1.86
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2139E+03 EXCESS= .0000E+00										OUTFLOW= .2139E+03	BASIN STORAGE= .1320E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON10 MANE										RATIO= .00 1.28	2092.66 235.28 1.83 5.00 2091.76 235.00 1.83
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2106E+03 EXCESS= .0000E+00										OUTFLOW= .2106E+03	BASIN STORAGE= .1358E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON10 MANE										RATIO= .00 1.28	2069.86 234.86 1.81 5.00 2069.49 235.00 1.81
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2082E+03 EXCESS= .0000E+00										OUTFLOW= .2082E+03	BASIN STORAGE= .1289E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON10 MANE										RATIO= .00 1.29	2053.30 235.46 1.79 5.00 2052.26 235.00 1.79
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2065E+03 EXCESS= .0000E+00										OUTFLOW= .2065E+03	BASIN STORAGE= .1544E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON10 MANE										RATIO= .00 1.29	2028.73 235.17 1.77 5.00 2028.03 235.00 1.77
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2039E+03 EXCESS= .0000E+00										OUTFLOW= .2039E+03	BASIN STORAGE= .1398E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON10 MANE										RATIO= .00 1.63	1018.69 237.34 .87 5.00 1014.91 235.00 .87
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1007E+03 EXCESS= .0000E+00										OUTFLOW= .1007E+03	BASIN STORAGE= .1586E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON14 MANE										RATIO= .00 4.25	167.38 221.00 1.99 5.00 166.33 220.00 1.99
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1179E+02 EXCESS= .0000E+00										OUTFLOW= .1181E+02	BASIN STORAGE= .2635E-02 PERCENT ERROR= -.1
FOR PLAN = 1 RCON14 MANE										RATIO= .00 4.25	164.16 221.00 1.95 5.00 163.07 220.00 1.95
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1155E+02 EXCESS= .0000E+00										OUTFLOW= .1156E+02	BASIN STORAGE= .2609E-02 PERCENT ERROR= -.1
FOR PLAN = 1 RCON14 MANE										RATIO= .00 4.25	158.77 221.00 1.88 5.00 157.63 220.00 1.88
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1114E+02 EXCESS= .0000E+00										OUTFLOW= .1115E+02	BASIN STORAGE= .2565E-02 PERCENT ERROR= -.1
FOR PLAN = 1 RCON14 MANE										RATIO= .00 4.00	155.50 220.00 1.81 5.00 155.50 220.00 1.81
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1074E+02 EXCESS= .0000E+00										OUTFLOW= .1075E+02	BASIN STORAGE= .2457E-02 PERCENT ERROR= -.1
FOR PLAN = 1 RCON14 MANE										RATIO= .00 4.00	153.27 220.00 1.78 5.00 153.27 220.00 1.79
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1057E+02 EXCESS= .0000E+00										OUTFLOW= .1059E+02	BASIN STORAGE= .2440E-02 PERCENT ERROR= -.1
FOR PLAN = 1 RCON14 MANE										RATIO= .00 4.00	151.72 220.00 1.77 5.00 151.72 220.00 1.77

										EXISTING.OUT	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1046E+02 EXCESS= .0000E+00										OUTFLOW= .1047E+02	BASIN STORAGE= .2427E-02 PERCENT ERROR= -.1
FOR PLAN = 1 RCON14 MANE										RATIO= .00	4.00 150.60 220.00 1.75 5.00 150.60 220.00 1.75
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1038E+02 EXCESS= .0000E+00										OUTFLOW= .1039E+02	BASIN STORAGE= .2418E-02 PERCENT ERROR= -.1
FOR PLAN = 1 RCON14 MANE										RATIO= .00	4.25 146.92 221.00 1.73 5.00 145.67 220.00 1.73
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1024E+02 EXCESS= .0000E+00										OUTFLOW= .1025E+02	BASIN STORAGE= .2466E-02 PERCENT ERROR= -.1
FOR PLAN = 1 RCON14 MANE										RATIO= .00	5.00 78.65 220.00 .88 5.00 78.65 220.00 .88
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5186E+01 EXCESS= .0000E+00										OUTFLOW= .5194E+01	BASIN STORAGE= .2404E-02 PERCENT ERROR= -.2
FOR PLAN = 1 RCON16 MANE										RATIO= .00	1.69 366.03 216.69 1.76 5.00 353.70 215.00 1.76
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2617E+02 EXCESS= .0000E+00										OUTFLOW= .2617E+02	BASIN STORAGE= .1013E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON16 MANE										RATIO= .00	1.71 357.22 216.61 1.72 5.00 345.96 215.00 1.72
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2558E+02 EXCESS= .0000E+00										OUTFLOW= .2558E+02	BASIN STORAGE= .1022E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON16 MANE										RATIO= .00	1.73 339.51 217.68 1.65 5.00 333.18 215.00 1.65
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2459E+02 EXCESS= .0000E+00										OUTFLOW= .2460E+02	BASIN STORAGE= .9731E-03 PERCENT ERROR= .0
FOR PLAN = 1 RCON16 MANE										RATIO= .00	1.75 331.60 216.91 1.59 5.00 319.76 215.00 1.59
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2367E+02 EXCESS= .0000E+00										OUTFLOW= .2367E+02	BASIN STORAGE= .1040E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON16 MANE										RATIO= .00	1.76 323.47 216.34 1.56 5.00 315.26 215.00 1.56
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2327E+02 EXCESS= .0000E+00										OUTFLOW= .2327E+02	BASIN STORAGE= .9851E-03 PERCENT ERROR= .0
FOR PLAN = 1 RCON16 MANE										RATIO= .00	1.77 321.71 217.18 1.55 5.00 310.86 215.00 1.55
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2301E+02 EXCESS= .0000E+00										OUTFLOW= .2301E+02	BASIN STORAGE= .9887E-03 PERCENT ERROR= .0
FOR PLAN = 1 RCON16 MANE										RATIO= .00	1.77 316.30 217.78 1.53 5.00 308.90 215.00 1.53
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2281E+02 EXCESS= .0000E+00										OUTFLOW= .2281E+02	BASIN STORAGE= .1032E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON16 MANE										RATIO= .00	1.78 314.00 217.16 1.51 5.00 303.28 215.00 1.51
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2248E+02 EXCESS= .0000E+00										OUTFLOW= .2249E+02	BASIN STORAGE= .1041E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON16 MANE										RATIO= .00	2.29 150.40 219.44 .72 5.00 148.93 220.00 .72
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1076E+02 EXCESS= .0000E+00										OUTFLOW= .1076E+02	BASIN STORAGE= .1017E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON17 MANE										RATIO= .00	2.23 364.75 218.67 1.74 5.00 356.45 220.00 1.74
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2715E+02 EXCESS= .0000E+00										OUTFLOW= .2716E+02	BASIN STORAGE= .1496E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON17 MANE										RATIO= .00	2.25 357.02 218.14 1.70 5.00 349.64 220.00 1.70
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2653E+02 EXCESS= .0000E+00										OUTFLOW= .2653E+02	BASIN STORAGE= .1654E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON17 MANE										RATIO= .00	2.28 344.14 218.77 1.63 5.00 337.46 220.00 1.63
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2553E+02 EXCESS= .0000E+00										OUTFLOW= .2553E+02	BASIN STORAGE= .1878E-02 PERCENT ERROR= .0
FOR PLAN = 1 RCON17 MANE										RATIO= .00	2.31 330.60 219.64 1.57 5.00 328.28 220.00 1.57

										EXISTING.OUT							
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2455E+02 EXCESS= .0000E+00										OUTFLOW= .2455E+02	BASIN STORAGE= .1844E-02	PERCENT ERROR= .0					
FOR PLAN = 1 RCON17 MANE										RATIO= .00							
										2.32	326.22	218.42	1.54	5.00	321.01	220.00	1.54
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2412E+02 EXCESS= .0000E+00										OUTFLOW= .2413E+02	BASIN STORAGE= .1875E-02	PERCENT ERROR= .0					
FOR PLAN = 1 RCON17 MANE										RATIO= .00							
										2.34	322.39	219.50	1.53	5.00	319.39	220.00	1.53
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2387E+02 EXCESS= .0000E+00										OUTFLOW= .2387E+02	BASIN STORAGE= .1904E-02	PERCENT ERROR= .0					
FOR PLAN = 1 RCON17 MANE										RATIO= .00							
										2.34	319.55	217.66	1.51	5.00	318.05	220.00	1.52
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2367E+02 EXCESS= .0000E+00										OUTFLOW= .2367E+02	BASIN STORAGE= .1665E-02	PERCENT ERROR= .0					
FOR PLAN = 1 RCON17 MANE										RATIO= .00							
										2.36	314.02	219.05	1.49	5.00	309.48	220.00	1.49
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2331E+02 EXCESS= .0000E+00										OUTFLOW= .2331E+02	BASIN STORAGE= .1692E-02	PERCENT ERROR= .0					
FOR PLAN = 1 RCON17 MANE										RATIO= .00							
										3.04	152.09	221.83	.71	5.00	149.27	220.00	.71
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1110E+02 EXCESS= .0000E+00										OUTFLOW= .1110E+02	BASIN STORAGE= .1950E-02	PERCENT ERROR= .0					
FOR PLAN = 1 RC13B-1 MANE										RATIO= .00							
										5.00	353.60	225.00	2.27	5.00	353.60	225.00	2.27
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3020E+02 EXCESS= .0000E+00										OUTFLOW= .3021E+02	BASIN STORAGE= .1566E-02	PERCENT ERROR= -.1					
FOR PLAN = 1 RC13B-1 MANE										RATIO= .00							
										5.00	346.83	225.00	2.23	5.00	346.83	225.00	2.23
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2960E+02 EXCESS= .0000E+00										OUTFLOW= .2961E+02	BASIN STORAGE= .1548E-02	PERCENT ERROR= -.1					
FOR PLAN = 1 RC13B-1 MANE										RATIO= .00							
										5.00	335.54	225.00	2.15	5.00	335.54	225.00	2.15
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2860E+02 EXCESS= .0000E+00										OUTFLOW= .2861E+02	BASIN STORAGE= .1518E-02	PERCENT ERROR= -.1					
FOR PLAN = 1 RC13B-1 MANE										RATIO= .00							
										5.00	324.25	225.00	2.08	5.00	324.25	225.00	2.08
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2760E+02 EXCESS= .0000E+00										OUTFLOW= .2762E+02	BASIN STORAGE= .1489E-02	PERCENT ERROR= -.1					
FOR PLAN = 1 RC13B-1 MANE										RATIO= .00							
										5.00	319.73	225.00	2.05	5.00	319.73	225.00	2.05
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2721E+02 EXCESS= .0000E+00										OUTFLOW= .2722E+02	BASIN STORAGE= .1476E-02	PERCENT ERROR= -.1					
FOR PLAN = 1 RC13B-1 MANE										RATIO= .00							
										5.00	316.57	225.00	2.03	5.00	316.57	225.00	2.03
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2693E+02 EXCESS= .0000E+00										OUTFLOW= .2694E+02	BASIN STORAGE= .1468E-02	PERCENT ERROR= -.1					
FOR PLAN = 1 RC13B-1 MANE										RATIO= .00							
										5.00	314.32	230.00	2.01	5.00	314.32	230.00	2.01
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2673E+02 EXCESS= .0000E+00										OUTFLOW= .2675E+02	BASIN STORAGE= .1462E-02	PERCENT ERROR= -.1					
FOR PLAN = 1 RC13B-1 MANE										RATIO= .00							
										5.00	310.89	230.00	1.99	5.00	310.89	230.00	1.99
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2641E+02 EXCESS= .0000E+00										OUTFLOW= .2643E+02	BASIN STORAGE= .1452E-02	PERCENT ERROR= -.1					
FOR PLAN = 1 RC13B-1 MANE										RATIO= .00							
										5.00	171.06	230.00	1.05	5.00	171.06	230.00	1.05
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1391E+02 EXCESS= .0000E+00										OUTFLOW= .1392E+02	BASIN STORAGE= .1716E-02	PERCENT ERROR= -.1					
FOR PLAN = 1 RC13B-2 MANE										RATIO= .00							
										5.00	640.80	230.00	2.18	5.00	640.80	230.00	2.18
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5392E+02 EXCESS= .0000E+00										OUTFLOW= .5398E+02	BASIN STORAGE= .5817E-02	PERCENT ERROR= -.1					
FOR PLAN = 1 RC13B-2 MANE										RATIO= .00							
										5.00	628.20	230.00	2.13	5.00	628.20	230.00	2.13

					EXISTING	OUT				
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.5282E+02	EXCESS=	.0000E+00	OUTFLOW=	.5288E+02	BASIN STORAGE=	.5767E-02	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
RC13B-2	MANE	5.00	607.17	230.00	2.06	5.00	607.17	230.00	2.06	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.5100E+02	EXCESS=	.0000E+00	OUTFLOW=	.5105E+02	BASIN STORAGE=	.5683E-02	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
RC13B-2	MANE	5.00	586.10	230.00	1.99	5.00	586.10	230.00	1.99	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.4918E+02	EXCESS=	.0000E+00	OUTFLOW=	.4923E+02	BASIN STORAGE=	.5597E-02	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
RC13B-2	MANE	5.00	578.31	230.00	1.96	5.00	578.31	230.00	1.96	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.4845E+02	EXCESS=	.0000E+00	OUTFLOW=	.4850E+02	BASIN STORAGE=	.7165E-02	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
RC13B-2	MANE	5.00	572.39	230.00	1.94	5.00	572.39	230.00	1.94	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.4794E+02	EXCESS=	.0000E+00	OUTFLOW=	.4799E+02	BASIN STORAGE=	.7136E-02	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
RC13B-2	MANE	5.00	568.15	230.00	1.92	5.00	568.15	230.00	1.92	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.4758E+02	EXCESS=	.0000E+00	OUTFLOW=	.4763E+02	BASIN STORAGE=	.7115E-02	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
RC13B-2	MANE	5.00	561.38	230.00	1.90	5.00	561.38	230.00	1.90	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.4700E+02	EXCESS=	.0000E+00	OUTFLOW=	.4705E+02	BASIN STORAGE=	.6748E-02	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
RC13B-2	MANE	5.00	295.27	235.00	.98	5.00	295.27	235.00	.98	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2427E+02	EXCESS=	.0000E+00	OUTFLOW=	.2430E+02	BASIN STORAGE=	.7210E-02	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
R19A	MANE	5.00	318.89	235.00	2.18	5.00	318.89	235.00	2.18	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2936E+02	EXCESS=	.0000E+00	OUTFLOW=	.2938E+02	BASIN STORAGE=	.2006E-02	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
R19A	MANE	5.00	312.72	235.00	2.13	5.00	312.72	235.00	2.13	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2875E+02	EXCESS=	.0000E+00	OUTFLOW=	.2877E+02	BASIN STORAGE=	.1983E-02	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
R19A	MANE	5.00	302.45	235.00	2.06	5.00	302.45	235.00	2.06	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2774E+02	EXCESS=	.0000E+00	OUTFLOW=	.2776E+02	BASIN STORAGE=	.1945E-02	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
R19A	MANE	5.00	292.17	235.00	1.98	5.00	292.17	235.00	1.98	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2673E+02	EXCESS=	.0000E+00	OUTFLOW=	.2675E+02	BASIN STORAGE=	.1906E-02	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
R19A	MANE	5.00	288.05	235.00	1.95	5.00	288.05	235.00	1.95	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2633E+02	EXCESS=	.0000E+00	OUTFLOW=	.2635E+02	BASIN STORAGE=	.1891E-02	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
R19A	MANE	5.00	285.17	235.00	1.93	5.00	285.17	235.00	1.93	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2605E+02	EXCESS=	.0000E+00	OUTFLOW=	.2606E+02	BASIN STORAGE=	.1880E-02	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
R19A	MANE	5.00	283.11	235.00	1.92	5.00	283.11	235.00	1.92	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2585E+02	EXCESS=	.0000E+00	OUTFLOW=	.2586E+02	BASIN STORAGE=	.1872E-02	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
R19A	MANE	5.00	279.82	235.00	1.89	5.00	279.82	235.00	1.89	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2553E+02	EXCESS=	.0000E+00	OUTFLOW=	.2554E+02	BASIN STORAGE=	.1860E-02	PERCENT ERROR=	-.1
FOR PLAN = 1	RATIO=	.00								
R19A	MANE	5.00	146.43	235.00	.96	5.00	146.43	235.00	.96	

										EXISTING.OUT		
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1300E+02 EXCESS= .0000E+00										OUTFLOW= .1300E+02	BASIN STORAGE= .2023E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RC13A-2	MANE	5.00	780.51	235.00	2.18	5.00	780.51	235.00	2.18			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7731E+02 EXCESS= .0000E+00										OUTFLOW= .7736E+02	BASIN STORAGE= .8795E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RC13A-2	MANE	5.00	764.75	235.00	2.14	5.00	764.75	235.00	2.14			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7572E+02 EXCESS= .0000E+00										OUTFLOW= .7577E+02	BASIN STORAGE= .8721E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RC13A-2	MANE	5.00	738.48	235.00	2.06	5.00	738.48	235.00	2.06			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7309E+02 EXCESS= .0000E+00										OUTFLOW= .7314E+02	BASIN STORAGE= .8303E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RC13A-2	MANE	5.00	712.20	235.00	1.99	5.00	712.20	235.00	1.99			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7047E+02 EXCESS= .0000E+00										OUTFLOW= .7051E+02	BASIN STORAGE= .8180E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RC13A-2	MANE	5.00	701.68	235.00	1.96	5.00	701.68	235.00	1.96			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6942E+02 EXCESS= .0000E+00										OUTFLOW= .6947E+02	BASIN STORAGE= .8130E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RC13A-2	MANE	5.00	694.32	235.00	1.94	5.00	694.32	235.00	1.94			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6869E+02 EXCESS= .0000E+00										OUTFLOW= .6873E+02	BASIN STORAGE= .8095E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RC13A-2	MANE	5.00	689.06	235.00	1.92	5.00	689.06	235.00	1.92			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6817E+02 EXCESS= .0000E+00										OUTFLOW= .6821E+02	BASIN STORAGE= .7878E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RC13A-2	MANE	5.00	680.64	235.00	1.90	5.00	680.64	235.00	1.90			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .6733E+02 EXCESS= .0000E+00										OUTFLOW= .6738E+02	BASIN STORAGE= .7838E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RC13A-2	MANE	5.00	353.55	240.00	.98	5.00	353.55	240.00	.98			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3459E+02 EXCESS= .0000E+00										OUTFLOW= .3462E+02	BASIN STORAGE= .6811E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RCPIC-C	MANE	2.90	1036.21	237.50	2.15	5.00	1029.58	235.00	2.15			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1041E+03 EXCESS= .0000E+00										OUTFLOW= .1041E+03	BASIN STORAGE= .2599E-02	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCPIC-C	MANE	2.92	1018.48	236.21	2.11	5.00	1009.34	235.00	2.11			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1020E+03 EXCESS= .0000E+00										OUTFLOW= .1020E+03	BASIN STORAGE= .2441E-02	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCPIC-C	MANE	2.95	983.10	236.05	2.03	5.00	975.10	235.00	2.03			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9842E+02 EXCESS= .0000E+00										OUTFLOW= .9843E+02	BASIN STORAGE= .3029E-02	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCPIC-C	MANE	2.99	947.55	235.94	1.96	5.00	940.20	235.00	1.96			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9487E+02 EXCESS= .0000E+00										OUTFLOW= .9488E+02	BASIN STORAGE= .2774E-02	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCPIC-C	MANE	3.00	935.30	237.12	1.93	5.00	921.65	235.00	1.93			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9346E+02 EXCESS= .0000E+00										OUTFLOW= .9347E+02	BASIN STORAGE= .2840E-02	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCPIC-C	MANE	3.01	923.69	237.96	1.91	5.00	914.93	235.00	1.91			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9247E+02 EXCESS= .0000E+00										OUTFLOW= .9248E+02	BASIN STORAGE= .2450E-02	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCPIC-C	MANE	3.02	912.75	235.55	1.90	5.00	907.94	235.00	1.89			

					EXISTING	OUT						
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.9176E+02	EXCESS=	.0000E+00	OUTFLOW=	.9177E+02	BASIN STORAGE=	.2737E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00										
RCPIC-C	MANE	3.03	906.65	236.52	1.87	5.00	895.54	235.00	1.87			
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.9064E+02	EXCESS=	.0000E+00	OUTFLOW=	.9064E+02	BASIN STORAGE=	.3045E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00										
RCPIC-C	MANE	3.82	462.80	240.43	.96	5.00	461.30	240.00	.96			
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.4647E+02	EXCESS=	.0000E+00	OUTFLOW=	.4648E+02	BASIN STORAGE=	.2735E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00										
RCON19	MANE	1.80	2048.82	237.17	2.11	5.00	2044.69	235.00	2.11			
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.2079E+03	EXCESS=	.0000E+00	OUTFLOW=	.2079E+03	BASIN STORAGE=	.3173E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00										
RCON19	MANE	1.81	2010.80	237.05	2.07	5.00	2005.77	235.00	2.07			
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.2036E+03	EXCESS=	.0000E+00	OUTFLOW=	.2036E+03	BASIN STORAGE=	.3176E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00										
RCON19	MANE	1.83	1943.99	236.30	1.99	5.00	1940.79	235.00	1.99			
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.1965E+03	EXCESS=	.0000E+00	OUTFLOW=	.1965E+03	BASIN STORAGE=	.3190E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00										
RCON19	MANE	1.86	1873.16	237.49	1.92	5.00	1871.11	235.00	1.92			
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.1894E+03	EXCESS=	.0000E+00	OUTFLOW=	.1894E+03	BASIN STORAGE=	.3294E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00										
RCON19	MANE	1.87	1848.15	237.07	1.89	5.00	1840.12	235.00	1.89			
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.1866E+03	EXCESS=	.0000E+00	OUTFLOW=	.1866E+03	BASIN STORAGE=	.2772E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00										
RCON19	MANE	1.87	1825.71	235.94	1.87	5.00	1823.96	235.00	1.87			
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.1846E+03	EXCESS=	.0000E+00	OUTFLOW=	.1846E+03	BASIN STORAGE=	.2965E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00										
RCON19	MANE	1.88	1818.28	236.57	1.86	5.00	1811.20	235.00	1.86			
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.1832E+03	EXCESS=	.0000E+00	OUTFLOW=	.1832E+03	BASIN STORAGE=	.2898E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00										
RCON19	MANE	1.89	1789.80	237.66	1.84	5.00	1787.73	235.00	1.84			
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.1809E+03	EXCESS=	.0000E+00	OUTFLOW=	.1809E+03	BASIN STORAGE=	.2791E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00										
RCON19	MANE	2.41	925.16	238.68	.94	5.00	921.96	240.00	.94			
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.9262E+02	EXCESS=	.0000E+00	OUTFLOW=	.9263E+02	BASIN STORAGE=	.3358E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00										
RCON20	MANE	.56	2044.29	235.85	2.10	5.00	2039.68	235.00	2.10			
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.2087E+03	EXCESS=	.0000E+00	OUTFLOW=	.2087E+03	BASIN STORAGE=	.7328E-03	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00										
RCON20	MANE	.56	2006.18	235.75	2.06	5.00	2000.73	235.00	2.06			
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.2044E+03	EXCESS=	.0000E+00	OUTFLOW=	.2044E+03	BASIN STORAGE=	.7376E-03	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00										
RCON20	MANE	.57	1942.31	235.64	1.99	5.00	1935.31	235.00	1.99			
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.1972E+03	EXCESS=	.0000E+00	OUTFLOW=	.1972E+03	BASIN STORAGE=	.6937E-03	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00										
RCON20	MANE	.58	1871.72	235.79	1.92	5.00	1864.98	235.00	1.92			
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.1901E+03	EXCESS=	.0000E+00	OUTFLOW=	.1901E+03	BASIN STORAGE=	.7025E-03	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00										
RCON20	MANE	.58	1840.42	235.43	1.89	5.00	1834.24	235.00	1.89			

										EXISTING.OUT							
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1873E+03 EXCESS= .0000E+00										OUTFLOW= .1873E+03	BASIN STORAGE= .6843E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RCON20 MANE										.58	1826.16	235.58	1.87	5.00	1817.88	235.00	1.87
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1853E+03 EXCESS= .0000E+00										OUTFLOW= .1853E+03	BASIN STORAGE= .7252E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RCON20 MANE										.58	1813.24	235.58	1.85	5.00	1805.07	235.00	1.85
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1839E+03 EXCESS= .0000E+00										OUTFLOW= .1839E+03	BASIN STORAGE= .6861E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RCON20 MANE										.59	1788.45	235.48	1.83	5.00	1781.38	235.00	1.83
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1816E+03 EXCESS= .0000E+00										OUTFLOW= .1816E+03	BASIN STORAGE= .7265E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RCON20 MANE										.74	922.05	240.78	.94	5.00	919.90	240.00	.94
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9284E+02 EXCESS= .0000E+00										OUTFLOW= .9284E+02	BASIN STORAGE= .7597E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RPIC-B MANE										1.74	439.87	237.27	2.03	5.00	439.01	235.00	2.03
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4783E+02 EXCESS= .0000E+00										OUTFLOW= .4783E+02	BASIN STORAGE= .2578E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RPIC-B MANE										1.75	432.13	236.45	1.99	5.00	430.53	235.00	1.99
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4685E+02 EXCESS= .0000E+00										OUTFLOW= .4685E+02	BASIN STORAGE= .2499E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RPIC-B MANE										1.76	417.58	236.27	1.92	5.00	416.38	235.00	1.92
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4522E+02 EXCESS= .0000E+00										OUTFLOW= .4522E+02	BASIN STORAGE= .2493E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RPIC-B MANE										1.78	403.10	236.14	1.85	5.00	402.16	235.00	1.85
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4360E+02 EXCESS= .0000E+00										OUTFLOW= .4360E+02	BASIN STORAGE= .2464E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RPIC-B MANE										1.78	398.34	236.81	1.83	5.00	396.16	235.00	1.83
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4296E+02 EXCESS= .0000E+00										OUTFLOW= .4296E+02	BASIN STORAGE= .2533E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RPIC-B MANE										1.78	393.51	237.29	1.81	5.00	392.22	235.00	1.81
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4251E+02 EXCESS= .0000E+00										OUTFLOW= .4250E+02	BASIN STORAGE= .2248E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RPIC-B MANE										1.79	390.10	235.85	1.79	5.00	389.58	235.00	1.79
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4218E+02 EXCESS= .0000E+00										OUTFLOW= .4218E+02	BASIN STORAGE= .2523E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RPIC-B MANE										1.79	386.39	236.40	1.77	5.00	385.05	235.00	1.77
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4167E+02 EXCESS= .0000E+00										OUTFLOW= .4167E+02	BASIN STORAGE= .2662E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RPIC-B MANE										2.03	203.87	238.08	.91	5.00	202.47	235.00	.91
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2143E+02 EXCESS= .0000E+00										OUTFLOW= .2143E+02	BASIN STORAGE= .2507E-03	PERCENT ERROR= .0					

*** NORMAL END OF HEC-1 ***

HYDROLOGIC CRITERIA AND DESIGN MANUAL

TIME OF CONCENTRATION



The Seventy
Proposed Conditions

Project No: 840-050
Date: 17-Feb-16
Calculated by: MMC

SUB-BASIN DATA					INITIAL / OVERLAND TIME (Ti)			TRAVEL TIME (Tt)					Tc CHECK URBANIZED BASINS			Tc	Tag	REMARKS
DESIG:	DEV./EX. (D or E)	CN	K	AREA Ac	AREA Sq Mli	INITIAL LENGTH Feet	SLOPE %	Ti Min	TRAVEL LENGTH Feet	SLOPE %	V1 VELOCITY fps	V2 VELOCITY fps	Tt Min	TOTAL LENGTH Feet	Tc = (L/180)*10 Min	Min		
(1)	(16)	(2)	(3)	(4)		(5)	(6)	(7)	(8)	(9a)	(9b)	(10)	(11)	(12)	(13)	(14)		
57B-1	D	93.7	0.8468	31.1	0.0485	250	2.80	5.1	3020	2.2	3.0	4.5	12.2	3270	28.2	17.3	0.173	2.89
57B-1A	D	85	0.7320	28.4	0.0443	370	2.40	9.5	2080	2.3	3.1	4.6	8.4	2450	23.6	17.9	0.179	2.96
57B-1B	D	93	0.8376	19.3	0.0301	100	1.00	4.7	1630	1.0	2.0	3.1	10.3	1730	19.6	15.0	0.150	2.91
57B-1C	D	96	0.8772	0.6	0.0009	50	1.00	2.8	490	1.2	2.2	3.4	3.7	540	13.0	6.5	0.065	2.89
57B-2A	D	87	0.7584	6.3	0.0098	186	13.40	3.5	2700	1.7	2.6	4.0	12.4	2886	26.0	15.9	0.159	3.05
57B-2B	D	87	0.7584	3.0	0.0047	50	2.00	3.5	1400	2.7	3.3	5.0	5.5	1450	18.1	8.9	0.089	2.99
57B-2C	D	87	0.7584	1.7	0.0027	100	1.00	6.1	222	6.8	5.3	8.0	0.7	322	11.8	6.9	0.069	2.96
57B-2D	D	91	0.8112	5.7	0.0088	110	1.00	5.5	1200	1.1	2.1	3.2	7.6	1310	17.3	13.0	0.130	3.09
57B-2E	D	91	0.8112	14.5	0.0227	110	1.00	5.5	1360	3.4	3.7	5.6	4.8	1470	18.2	10.2	0.102	3.08
57B-2F	D	91	0.8112	57.8	0.0902	110	1.00	5.5	3000	2.5	3.2	4.8	11.2	3110	27.3	16.7	0.167	3.03
57B-2G1	D	87	0.7584	1.6	0.0026	35	5.60	2.0	730	2.9	3.4	5.2	3.2	765	14.3	5.2	0.052	3.08
57B-2G2	D	87	0.7584	4.6	0.0073	40	2.50	2.9	1511	2.2	3.0	4.5	6.5	1551	18.6	9.4	0.094	3.03
57B-2H1	D	87	0.7584	18.6	0.0291	300	3.70	6.9	4120	1.1	2.1	3.2	22.7	4420	34.6	29.6	0.296	3.01
57B-2H2	D	87	0.7584	10.0	0.0156	300	2.30	8.1	2500	2.2	3.0	4.5	10.1	2800	25.6	18.2	0.182	3.04
57B-2I	D	87	0.7584	4.6	0.0072	80	7.50	2.8	1575	2.6	3.3	4.9	6.2	1655	19.2	9.0	0.090	2.99
57B-3	D	89.3	0.7888	30.8	0.0481	380	1.30	10.0	4170	2.4	3.1	4.7	15.6	4550	35.3	25.6	0.256	3.06
57B-3A	D	85	0.7320	16.6	0.0259	170	1.00	8.6	1360	2.0	2.9	4.3	6.2	1530	18.5	14.9	0.149	3.07
57B-3B	D	85	0.7320	32.8	0.0513	110	1.00	6.9	2500	2.4	3.1	4.7	9.7	2610	24.5	16.6	0.166	3.00
57B-3C	D	87	0.7584	4.4	0.0069	130	1.00	7.0	1140	2.5	3.2	4.8	4.8	1270	17.1	11.8	0.118	3.05
57B-3D	D	87	0.7584	11.8	0.0184	125	1.00	6.9	2500	2.7	3.3	5.0	9.1	2625	24.6	16.0	0.160	2.99
57B-3E	D	87	0.7584	16.0	0.0251	240	1.00	9.5	3200	2.5	3.2	4.8	11.9	3440	29.1	21.4	0.214	3.06
57B-3F	D	87	0.7584	7.4	0.0116	180	2.70	5.9	2170	2.5	3.2	4.9	8.3	2350	23.1	14.2	0.142	3.05
57B-3G	D	87	0.7584	1.5	0.0023	220	3.20	6.2	260	4.6	4.3	6.6	1.0	480	12.7	7.2	0.072	2.99
57B-4	D	93.8	0.8482	82.7	0.1293	35	2.00	2.1	4890	2.4	3.1	4.7	18.1	4925	37.4	20.2	0.202	2.91
57B-4B	D	96	0.8772	7.1	0.0110	150	2.70	3.5	860	2.9	3.4	5.2	3.6	1010	15.6	7.1	0.071	2.91
57B-4C	D	96	0.8772	7.8	0.0122	100	1.00	4.0	1560	1.6	2.6	3.9	7.8	1660	19.2	11.8	0.118	2.90
ON1	D	82	0.6924	25.4	0.0397	165	4.20	5.8	2040	3.0	3.5	5.3	7.2	2205	22.3	13.1	0.131	3.08
ON2	D	82	0.6924	17.5	0.0273	180	5.00	5.8	2700	2.5	3.2	4.8	10.2	2880	26.0	15.9	0.159	3.00
ON3R	D	82	0.6924	4.1	0.0065	135	12.00	3.7	500	1.7	2.6	4.0	3.2	635	13.5	6.9	0.069	2.96
ON5	D	82	0.6924	9.4	0.0147	125	4.00	5.2	1420	2.9	3.4	5.2	5.4	1545	18.6	10.5	0.105	3.05
ON6	D	93	0.8376	2.3	0.0035	20	4.00	1.3	785	1.7	2.6	4.0	4.4	805	14.5	5.7	0.057	3.04
ON8	D	82	0.6924	12.2	0.0190	65	6.20	3.2	1950	8.7	6.0	9.0	4.1	2015	21.2	7.3	0.073	2.99

ON9	D	82	0.6924	25.5	0.0399	290	15.50	5.0	3085	1.0	2.0	3.1	18.2	3375	28.8	23.2	0.232	3.06
ON10	D	82	0.6924	11.4	0.0177	100	29.00	2.4	1460	2.9	3.4	5.2	5.5	1560	18.7	7.9	0.079	2.98
ON11R	D	82	0.6924	5.1	0.0080	270	13.70	5.0	350	1.6	2.6	3.9	2.3	620	13.4	7.3	0.073	2.95
ON12	D	82	0.6924	11.6	0.0182	225	3.50	7.2	1300	3.1	3.6	5.4	4.8	1525	18.5	12.1	0.121	3.08
ON13	D	82	0.6924	12.0	0.0187	210	7.10	5.5	1540	3.6	3.8	5.8	5.2	1750	19.7	10.7	0.107	3.04
ON14	D	82	0.6924	3.5	0.0054	100	1.00	7.3	1575	0.5	1.4	2.2	14.1	1675	19.3	21.5	0.193	3.00
ON15R	D	82	0.6924	21.5	0.0335	120	7.50	4.1	2070	3.3	3.7	5.6	7.0	2190	22.2	11.1	0.111	2.98
ON16R	D	82	0.6924	10.9	0.0171	45	45.00	1.4	2050	3.3	3.7	5.6	6.9	2095	21.6	8.3	0.083	2.97
ON18R	D	82	0.6924	18.5	0.0289	175	0.60	11.5	2565	2.5	3.2	4.9	9.7	2740	25.2	21.2	0.212	2.95
DON1	D	95	0.8640	10.8	0.0169	138	15.50	2.0	1515	1.9	2.8	4.2	7.0	1653	19.2	9.0	0.090	2.93
DON2	D	95	0.8640	19.5	0.0304	100	21.00	1.5	1735	1.7	2.6	4.0	8.3	1835	20.2	9.9	0.099	2.93
DON3	D	95	0.8640	21.1	0.0330	240	5.00	3.8	1530	2.8	3.4	5.1	5.8	1770	19.8	9.7	0.097	2.91
DON4	D	95	0.8640	17.4	0.0272	109	2.80	3.1	1650	0.03	0.3	0.5	60.0	1759	19.8	63.1	0.198	2.88

$T_c = T_i + T_t$ For the travel time (T_t) calculations,
 $T_i = 1.8 (1.1 - K) L^{1/2} / S^{1/3}$ V1 applies to the first 500 feet of travel distance;
 $K = 0.0132 (CN) - 0.39$ V2 applies to the remaining travel distance.

Existing: $V1 = 14.8*(S/100)^{1/2}$ Developed: $V1 = 20.2*(S/100)^{1/2}$
 $V2 = 29.4*(S/100)^{1/2}$ $V2 = 30.6*(S/100)^{1/2}$

REFERENCE: CN values referenced from MPU

STANDARD FORM 4

PROPOSED.OUT

```

67      UD      .131
        *
68      KK      57B-3A
69      KM      ONSITE BASIN 57B-3A
70      PB      3.07
71      BA      0.0259      85
72      LS      0
73      UD      .149
        *
74      KK      CON1
75      KM      COMBINE 57B-3A AND ON1
76      HC      2
        *
77      KK      RCON1
78      KM      ROUTE CON1 TO CON2
79      KM      LENGTH SLOPE n-VALUE      0      SHAPE      WIDTH      S-SLOPE
80      RD      3020      .027      .040      TRAP      50      3
        *
81      KK      57B-3B
82      KM      OFFSITE BASIN 57B-3B
83      PB      3.00
84      BA      0.0513      85
85      LS      0
86      UD      .166
        *
87      KK      ON2
88      KM      OFFSITE BASIN ON2
89      PB      3.00
90      BA      0.0273      82
91      LS      0
92      UD      .159
        *

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HEC-1 INPUT

PAGE 3

1

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
93      KK      CON2
94      KM      COMBINE CON1, 57B-3B AND ON2
95      HC      3
        *
96      KK      57B-3D
97      KM      OFFSITE BASIN 57B-3D
98      PB      2.99
99      BA      0.0184      87
100     LS      0
101     UD      .160
        *
102     KK      ON3R
103     KM      ONSITE BASIN ON3R
104     PB      2.96
105     BA      0.0065      82
106     LS      0
107     UD      .069
        *
108     KK      CON3R
109     KM      COMBINE CON2, 57B-3D AND ON3R
110     HC      3
        *
111     KK      ON5
112     KM      OFFSITE BASIN ON5
113     PB      3.05
114     BA      0.0147      82
115     LS      0
116     UD      .105
        *
117     KK      57B-3C
118     KM      OFFSITE BASIN 57B-3C
119     PB      3.05
120     BA      0.0069      87
121     LS      0
122     UD      .118
        *
123     KK      ON6
124     KM      OFFSITE BASIN ON6
125     PB      3.04
126     BA      0.0035      93
127     LS      0
128     UD      .057
        *

```

HEC-1 INPUT

PAGE 4

1

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
129     KK      CON6
130     KM      COMBINE 57B-3C AND ON6
131     HC      2
        *
132     KK      CCON6
133     KM      COMBINE ON5 AND CON6
134     HC      2
        *
135     KK      RCON6
136     KM      ROUTE CCON6 TO CON8
137     KM      LENGTH SLOPE n-VALUE      0      SHAPE      WIDTH      S-SLOPE
138     RD      2015      .037      .040      TRAP      20      2
        *

```

PROPOSED.OUT

139 KK ON8
140 KM ONSITE BASIN ON8
141 PB 2.99
142 BA 0.0190 82
143 LS 0
144 UD .073
*

145 KK CON8
146 KM COMBINE CCON6 AND ON8
147 HC 2
*

148 KK SW11
149 KM REFERENCED FROM 2013 MPU
150 BA 0.589
151 PB 3.34
152 LS 0 87.8
153 UD 0.311
*

154 KK RSW11
155 KM REFERENCED FROM 2013 MPU
156 KM ROUTE SW11 TO CSW17
157 KM FACILITY = ANGEL PARK - CHARLESTON BOULEVARD
158 KM FACILITY # = APCB 0064, 0080
159 KM LINING = RCB
160 RD 2338 0.0167 0.015 0 TRAP 7 0
*

161 KK SW17
162 KM REFERENCED FROM 2013 MPU
163 BA 0.356
164 PB 3.30
165 LS 0 87.8
166 UD 0.271
*

HEC-1 INPUT

PAGE 5

1
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

167 KK CSW17
168 KM REFERENCED FROM 2013 MPU
169 KM COMBINE RSW11 AND SW17
170 HC 2
*

171 KK RCSW17
172 KM REFERENCED FROM 2013 MPU
173 KM ROUTE CSW17 TO CSW18
174 KM FACILITY = ANGEL PARK - CHARLESTON BOULEVARD
175 KM FACILITY # = APCB 0000,0001,0019,0050
176 KM LINING = RCB
177 RD 3600 0.014 0.015 0 TRAP 11 0
*

178 KK SW18
179 KM REFERENCED FROM 2013 MPU
180 BA 0.405
181 PB 3.27
182 LS 0 86.8
183 UD 0.271
*

184 KK CSW18
185 KM REFERENCED FROM 2013 MPU
186 KM COMBINE RCSW17 AND SW18
187 HC 2
*

188 KK RCSW18
189 KM REFERENCED FROM 2013 MPU
190 KM ROUTE CSW18 TO C12A
191 KM FACILITY = ANGEL PARK SOUTH
192 KM FACILITY # = APSO 0254,0255,0258,0345,0346; APCB 0000
193 KM NATURAL WASH
194 KM LENGTH = 5,200
195 KM SLOPE = 1.4%
196 KM N = 0.040
197 KM HYDRAULIC RADIUS = 1.5
198 KM VELOCITY = 9.2
199 RM 2 0.157 0.15
*

200 KK 12A
201 KM REFERENCED FROM 2013 MPU
202 BA 0.392
203 PB 3.20
204 LS 0 91.2
205 UD 0.264
*

HEC-1 INPUT

PAGE 6

1
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

206 KK C12A
207 KM REFERENCED FROM 2013 MPU
208 KM COMBINE 12A AND RCSW18
209 HC 2
*

210 KK RC12A
211 KM REFERENCED FROM 2013 MPU
212 KM ROUTE THRU 12B
213 KM FACILITY = ANGEL PARK SOUTH
214 KM FACILITY # = APSO 0204, 0205
215 KM NATURAL WASH
216 KM LENGTH = 2,600
217 KM SLOPE = 3.5%
218 KM N = 0.040

PROPOSED.OUT

219 KM HYDRAULIC RADIUS = 1.5
220 KM VELOCITY = 14.5
221 RM 1 0.05 0.15
*

222 KK 12B
223 KM REFERENCED FROM 2013 MPU
224 BA 0.260
225 PB 3.13
226 LS 0 91.0
227 UD 0.233
*

228 KK C12B
229 KM REFERENCED FROM 2013 MPU
230 KM COMBINE 12B AND RC12A
231 HC 2
*

232 KK 57B-2A
233 KM OFFSITE BASIN 57B-2A
234 PB 3.05
235 BA 0.0098
236 LS 0 87
237 UD .159
*

238 KK 57B-3F
239 KM OFFSITE BASIN 57B-3F
240 PB 3.05
241 BA 0.0116
242 LS 0 87
243 UD .142
*

HEC-1 INPUT

PAGE 7

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

244 KK 57B-3E
245 KM OFFSITE BASIN 57B-3E
246 PB 3.06
247 BA 0.0251
248 LS 0 87
249 UD .214
*

250 KK ON9
251 KM ONSITE BASIN ON9
252 PB 3.06
253 BA 0.0399
254 LS 0 82
255 UD .232
*

256 KK CON9
257 KM COMBINE C12B, 57B-2A, 57B-3F, 57B-3E AND ON9
258 HC 5
*

259 KK RCON9
260 KM ROUTE CON9 TO CON10
261 KM LENGTH SLOPE n-VALUE 0 SHAPE WIDTH S-SLOPE
262 RD 1540 .030 .040 0 TRAP 50 2
*

263 KK 57B-3G
264 KM OFFSITE BASIN 57B-3G
265 PB 2.99
266 BA 0.0023
267 LS 0 87
268 UD .072
*

269 KK 57B-2B
270 KM OFFSITE BASIN 57B-2B
271 PB 2.99
272 BA 0.0047
273 LS 0 87
274 UD .089
*

275 KK 57B-2C
276 KM OFFSITE BASIN 57B-2C
277 PB 2.96
278 BA 0.0027
279 LS 0 87
280 UD .069
*

HEC-1 INPUT

PAGE 8

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

281 KK ON10
282 KM ONSITE BASIN ON10
283 PB 2.98
284 BA 0.0177
285 LS 0 82
286 UD .079
*

287 KK CON10
288 KM COMBINE CON9, 57B-3G, 57B-2B, 57B-2C AND ON10
289 HC 5
*

290 KK CCON10
291 KM COMBINE CON8 AND CON10
292 HC 2
*

PROPOSED.OUT

293 KK ON11R
294 KM ONSITE BASIN ON11R
295 PB 2.95
296 BA 0.0080
297 LS 0 82
298 UD .073
*

299 KK CON11R
300 KM COMBINE CCON10 AND ON11R
301 HC 2
*

302 KK 57B-2D
303 KM OFFSITE BASIN 57B-2D
304 PB 3.09
305 BA 0.0088
306 LS 0 91
307 UD .130
*

308 KK 57B-2E
309 KM OFFSITE BASIN 57B-2E
310 PB 3.08
311 BA 0.0227
312 LS 0 91
313 UD .102
*

314 KK C57B-2E
315 KM COMBINE 57B-2D AND 57B-2E
316 HC 2
*

HEC-1 INPUT

PAGE 9

1 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

317 KK 57B-2G1
318 KM OFFSITE BASIN 57B-2G1
319 PB 3.08
320 BA 0.0026
321 LS 0 87
322 UD .052
*

323 KK ON12
324 KM ONSITE BASIN ON12
325 PB 3.08
326 BA 0.0182
327 LS 0 82
328 UD .121
*

329 KK CON12
330 KM COMBINE C57B-2E, 57B-2G1 AND ON12
331 HC 3
*

332 KK 57B-2G2
333 KM OFFSITE BASIN 57B-2G2
334 PB 3.03
335 BA 0.0073
336 LS 0 87
337 UD .094
*

338 KK ON13
339 KM ONSITE BASIN ON13
340 PB 3.04
341 BA 0.0187
342 LS 0 82
343 UD .107
*

344 KK CON13
345 KM COMBINE CON12, 57B-2G2 AND ON13
346 HC 3
*

347 KK 57B-2F
348 KM OFFSITE BASIN 57B-2F
349 PB 3.03
350 BA 0.0902
351 LS 0 91
352 UD .167
*

HEC-1 INPUT

PAGE 10

1 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

353 KK 57B-2H2
354 KM OFFSITE BASIN 57B-2H2
355 PB 3.04
356 BA 0.0156
357 LS 0 87
358 UD .182
*

359 KK ON14
360 KM ONSITE BASIN ON14
361 PB 3.00
362 BA 0.0054
363 LS 0 82
364 UD .193
*

365 KK CON14
366 KM COMBINE C57B-2F, 57B-2H2 AND ON14
367 HC 3
*

PROPOSED.OUT

```

368 KK RCON14
369 KM ROUTE CON14 TO CON15R
370 KM LENGTH 2160 SLOPE .032 n-VALUE .040 0 SHAPE WIDTH S-SLOPE
371 RD TRAP 20 2
    *

372 KK 57B-2I
373 KM OFFSITE BASIN 57B-2I
374 PB 2.99
375 BA 0.0072
376 LS 0 87
377 UD .090
    *

378 KK 57B-2H1
379 KM OFFSITE BASIN 57B-2H1
380 PB 3.01
381 BA 0.0291
382 LS 0 87
383 UD .296
    *

384 KK ON15R
385 KM ONSITE BASIN ON15R
386 PB 2.98
387 BA 0.0335
388 LS 0 82
389 UD .111
    *

```

HEC-1 INPUT

PAGE 11

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

390 KK CON15R
391 KM COMBINE CON13, CON14, 57B-2I, 57B-2H1 AND ON15R
392 HC 5
    *

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393 KK ON16R
394 KM ONSITE BASIN ON16R
395 PB 2.97
396 BA 0.0171
397 LS 0 82
398 UD .083
    *

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```

399 KK CON16R
400 KM COMBINE CON15R AND ON16R
401 HC 2
    *

```

```

402 KK CPPH1
403 KM COMBINE CON3R, CON11R AND CON16R
404 HC 3
    *

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```

405 KK DON1
406 KM ONSITE BASIN DON1
407 PB 2.93
408 BA 0.0169
409 LS 0 95
410 UD .090
    *

```

```

411 KK DON2
412 KM ONSITE BASIN DON2
413 PB 2.93
414 BA 0.0304
415 LS 0 95
416 UD .099
    *

```

```

417 KK CDON2
418 KM COMBINE CCON16R, CDON1 AND DON2
419 HC 3
    *

```

```

420 KK RCDON2
421 KM ROUTE CDON2 TO CDON3
422 KM LENGTH 1000 SLOPE .048 n-VALUE .016 0 SHAPE WIDTH S-SLOPE
423 RD TRAP 10 50
    *

```

HEC-1 INPUT

PAGE 12

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

424 KK 13B-1
425 KM REFERENCED FROM 2013 MPU
426 BA 0.249
427 PB 3.19
428 LS 0 91.6
429 UD 0.284
    *

```

```

430 KK RCL3B-1
431 KM REFERENCED FROM 2013 MPU
432 KM ROUTE 13B-1 TO C13B-2
433 KM GRIFFITH PARK DRIVE AND HUALAPAI WAY
434 RD 3000 0.018 0.016 0 TRAP 0 50
    *

```

```

435 KK 13B-2
436 KM REFERENCED FROM 2013 MPU
437 BA 0.216
438 PB 3.14
439 LS 0 89.7
440 UD 0.231
    *

```

PROPOSED.OUT

441 KK C13B-2
442 KM REFERENCED FROM 2013 MPU
443 KM COMBINE 13B-2 AND RC13B-1
444 KM HUALAPAI WAY AND LOCAL FACILITY
445 HC 2
*

446 KK RC13B-2
447 KM REFERENCED FROM 2013 MPU
448 KM ROUTE C13B-2 TO CCPIC-A
449 KM LINING = GRASS
450 RD 4900 0.021 0.03 0 TRAP 40 6
*

451 KK 19A
452 KM REFERENCED FROM 2013 MPU
453 BA 0.253
454 PB 3.25
455 LS 0 89.9
456 UD 0.351
*

457 KK R19A
458 KM REFERENCED FROM 2013 MPU
459 KM ROUTE 19A TO C13A-1
460 KM UNNAMED ROAD
461 RD 4300 0.021 0.016 0 TRAP 0 50
*

HEC-1 INPUT

PAGE 13

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

462 KK 13A-1
463 KM REFERENCED FROM 2013 MPU
464 BA 0.224
465 PB 3.19
466 LS 0 91.4
467 UD 0.302
*

468 KK C13A-1
469 KM REFERENCED FROM 2013 MPU
470 KM COMBINE 13A-1 AND R19A
471 KM TOWN CENTER DRIVE AND SWALE
472 HC 2
*

473 KK RC13A-1
474 KM REFERENCED FROM 2013 MPU
475 KM ROUTE C13A-1 TO C13A-2
476 KM NATURAL WASH
477 KM TRAVEL LENGTH = 2,800
478 KM SLOPE = 2.1%
479 KM N = 0.040
480 KM HYDRAULIC RADIUS = 1.5
481 KM VELOCITY = 11.4
482 RM 1 0.068 0.15
*

483 KK 13A-2
484 KM REFERENCED FROM 2013 MPU
485 BA 0.188
486 PB 3.15
487 LS 0 90.0
488 UD 0.236
*

489 KK C13A-2
490 KM REFERENCED FROM 2013 MPU
491 KM COMBINE 13A-2 AND RC13A-1
492 HC 2
*

493 KK RC13A-2
494 KM REFERENCED FROM 2013 MPU
495 KM ROUTE C13A-2 TO CPIC-C
496 KM LINING = GRASS
497 RD 5200 0.015 0.03 0 TRAP 40 4
*

498 KK PIC-C
499 KM REFERENCED FROM 2013 MPU
500 BA 0.243
501 PB 3.08
502 LS 0 90.4
503 UD 0.373
*

HEC-1 INPUT

PAGE 14

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

504 KK CPIC-C
505 KM REFERENCED FROM 2013 MPU
506 KM COMBINE PIC-C AND RC13A-2
507 HC 2
*

508 KK RCPIC-C
509 KM REFERENCED FROM 2013 MPU
510 KM ROUTE CPIC-C TO CPIC-A
511 KM LINING = GRASS
512 RD 2200 0.025 0.03 0 TRAP 40 4
*

513 KK PIC-A
514 KM REFERENCED FROM 2013 MPU
515 BA 0.359
516 PB 3.03
517 LS 0 91.1
518 UD 0.499

PROPOSED.OUT

519 KK CPIC-A
520 KM REFERENCED FROM 2013 MPU
521 KM COMBINE CPIC-C AND PIC-A
522 HC 2
*

523 KK CCPIC-A
524 KM REFERENCED FROM 2013 MPU
525 KM COMBINE CPIC-A AND RC13B-2
526 HC 2
*

527 KK ON18R
528 KM ONSITE BASIN ON18R
529 PB 2.95
530 BA 0.0289
531 LS 0 82
532 UD .212
*

533 KK CON18R
534 KM COMBINE CCPIC-A AND ON18R
535 HC 2
*

536 KK 57B-1A
537 KM OFFSITE BASIN 57B-1A
538 PB 2.96
539 BA 0.0443
540 LS 0 85
541 UD .179
*

1

HEC-1 INPUT

PAGE 15

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

542 KK CCON18R
543 KM COMBINE 57B-1A AND CON18R
544 HC 2
*

545 KKRCCON18R
546 KM ROUTE CCON18R TO CDON3
547 KM LENGTH SLOPE n-VALUE
548 RD 1520 .014 .016 0 SHAPE TRAP WIDTH 10 S-SLOPE 50
*

549 KK 57B-1B
550 KM OFFSITE BASIN 57B-1B
551 PB 2.91
552 BA 0.0301
553 LS 0 93
554 UD .150
*

555 KK CP19
556 KM COMBINE CCON18R AND 57B-1B
557 HC 2
*

558 KK 57B-1C
559 KM OFFSITE BASIN 57B-1C
560 PB 2.89
561 BA 0.0009
562 LS 0 96
563 UD .065
*

564 KK CP20
565 KM COMBINE CP19 AND 57B-1C
566 HC 2
*

567 KK DON3
568 KM ONSITE BASIN DON3
569 PB 2.91
570 BA 0.0330
571 LS 0 95
572 UD .097
*

573 KK CDON3
574 KM COMBINE DON3, CP20 AND CDON2
575 HC 3
*

1

HEC-1 INPUT

PAGE 16

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

576 KK RCDON3
577 KM ROUTE CDON3 TO CDON4
578 KM LENGTH SLOPE n-VALUE
579 RD 1500 .003 .016 0 SHAPE TRAP WIDTH 15 S-SLOPE 50
*

580 KK DON4
581 KM ONSITE BASIN DON4
582 PB 2.88
583 BA 0.0272
584 LS 0 95
585 UD .198
*

586 KK 57B-4B
587 KM OFFSITE BASIN 57B-4B
588 PB 2.91
589 BA 0.0110
590 LS 0 96

PROPOSED.OUT

591 UD .071
 *
 592 KK 57B-4C
 593 KM OFFSITE BASIN 57B-4C
 594 PB 2.90
 595 BA 0.0122
 596 LS 0 96
 597 UD .118
 *
 598 KK C57B-4C
 599 KM COMBINE 57B-4B AND 57B-4C
 600 HC 2
 *
 601 KK CDON4
 602 KM COMBINE DON4, CDON3 AND C57B-4C
 603 HC 3
 *
 604 KK 57B-1
 605 KM OFFSITE BASIN 57B-1
 606 BA 0.0485
 607 PB 2.89
 608 LS 0 93.7
 609 UD 0.173
 *
 610 KK PIC-B
 611 KM REFERENCED FROM 2013 MPU
 612 BA 0.441
 613 PB 2.98
 614 LS 0 91.1
 615 UD 0.471
 *

HEC-1 INPUT

PAGE 17

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

616 KK RPIC-B
 617 KM REFERENCED FROM 2013 MPU
 618 KM ROUTE PIC-B TO CC57B-4
 619 KM FACILITY = ANGEL PARK - PECCOLE 1
 620 KM FACILITY # = APP1 0000
 621 KM LINING = RCP
 622 RD 2982 0.024 0.013 0 CIRC 6
 *
 623 KK 57B-3
 624 KM OFFSITE BASIN 57B-3
 625 BA 0.0481
 626 PB 3.06
 627 LS 0 89.3
 628 UD 0.256
 *
 629 KK 57B-4
 630 KM OFFSITE BASIN 57B-4
 631 BA 0.1293
 632 PB 2.91
 633 LS 0 93.8
 634 UD 0.202
 *
 635 KK C57B-4
 636 KM COMBINE 57B-3 AND 57B-4
 637 HC 2
 *
 638 KK CC57B-4
 639 KM COMBINE RPIC-B, 57B-1, C57B-4, AND CDON4
 640 HC 4
 *
 641 ZZ

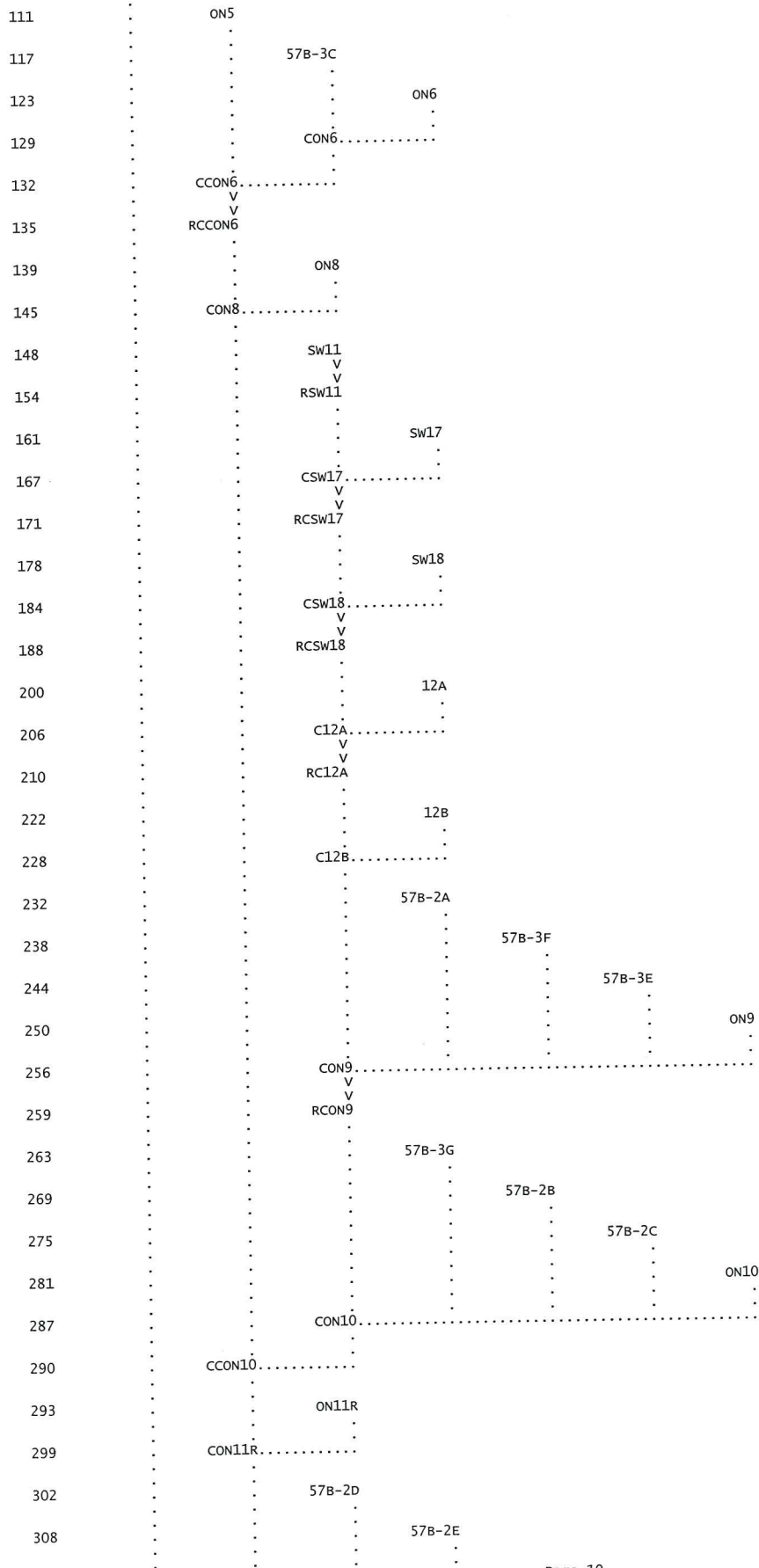
1

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

54 ON1
 .
 68 . 57B-3A
 .
 74 CON1.....
 V
 77 RCON1
 .
 81 . 57B-3B
 .
 87 . ON2
 .
 93 CON2.....
 .
 96 . 57B-3D
 .
 102 . ON3R
 .
 108 CON3R.....

PROPOSED.OUT



314	.	.	C57B-2E.....	PROPOSED.OUT
317	.	.	57B-2G1	
323	.	.		ON12
329	.	.	CON12.....	
332	.	.	57B-2G2	
338	.	.		ON13
344	.	.	CON13.....	
347	.	.	57B-2F	
353	.	.		57B-2H2
359	.	.		ON14
365	.	.	CON14.....	
368	.	.	V	
	.	.	RCON14	
372	.	.		57B-2I
378	.	.		57B-2H1
384	.	.		ON15R
390	.	.	CON15R.....	
393	.	.		ON16R
399	.	.	CON16R.....	
402	CPPH1.....	.		
405	.	.	DON1	
411	.	.		DON2
417	CDON2.....	.		
420	V	.		
	RCDON2	.		
424	.	.	13B-1	
430	.	.	V	
	RC13B-1	.		
435	.	.		13B-2
441	.	.	C13B-2.....	
446	.	.	V	
	RC13B-2	.		
451	.	.	19A	
457	.	.	V	
	R19A	.		
462	.	.		13A-1
468	.	.	C13A-1.....	
473	.	.	V	
	RC13A-1	.		
483	.	.		13A-2
489	.	.	C13A-2.....	
493	.	.	V	
	RC13A-2	.		
498	.	.		PIC-C
504	.	.	CPIC-C.....	

508	V V RCPIC-C
513	PIC-A
519	CPIC-A.....
523	CCPIC-A.....
527	ON18R
533	CON18R.....
536	57B-1A
542	CCON18R.....
545	V V RCCON18R
549	57B-1B
555	CP19.....
558	57B-1C
564	CP20.....
567	DON3
573	CDON3.....
576	V V RCDON3
580	DON4
586	57B-4B
592	57B-4C
598	C57B-4C.....
601	CDON4.....
604	57B-1
610	PIC-B V V
616	RPIC-B
623	57B-3
629	57B-4
635	C57B-4.....
638	CC57B-4.....

```

*****
*
*   FLOOD HYDROGRAPH PACKAGE   (HEC-1)
*       JUN      1988
*       VERSION  4.1
*
*   RUN DATE    24FEB16   TIME  10:49:22
*
*****

```

*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*

```

*****
*
* .....
*
* THE SEVENTY
* EHB COMPANIES
* PROPOSED CONDITIONS
*
* .....
*
* RETURN PERIOD_ _ _ _100 & 10 -YEAR
* DISTRIBUTION_ _ _ _6-HOUR SDN3
* PROJECT NO_ _ _ _840.050
* FILENAME_ _ _ _PROPOSED.H1
* DATE MODELED_ _ _ _2/22/16
*
*
* Page 12

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      PROPOSED.OUT
      MODELED BY _ _ _ _ JAM, MMC, RRD, SHT
      *
      *
      *
      *
      *****

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REFERENCED HYDROLOGIC MODELS:
 2013 LAS VEGAS VALLEY FLOOD CONTROL MASTER PLAN UPDATE
 CITY OF LAS VEGAS CITY WIDE HYDROLOGY ANALYSIS (PBS&J 1997)
 CLARK COUNTY REGIONAL FLOOD CONTROL DISTRICT 2008 MASTER PLAN UPDATE
 GOWAN WATERSHED (ALL)
 RECOMMENDED DRAINAGE SYSTEM WITH ULTIMATE DEVELOPMENT
 INPUT FILE = ALLGOW3.DAT
 INPUT FILE DATE = MAY 5, 2008
 DESIGN STORM = 100-YEAR 6-HR STORM
 STORM DISTRIBUTION = SDN #3
 MODELED BY PBS&J (MICHELE L. D'ALESSANDRO, E.I., CFM)
 CHECKED BY PBS&J (HARSHAL B. DESAI, P.E., CFM)
 STORM CENTERING = FULL WATERSHED
 JR CARDS CONTAIN DARFS BASED ON THE FOLLOWING VALUES:

AREA SQ. MI.	DARF
0-0.5	0.99
0.5-1	0.975
1-2	0.95
2-3	0.925
3-4	0.915
4-5	0.908
5-6	0.903
6-7	0.895
10YR	0.570

JR CARD RATIOS REPRESENT DEPTH-AREA REDUCTION FACTORS (DARF'S)

100-YEAR, 6-HOUR STORM, SDN3

51 IO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 5 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 700 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 3 0 ENDING DATE
 NDTIME 1015 ENDING TIME
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS
 TOTAL TIME BASE 58.25 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-Feet
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
 NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
 RATIOS OF PRECIPITATION
 .99 .98 .95 .93 .92 .91 .90 .89 .57

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
 TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN		RATIOS APPLIED TO PRECIPITATION								
					RATIO 1 .99	RATIO 2 .98	RATIO 3 .95	RATIO 4 .93	RATIO 5 .92	RATIO 6 .91	RATIO 7 .90	RATIO 8 .89	RATIO 9 .57
HYDROGRAPH AT	ON1	.04	1	FLOW	50.	49.	47.	45.	44.	43.	43.	42.	18.
+				TIME	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58
HYDROGRAPH AT	57B-3A	.03	1	FLOW	36.	35.	34.	32.	32.	31.	31.	31.	14.
+				TIME	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58
2 COMBINED AT	CON1	.07	1	FLOW	86.	84.	80.	77.	76.	75.	74.	73.	32.
+				TIME	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58
ROUTED TO	RCON1	.07	1	FLOW	86.	84.	80.	77.	76.	75.	74.	73.	30.
+				TIME	3.75	3.75	3.75	3.75	3.75	3.75	3.75	3.75	3.83
HYDROGRAPH AT	57B-3B	.05	1	FLOW	66.	65.	62.	59.	58.	58.	57.	56.	25.
+				TIME	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58
HYDROGRAPH AT	ON2	.03	1	FLOW	31.	30.	29.	28.	27.	27.	27.	26.	11.
+				TIME	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58
3 COMBINED AT	CON2	.14	1	FLOW	164.	160.	153.	145.	143.	141.	139.	137.	55.
+				TIME	3.67	3.67	3.67	3.67	3.67	3.67	3.67	3.67	3.75
HYDROGRAPH AT	57B-3D	.02	1	FLOW	26.	25.	24.	23.	23.	23.	23.	22.	11.
+				TIME	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58	3.58

PROPOSED.OUT

HYDROGRAPH AT	ON3R	.01	1	FLOW	9. 3.50	9. 3.50	9. 3.50	8. 3.50	8. 3.50	8. 3.50	8. 3.50	8. 3.50	3. 3.50
+ 3 COMBINED AT	CON3R	.17	1	FLOW	191. 3.67	187. 3.67	178. 3.67	170. 3.67	167. 3.67	165. 3.67	163. 3.67	161. 3.67	65. 3.75
HYDROGRAPH AT	ON5	.01	1	FLOW	18. 3.50	18. 3.58	17. 3.58	16. 3.58	16. 3.58	16. 3.58	16. 3.58	16. 3.58	7. 3.58
HYDROGRAPH AT	57B-3C	.01	1	FLOW	11. 3.58	10. 3.58	10. 3.58	10. 3.58	9. 3.58	9. 3.58	9. 3.58	9. 3.58	4. 3.58
HYDROGRAPH AT	ON6	.00	1	FLOW	8. 3.50	8. 3.50	8. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	4. 3.50
+ 2 COMBINED AT	CON6	.01	1	FLOW	18. 3.50	18. 3.50	17. 3.50	16. 3.50	16. 3.50	16. 3.50	16. 3.50	16. 3.50	8. 3.50
+ 2 COMBINED AT	CCON6	.03	1	FLOW	36. 3.50	36. 3.50	34. 3.50	33. 3.50	32. 3.50	32. 3.50	32. 3.50	31. 3.50	14. 3.50
ROUTED TO	RCCON6	.03	1	FLOW	34. 3.67	33. 3.67	32. 3.67	31. 3.67	30. 3.67	30. 3.67	30. 3.67	29. 3.67	14. 3.67
HYDROGRAPH AT	ON8	.02	1	FLOW	27. 3.50	26. 3.50	25. 3.50	24. 3.50	23. 3.50	23. 3.50	23. 3.50	22. 3.50	9. 3.50
+ 2 COMBINED AT	CON8	.04	1	FLOW	54. 3.58	53. 3.58	50. 3.58	48. 3.58	47. 3.58	47. 3.58	46. 3.58	46. 3.58	19. 3.67
HYDROGRAPH AT	SW11	.59	1	FLOW	759. 3.75	743. 3.75	717. 3.75	691. 3.75	680. 3.75	673. 3.75	668. 3.75	660. 3.75	330. 3.75
ROUTED TO	RSW11	.59	1	FLOW	754. 3.75	738. 3.75	712. 3.75	686. 3.75	676. 3.75	668. 3.75	663. 3.75	655. 3.75	325. 3.75
HYDROGRAPH AT	SW17	.36	1	FLOW	479. 3.67	469. 3.67	452. 3.67	436. 3.67	429. 3.67	424. 3.67	421. 3.67	416. 3.67	205. 3.67
+ 2 COMBINED AT	CSW17	.94	1	FLOW	1221. 3.75	1196. 3.75	1153. 3.75	1111. 3.75	1095. 3.75	1083. 3.75	1075. 3.75	1061. 3.75	530. 3.75
ROUTED TO	RCSW17	.94	1	FLOW	1211. 3.75	1186. 3.75	1143. 3.75	1101. 3.75	1083. 3.75	1073. 3.75	1063. 3.75	1051. 3.75	521. 3.75
HYDROGRAPH AT	SW18	.41	1	FLOW	519. 3.67	507. 3.67	489. 3.67	470. 3.67	463. 3.67	457. 3.67	454. 3.67	448. 3.67	215. 3.75
+ 2 COMBINED AT	CSW18	1.35	1	FLOW	1718. 3.75	1682. 3.75	1622. 3.75	1562. 3.75	1537. 3.75	1521. 3.75	1508. 3.75	1490. 3.75	736. 3.75
ROUTED TO	RCSW18	1.35	1	FLOW	1610. 3.92	1576. 3.92	1520. 3.92	1464. 3.92	1441. 3.92	1426. 3.92	1414. 3.92	1397. 3.92	690. 3.92
HYDROGRAPH AT	12A	.39	1	FLOW	576. 3.67	565. 3.67	547. 3.67	529. 3.67	521. 3.67	516. 3.67	513. 3.67	507. 3.67	272. 3.67
+ 2 COMBINED AT	C12A	1.74	1	FLOW	2046. 3.83	2003. 3.83	1932. 3.83	1861. 3.83	1832. 3.83	1813. 3.83	1798. 3.83	1776. 3.83	881. 3.83
ROUTED TO	RC12A	1.74	1	FLOW	2025. 3.92	1983. 3.92	1913. 3.92	1843. 3.92	1815. 3.92	1796. 3.92	1782. 3.92	1760. 3.92	880. 3.92
HYDROGRAPH AT	12B	.26	1	FLOW	387. 3.67	380. 3.67	367. 3.67	355. 3.67	350. 3.67	347. 3.67	344. 3.67	340. 3.67	182. 3.67
+ 2 COMBINED AT	C12B	2.00	1	FLOW	2259. 3.83	2212. 3.83	2134. 3.83	2056. 3.83	2024. 3.83	2002. 3.83	1987. 3.83	1962. 3.83	990. 3.92
HYDROGRAPH AT	57B-2A	.01	1	FLOW	14. 3.58	14. 3.58	13. 3.58	13. 3.58	13. 3.58	13. 3.58	12. 3.58	12. 3.58	6. 3.58
HYDROGRAPH AT	57B-3F	.01	1	FLOW	17. 3.58	17. 3.58	16. 3.58	16. 3.58	15. 3.58	15. 3.58	15. 3.58	15. 3.58	7. 3.58
HYDROGRAPH AT	57B-3E	.03	1	FLOW	32. 3.67	31. 3.67	30. 3.67	29. 3.67	29. 3.67	28. 3.67	28. 3.67	28. 3.67	13. 3.67
HYDROGRAPH AT	ON9	.04	1	FLOW	41. 3.67	40. 3.67	38. 3.67	36. 3.67	36. 3.67	35. 3.67	35. 3.67	34. 3.67	14. 3.67
+ 5 COMBINED AT	CON9	2.09	1	FLOW	2330. 3.83	2281. 3.83	2200. 3.83	2120. 3.83	2087. 3.83	2064. 3.83	2048. 3.83	2023. 3.83	1012. 3.92

PROPOSED . OUT													
ROUTED TO +	RCON9	2.09	1	FLOW TIME	2307. 3.92	2259. 3.92	2181. 3.92	2103. 3.92	2071. 3.92	2048. 3.92	2032. 3.92	2007. 3.92	1012. 3.92
HYDROGRAPH AT +	57B-3G	.00	1	FLOW TIME	4. 3.50	4. 3.50	4. 3.50	4. 3.50	4. 3.50	4. 3.50	3. 3.50	3. 3.50	2. 3.50
HYDROGRAPH AT +	57B-2B	.00	1	FLOW TIME	8. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	7. 3.50	3. 3.50
HYDROGRAPH AT +	57B-2C	.00	1	FLOW TIME	5. 3.50	5. 3.50	4. 3.50	4. 3.50	4. 3.50	4. 3.50	4. 3.50	4. 3.50	2. 3.50
HYDROGRAPH AT +	ON10	.02	1	FLOW TIME	24. 3.50	23. 3.50	22. 3.50	21. 3.50	21. 3.50	21. 3.50	21. 3.50	20. 3.50	8. 3.50
5 COMBINED AT +	CON10	2.12	1	FLOW TIME	2314. 3.92	2266. 3.92	2188. 3.92	2110. 3.92	2077. 3.92	2055. 3.92	2039. 3.92	2014. 3.92	1015. 3.92
2 COMBINED AT +	CCON10	2.16	1	FLOW TIME	2335. 3.92	2286. 3.92	2208. 3.92	2128. 3.92	2096. 3.92	2073. 3.92	2057. 3.92	2032. 3.92	1025. 3.92
HYDROGRAPH AT +	ON11R	.01	1	FLOW TIME	11. 3.50	11. 3.50	10. 3.50	10. 3.50	10. 3.50	9. 3.50	9. 3.50	9. 3.50	4. 3.50
2 COMBINED AT +	CON11R	2.17	1	FLOW TIME	2337. 3.92	2288. 3.92	2209. 3.92	2130. 3.92	2098. 3.92	2075. 3.92	2059. 3.92	2033. 3.92	1026. 3.92
HYDROGRAPH AT +	57B-2D	.01	1	FLOW TIME	16. 3.58	15. 3.58	15. 3.58	14. 3.58	14. 3.58	14. 3.58	14. 3.58	14. 3.58	7. 3.58
HYDROGRAPH AT +	57B-2E	.02	1	FLOW TIME	42. 3.50	41. 3.50	40. 3.50	38. 3.50	38. 3.50	37. 3.50	37. 3.50	37. 3.50	19. 3.50
2 COMBINED AT +	C57B-2E	.03	1	FLOW TIME	56. 3.50	55. 3.50	53. 3.50	52. 3.50	51. 3.50	50. 3.50	50. 3.50	49. 3.50	26. 3.50
HYDROGRAPH AT +	57B-2G1	.00	1	FLOW TIME	5. 3.50	5. 3.50	5. 3.50	5. 3.50	5. 3.50	4. 3.50	4. 3.50	4. 3.50	2. 3.50
HYDROGRAPH AT +	ON12	.02	1	FLOW TIME	23. 3.58	23. 3.58	22. 3.58	21. 3.58	20. 3.58	20. 3.58	20. 3.58	20. 3.58	8. 3.58
3 COMBINED AT +	CON12	.05	1	FLOW TIME	83. 3.50	81. 3.50	78. 3.50	75. 3.50	74. 3.50	73. 3.50	73. 3.50	72. 3.50	36. 3.58
HYDROGRAPH AT +	57B-2G2	.01	1	FLOW TIME	12. 3.50	11. 3.50	11. 3.50	11. 3.50	10. 3.50	10. 3.50	10. 3.50	10. 3.50	5. 3.50
HYDROGRAPH AT +	ON13	.02	1	FLOW TIME	23. 3.58	23. 3.58	22. 3.58	21. 3.58	21. 3.58	20. 3.58	20. 3.58	20. 3.58	8. 3.58
3 COMBINED AT +	CON13	.08	1	FLOW TIME	118. 3.50	115. 3.50	111. 3.50	107. 3.50	105. 3.50	104. 3.50	103. 3.50	101. 3.50	49. 3.58
HYDROGRAPH AT +	57B-2F	.09	1	FLOW TIME	147. 3.58	145. 3.58	140. 3.58	135. 3.58	133. 3.58	132. 3.58	131. 3.58	129. 3.58	69. 3.58
HYDROGRAPH AT +	57B-2H2	.02	1	FLOW TIME	21. 3.58	21. 3.58	20. 3.58	19. 3.58	19. 3.58	19. 3.58	19. 3.58	18. 3.58	9. 3.58
HYDROGRAPH AT +	ON14	.01	1	FLOW TIME	6. 3.58	5. 3.58	5. 3.58	5. 3.58	5. 3.58	5. 3.58	5. 3.58	5. 3.58	2. 3.67
3 COMBINED AT +	CON14	.11	1	FLOW TIME	174. 3.58	171. 3.58	165. 3.58	159. 3.58	157. 3.58	155. 3.58	154. 3.58	152. 3.58	79. 3.58
ROUTED TO +	RCON14	.11	1	FLOW TIME	166. 3.67	163. 3.67	158. 3.67	156. 3.67	153. 3.67	152. 3.67	151. 3.67	146. 3.67	79. 3.67
HYDROGRAPH AT +	57B-2I	.01	1	FLOW TIME	12. 3.50	11. 3.50	11. 3.50	10. 3.50	10. 3.50	10. 3.50	10. 3.50	10. 3.50	5. 3.50
HYDROGRAPH AT +	57B-2H1	.03	1	FLOW TIME	32. 3.75	31. 3.75	30. 3.75	29. 3.75	29. 3.75	28. 3.75	28. 3.75	28. 3.75	13. 3.75
HYDROGRAPH AT +	ON15R	.03	1	FLOW TIME	41. 3.58	40. 3.58	38. 3.58	36. 3.58	36. 3.58	35. 3.58	35. 3.58	34. 3.58	14. 3.58
5 COMBINED AT +	CON15R	.26	1	FLOW TIME	344. 3.58	337. 3.58	324. 3.58	312. 3.58	307. 3.58	304. 3.58	301. 3.58	297. 3.58	142. 3.58
HYDROGRAPH AT +	ON16R	.02	1	FLOW TIME	23. 3.50	22. 3.50	21. 3.50	20. 3.50	20. 3.50	20. 3.50	19. 3.50	19. 3.50	8. 3.50

PROPOSED .OUT

2 COMBINED AT	CON16R	.28	1	FLOW TIME	364. 3.58	356. 3.58	342. 3.58	330. 3.58	325. 3.58	321. 3.58	318. 3.58	313. 3.58	149. 3.58
3 COMBINED AT	CPPH1	2.61	1	FLOW TIME	2692. 3.83	2635. 3.83	2543. 3.83	2450. 3.83	2412. 3.83	2386. 3.83	2366. 3.83	2337. 3.83	1153. 3.83
HYDROGRAPH AT	DON1	.02	1	FLOW TIME	34. 3.50	34. 3.50	33. 3.50	32. 3.50	31. 3.50	31. 3.50	31. 3.50	31. 3.50	18. 3.50
HYDROGRAPH AT	DON2	.03	1	FLOW TIME	60. 3.50	59. 3.50	57. 3.50	55. 3.50	55. 3.50	54. 3.50	54. 3.50	53. 3.50	31. 3.50
3 COMBINED AT	CDON2	2.66	1	FLOW TIME	2720. 3.83	2663. 3.83	2570. 3.83	2476. 3.83	2438. 3.83	2412. 3.83	2392. 3.83	2363. 3.83	1169. 3.83
ROUTED TO	RCDON2	2.66	1	FLOW TIME	2712. 3.83	2655. 3.83	2561. 3.83	2467. 3.83	2429. 3.83	2404. 3.83	2383. 3.83	2353. 3.83	1163. 3.92
HYDROGRAPH AT	13B-1	.25	1	FLOW TIME	354. 3.67	347. 3.67	336. 3.67	325. 3.67	321. 3.67	318. 3.67	315. 3.67	312. 3.67	169. 3.75
ROUTED TO	RC13B-1	.25	1	FLOW TIME	354. 3.75	347. 3.75	336. 3.75	324. 3.75	320. 3.75	317. 3.75	314. 3.83	311. 3.83	171. 3.83
HYDROGRAPH AT	13B-2	.22	1	FLOW TIME	310. 3.67	304. 3.67	294. 3.67	283. 3.67	279. 3.67	277. 3.67	274. 3.67	271. 3.67	140. 3.67
2 COMBINED AT	C13B-2	.47	1	FLOW TIME	634. 3.75	622. 3.75	602. 3.75	581. 3.75	573. 3.75	567. 3.75	563. 3.75	557. 3.75	294. 3.75
ROUTED TO	RC13B-2	.47	1	FLOW TIME	641. 3.83	628. 3.83	607. 3.83	586. 3.83	578. 3.83	572. 3.83	568. 3.83	561. 3.83	295. 3.92
HYDROGRAPH AT	19A	.25	1	FLOW TIME	318. 3.75	312. 3.75	301. 3.75	291. 3.75	287. 3.75	284. 3.75	282. 3.75	278. 3.75	144. 3.75
ROUTED TO	R19A	.25	1	FLOW TIME	319. 3.92	313. 3.92	302. 3.92	292. 3.92	288. 3.92	285. 3.92	283. 3.92	280. 3.92	146. 3.92
HYDROGRAPH AT	13A-1	.22	1	FLOW TIME	308. 3.75	303. 3.75	293. 3.75	283. 3.75	279. 3.75	277. 3.75	275. 3.75	272. 3.75	147. 3.75
2 COMBINED AT	C13A-1	.48	1	FLOW TIME	595. 3.83	583. 3.83	564. 3.83	545. 3.83	537. 3.83	532. 3.83	528. 3.83	522. 3.83	273. 3.83
ROUTED TO	RC13A-1	.48	1	FLOW TIME	581. 3.92	569. 3.92	551. 3.92	532. 3.92	524. 3.92	519. 3.92	515. 3.92	509. 3.92	268. 3.92
HYDROGRAPH AT	13A-2	.19	1	FLOW TIME	272. 3.67	267. 3.67	258. 3.67	249. 3.67	246. 3.67	243. 3.67	241. 3.67	238. 3.67	124. 3.67
2 COMBINED AT	C13A-2	.66	1	FLOW TIME	782. 3.83	766. 3.83	740. 3.83	715. 3.83	704. 3.83	697. 3.83	692. 3.83	684. 3.83	354. 3.83
ROUTED TO	RC13A-2	.66	1	FLOW TIME	781. 3.92	765. 3.92	738. 3.92	712. 3.92	702. 3.92	694. 3.92	689. 3.92	681. 3.92	354. 4.00
HYDROGRAPH AT	PIC-C	.24	1	FLOW TIME	280. 3.83	274. 3.83	265. 3.83	256. 3.83	252. 3.83	250. 3.83	248. 3.83	245. 3.83	129. 3.83
2 COMBINED AT	CPIC-C	.91	1	FLOW TIME	1041. 3.92	1020. 3.92	985. 3.92	951. 3.92	937. 3.92	927. 3.92	920. 3.92	909. 3.92	462. 3.92
ROUTED TO	RCPIC-C	.91	1	FLOW TIME	1030. 3.92	1009. 3.92	975. 3.92	940. 3.92	922. 3.92	915. 3.92	908. 3.92	896. 3.92	461. 4.00
HYDROGRAPH AT	PIC-A	.36	1	FLOW TIME	356. 3.92	349. 3.92	338. 3.92	326. 3.92	322. 3.92	318. 3.92	316. 3.92	312. 3.92	165. 3.92
2 COMBINED AT	CPIC-A	1.27	1	FLOW TIME	1386. 3.92	1359. 3.92	1313. 3.92	1266. 3.92	1243. 3.92	1233. 3.92	1224. 3.92	1208. 3.92	625. 4.00
2 COMBINED AT	CCPIC-A	1.73	1	FLOW TIME	1997. 3.92	1959. 3.92	1895. 3.92	1830. 3.92	1800. 3.92	1785. 3.92	1772. 3.92	1750. 3.92	900. 4.00
HYDROGRAPH AT	ON18R	.03	1	FLOW TIME	28. 3.67	28. 3.67	27. 3.67	25. 3.67	25. 3.67	25. 3.67	24. 3.67	24. 3.67	10. 3.67
2 COMBINED AT	CON18R	1.76	1	FLOW TIME	2013. 3.92	1975. 3.92	1910. 3.92	1844. 3.92	1814. 3.92	1799. 3.92	1786. 3.92	1763. 3.92	905. 4.00
HYDROGRAPH AT	57B-1A	.04	1	FLOW TIME	54. 3.58	53. 3.58	51. 3.58	48. 3.58	48. 3.58	47. 3.58	47. 3.58	46. 3.58	20. 3.58

PROPOSED .OUT

+	2 COMBINED AT	CCON18R	1.81	1	FLOW TIME	2037. 3.92	1998. 3.92	1933. 3.92	1866. 3.92	1836. 3.92	1820. 3.92	1807. 3.92	1784. 3.92	913. 4.00
+	ROUTED TO	RCCON18R	1.81	1	FLOW TIME	2026. 3.92	1983. 3.92	1915. 3.92	1848. 3.92	1823. 3.92	1804. 3.92	1787. 3.92	1767. 3.92	913. 4.00
+	HYDROGRAPH AT	57B-1B	.03	1	FLOW TIME	51. 3.58	50. 3.58	49. 3.58	47. 3.58	47. 3.58	46. 3.58	46. 3.58	45. 3.58	25. 3.58
+	2 COMBINED AT	CP19	1.84	1	FLOW TIME	2043. 3.92	1999. 3.92	1931. 3.92	1863. 3.92	1838. 3.92	1819. 3.92	1802. 3.92	1782. 3.92	920. 4.00
+	HYDROGRAPH AT	57B-1C	.00	1	FLOW TIME	2. 3.50	2. 3.50	2. 3.50	2. 3.50	2. 3.50	2. 3.50	2. 3.50	2. 3.50	1. 3.50
+	2 COMBINED AT	CP20	1.84	1	FLOW TIME	2043. 3.92	2000. 3.92	1932. 3.92	1864. 3.92	1839. 3.92	1819. 3.92	1802. 3.92	1782. 3.92	920. 4.00
+	HYDROGRAPH AT	DON3	.03	1	FLOW TIME	65. 3.50	64. 3.50	62. 3.50	60. 3.50	59. 3.50	59. 3.50	58. 3.50	58. 3.50	34. 3.50
+	3 COMBINED AT	CDON3	4.53	1	FLOW TIME	4694. 3.92	4597. 3.92	4440. 3.92	4283. 3.92	4221. 3.92	4177. 3.92	4141. 3.92	4092. 3.92	2057. 3.92
+	ROUTED TO	RCDON3	4.53	1	FLOW TIME	4670. 3.92	4572. 3.92	4412. 3.92	4253. 3.92	4186. 3.92	4135. 3.92	4103. 3.92	4063. 3.92	2046. 4.00
+	HYDROGRAPH AT	DON4	.03	1	FLOW TIME	44. 3.58	43. 3.58	42. 3.58	41. 3.58	40. 3.58	40. 3.58	40. 3.58	39. 3.58	23. 3.58
+	HYDROGRAPH AT	57B-4B	.01	1	FLOW TIME	24. 3.50	24. 3.50	23. 3.50	22. 3.50	22. 3.50	22. 3.50	22. 3.50	22. 3.50	13. 3.50
+	HYDROGRAPH AT	57B-4C	.01	1	FLOW TIME	23. 3.50	22. 3.50	22. 3.50	21. 3.50	21. 3.50	21. 3.50	21. 3.50	20. 3.50	12. 3.58
+	2 COMBINED AT	C57B-4C	.02	1	FLOW TIME	47. 3.50	46. 3.50	45. 3.50	43. 3.50	43. 3.50	43. 3.50	42. 3.50	42. 3.50	25. 3.50
+	3 COMBINED AT	CDON4	4.58	1	FLOW TIME	4700. 3.92	4602. 3.92	4441. 3.92	4281. 3.92	4214. 3.92	4162. 3.92	4130. 3.92	4089. 3.92	2059. 4.00
+	HYDROGRAPH AT	57B-1	.05	1	FLOW TIME	80. 3.58	79. 3.58	76. 3.58	74. 3.58	73. 3.58	72. 3.58	72. 3.58	71. 3.58	40. 3.58
+	HYDROGRAPH AT	PIC-B	.44	1	FLOW TIME	442. 3.92	433. 3.92	419. 3.92	405. 3.92	399. 3.92	395. 3.92	392. 3.92	388. 3.92	205. 3.92
+	ROUTED TO	RPIC-B	.44	1	FLOW TIME	439. 3.92	431. 3.92	416. 3.92	402. 3.92	396. 3.92	392. 3.92	390. 3.92	385. 3.92	202. 3.92
+	HYDROGRAPH AT	57B-3	.05	1	FLOW TIME	63. 3.67	62. 3.67	60. 3.67	58. 3.67	57. 3.67	56. 3.67	56. 3.67	55. 3.67	28. 3.67
+	HYDROGRAPH AT	57B-4	.13	1	FLOW TIME	202. 3.58	198. 3.58	192. 3.58	186. 3.58	184. 3.58	182. 3.58	181. 3.58	179. 3.58	101. 3.58
+	2 COMBINED AT	C57B-4	.18	1	FLOW TIME	259. 3.58	254. 3.58	246. 3.67	238. 3.67	235. 3.67	233. 3.67	232. 3.67	229. 3.67	127. 3.67
+	4 COMBINED AT	CC57B-4	5.25	1	FLOW TIME	5310. 3.92	5200. 3.92	5020. 3.92	4841. 3.92	4766. 3.92	4709. 3.92	4673. 3.92	4626. 3.92	2326. 4.00

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SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL PEAK	TIME TO PEAK	VOLUME
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
FOR PLAN = 1	RCON1	RATIO= .00	85.62	225.00	1.50	5.00	85.62	225.00	1.50
	MANE	5.00							

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5242E+01 EXCESS= .0000E+00 OUTFLOW= .5262E+01 BASIN STORAGE= .6505E-02 PERCENT ERROR= -.5

FOR PLAN = 1	RCON1	RATIO= .00	83.65	225.00	1.47	5.00	83.65	225.00	1.47
	MANE	5.00							

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5111E+01 EXCESS= .0000E+00 OUTFLOW= .5131E+01 BASIN STORAGE= .6457E-02 PERCENT ERROR= -.5

FOR PLAN = 1	RCON1	RATIO= .00	80.35	225.00	1.40	5.00	80.35	225.00	1.40
	MANE	5.00							

PROPOSED.OUT

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4894E+01 EXCESS= .0000E+00 OUTFLOW= .4914E+01 BASIN STORAGE= .6374E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RCON1 MANE 5.00 77.02 225.00 1.34 5.00 77.02 225.00 1.34

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4680E+01 EXCESS= .0000E+00 OUTFLOW= .4699E+01 BASIN STORAGE= .6290E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RCON1 MANE 5.00 75.69 225.00 1.32 5.00 75.69 225.00 1.32

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4594E+01 EXCESS= .0000E+00 OUTFLOW= .4613E+01 BASIN STORAGE= .6256E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RCON1 MANE 5.00 74.75 225.00 1.30 5.00 74.75 225.00 1.30

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4535E+01 EXCESS= .0000E+00 OUTFLOW= .4553E+01 BASIN STORAGE= .6232E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RCON1 MANE 5.00 74.08 225.00 1.29 5.00 74.08 225.00 1.29

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4492E+01 EXCESS= .0000E+00 OUTFLOW= .4511E+01 BASIN STORAGE= .6038E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RCON1 MANE 5.00 73.00 225.00 1.27 5.00 73.00 225.00 1.27

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4425E+01 EXCESS= .0000E+00 OUTFLOW= .4442E+01 BASIN STORAGE= .6011E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RCON1 MANE 4.00 31.17 228.00 .55 5.00 30.06 230.00 .54

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1896E+01 EXCESS= .0000E+00 OUTFLOW= .1909E+01 BASIN STORAGE= .5556E-02 PERCENT ERROR= -1.0

FOR PLAN = 1 RATIO= .00
RCON6 MANE 4.25 34.85 216.75 1.61 5.00 33.88 220.00 1.61

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2157E+01 EXCESS= .0000E+00 OUTFLOW= .2162E+01 BASIN STORAGE= .2734E-02 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RCON6 MANE 4.25 34.03 216.75 1.58 5.00 33.16 220.00 1.57

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2106E+01 EXCESS= .0000E+00 OUTFLOW= .2111E+01 BASIN STORAGE= .2708E-02 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RCON6 MANE 4.25 32.67 216.75 1.51 5.00 31.96 220.00 1.51

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2022E+01 EXCESS= .0000E+00 OUTFLOW= .2026E+01 BASIN STORAGE= .2664E-02 PERCENT ERROR= -.3

FOR PLAN = 1 RATIO= .00
RCON6 MANE 4.25 31.31 216.75 1.45 5.00 30.75 220.00 1.45

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1938E+01 EXCESS= .0000E+00 OUTFLOW= .1942E+01 BASIN STORAGE= .2619E-02 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .00
RCON6 MANE 4.25 30.77 216.75 1.43 5.00 30.27 220.00 1.42

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1905E+01 EXCESS= .0000E+00 OUTFLOW= .1909E+01 BASIN STORAGE= .2601E-02 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .00
RCON6 MANE 4.25 30.39 216.75 1.41 5.00 29.93 220.00 1.41

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1881E+01 EXCESS= .0000E+00 OUTFLOW= .1886E+01 BASIN STORAGE= .2588E-02 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .00
RCON6 MANE 4.25 30.11 216.75 1.40 5.00 29.69 220.00 1.39

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1865E+01 EXCESS= .0000E+00 OUTFLOW= .1869E+01 BASIN STORAGE= .2579E-02 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .00
RCON6 MANE 4.25 29.68 216.75 1.38 5.00 29.30 220.00 1.37

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1838E+01 EXCESS= .0000E+00 OUTFLOW= .1842E+01 BASIN STORAGE= .2564E-02 PERCENT ERROR= -.4

FOR PLAN = 1 RATIO= .00
RCON6 MANE 3.75 14.36 221.25 .63 5.00 14.02 220.00 .63

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8405E+00 EXCESS= .0000E+00 OUTFLOW= .8424E+00 BASIN STORAGE= .2039E-02 PERCENT ERROR= -.5

FOR PLAN = 1 RATIO= .00
RSW11 MANE 1.02 755.16 226.24 2.08 5.00 753.82 225.00 2.08

					PROPOSED	OUT							
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.6522E+02	EXCESS=	.0000E+00	OUTFLOW=	.6522E+02	BASIN STORAGE=	.1654E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00											
RSW11	MANE	1.03	740.95	226.07	2.03	5.00	738.42	225.00	2.03				
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.6380E+02	EXCESS=	.0000E+00	OUTFLOW=	.6381E+02	BASIN STORAGE=	.1696E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00											
RSW11	MANE	1.05	714.15	226.19	1.96	5.00	712.14	225.00	1.96				
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.6145E+02	EXCESS=	.0000E+00	OUTFLOW=	.6145E+02	BASIN STORAGE=	.1622E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00											
RSW11	MANE	1.06	686.99	226.38	1.88	5.00	685.95	225.00	1.88				
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.5911E+02	EXCESS=	.0000E+00	OUTFLOW=	.5911E+02	BASIN STORAGE=	.1763E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00											
RSW11	MANE	1.07	677.33	225.62	1.85	5.00	675.73	225.00	1.85				
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.5818E+02	EXCESS=	.0000E+00	OUTFLOW=	.5818E+02	BASIN STORAGE=	.1832E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00											
RSW11	MANE	1.07	669.72	225.52	1.83	5.00	668.38	225.00	1.83				
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.5752E+02	EXCESS=	.0000E+00	OUTFLOW=	.5752E+02	BASIN STORAGE=	.1613E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00											
RSW11	MANE	1.08	665.29	226.22	1.82	5.00	663.31	225.00	1.82				
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.5706E+02	EXCESS=	.0000E+00	OUTFLOW=	.5706E+02	BASIN STORAGE=	.1791E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00											
RSW11	MANE	1.08	656.69	226.27	1.79	5.00	654.91	225.00	1.79				
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.5631E+02	EXCESS=	.0000E+00	OUTFLOW=	.5632E+02	BASIN STORAGE=	.1761E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00											
RSW11	MANE	1.43	328.10	225.73	.88	5.00	324.89	225.00	.88				
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2754E+02	EXCESS=	.0000E+00	OUTFLOW=	.2754E+02	BASIN STORAGE=	.1787E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00											
RCSW17	MANE	1.65	1211.98	225.57	2.06	5.00	1210.68	225.00	2.06				
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.1040E+03	EXCESS=	.0000E+00	OUTFLOW=	.1040E+03	BASIN STORAGE=	.3928E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00											
RCSW17	MANE	1.66	1187.90	225.78	2.02	5.00	1185.71	225.00	2.02				
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.1018E+03	EXCESS=	.0000E+00	OUTFLOW=	.1018E+03	BASIN STORAGE=	.3507E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00											
RCSW17	MANE	1.68	1144.91	225.68	1.94	5.00	1143.40	225.00	1.94				
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9799E+02	EXCESS=	.0000E+00	OUTFLOW=	.9800E+02	BASIN STORAGE=	.3522E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00											
RCSW17	MANE	1.71	1102.37	225.64	1.87	5.00	1101.22	225.00	1.87				
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9424E+02	EXCESS=	.0000E+00	OUTFLOW=	.9424E+02	BASIN STORAGE=	.3477E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00											
RCSW17	MANE	1.72	1087.77	227.00	1.84	5.00	1083.30	225.00	1.84				
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9278E+02	EXCESS=	.0000E+00	OUTFLOW=	.9279E+02	BASIN STORAGE=	.3927E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00											
RCSW17	MANE	1.73	1077.08	226.26	1.82	5.00	1072.79	225.00	1.82				
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9172E+02	EXCESS=	.0000E+00	OUTFLOW=	.9173E+02	BASIN STORAGE=	.3817E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00											
RCSW17	MANE	1.73	1069.06	226.95	1.81	5.00	1062.80	225.00	1.81				
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9100E+02	EXCESS=	.0000E+00	OUTFLOW=	.9101E+02	BASIN STORAGE=	.3937E-02	PERCENT ERROR=	.0			
FOR PLAN = 1	RATIO=	.00											
RCSW17	MANE	1.74	1055.75	226.36	1.78	5.00	1050.97	225.00	1.78				

										PROPOSED.OUT		
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8979E+02 EXCESS= .0000E+00										OUTFLOW= .8980E+02	BASIN STORAGE= .3511E-02	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCSW17	MANE	2.30	524.06	227.64	.87	5.00	520.91	225.00	.87			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4386E+02 EXCESS= .0000E+00										OUTFLOW= .4387E+02	BASIN STORAGE= .3897E-02	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCON9	MANE	1.67	2325.51	231.44	2.07	5.00	2306.80	235.00	2.07			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2301E+03 EXCESS= .0000E+00										OUTFLOW= .2301E+03	BASIN STORAGE= .3123E-02	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCON9	MANE	1.68	2279.65	231.56	2.02	5.00	2258.94	235.00	2.02			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2252E+03 EXCESS= .0000E+00										OUTFLOW= .2252E+03	BASIN STORAGE= .2858E-02	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCON9	MANE	1.70	2197.90	232.94	1.95	5.00	2181.01	235.00	1.95			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2170E+03 EXCESS= .0000E+00										OUTFLOW= .2170E+03	BASIN STORAGE= .2984E-02	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCON9	MANE	1.72	2118.94	232.70	1.87	5.00	2102.63	235.00	1.88			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2088E+03 EXCESS= .0000E+00										OUTFLOW= .2088E+03	BASIN STORAGE= .3195E-02	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCON9	MANE	1.73	2088.03	232.28	1.85	5.00	2070.54	235.00	1.85			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2056E+03 EXCESS= .0000E+00										OUTFLOW= .2056E+03	BASIN STORAGE= .2784E-02	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCON9	MANE	1.74	2062.77	233.22	1.83	5.00	2047.86	235.00	1.83			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2033E+03 EXCESS= .0000E+00										OUTFLOW= .2033E+03	BASIN STORAGE= .2736E-02	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCON9	MANE	1.75	2050.03	232.14	1.81	5.00	2032.41	235.00	1.81			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2017E+03 EXCESS= .0000E+00										OUTFLOW= .2017E+03	BASIN STORAGE= .2832E-02	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCON9	MANE	1.75	2021.32	233.22	1.79	5.00	2006.95	235.00	1.79			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1991E+03 EXCESS= .0000E+00										OUTFLOW= .1991E+03	BASIN STORAGE= .2680E-02	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCON9	MANE	2.26	1012.15	235.03	.89	5.00	1012.06	235.00	.89			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9869E+02 EXCESS= .0000E+00										OUTFLOW= .9869E+02	BASIN STORAGE= .3005E-02	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCON14	MANE	4.25	167.38	221.00	1.99	5.00	166.33	220.00	1.99			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1179E+02 EXCESS= .0000E+00										OUTFLOW= .1181E+02	BASIN STORAGE= .2635E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RCON14	MANE	4.25	164.16	221.00	1.95	5.00	163.07	220.00	1.95			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1155E+02 EXCESS= .0000E+00										OUTFLOW= .1156E+02	BASIN STORAGE= .2609E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RCON14	MANE	4.25	158.77	221.00	1.88	5.00	157.63	220.00	1.88			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1114E+02 EXCESS= .0000E+00										OUTFLOW= .1115E+02	BASIN STORAGE= .2565E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RCON14	MANE	4.00	155.50	220.00	1.81	5.00	155.50	220.00	1.81			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1074E+02 EXCESS= .0000E+00										OUTFLOW= .1075E+02	BASIN STORAGE= .2457E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RCON14	MANE	4.00	153.27	220.00	1.78	5.00	153.27	220.00	1.79			
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1057E+02 EXCESS= .0000E+00										OUTFLOW= .1059E+02	BASIN STORAGE= .2440E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RCON14	MANE	4.00	151.72	220.00	1.77	5.00	151.72	220.00	1.77			

										PROPOSED.OUT		
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1046E+02 EXCESS= .0000E+00										OUTFLOW= .1047E+02	BASIN STORAGE= .2427E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RCON14 MANE 4.00										150.60	220.00	1.75
										5.00	150.60	220.00
										1.75		
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1038E+02 EXCESS= .0000E+00										OUTFLOW= .1039E+02	BASIN STORAGE= .2418E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RCON14 MANE 4.25										146.92	221.00	1.73
										5.00	145.67	220.00
										1.73		
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1024E+02 EXCESS= .0000E+00										OUTFLOW= .1025E+02	BASIN STORAGE= .2466E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RCON14 MANE 5.00										78.65	220.00	.88
										5.00	78.65	220.00
										.88		
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5186E+01 EXCESS= .0000E+00										OUTFLOW= .5194E+01	BASIN STORAGE= .2404E-02	PERCENT ERROR= -.2
FOR PLAN = 1 RATIO= .00												
RCDON2 MANE .81										2715.41	230.47	1.99
										5.00	2711.59	230.00
										1.99		
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2819E+03 EXCESS= .0000E+00										OUTFLOW= .2819E+03	BASIN STORAGE= .2945E-03	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCDON2 MANE .81										2659.57	230.89	1.94
										5.00	2655.45	230.00
										1.94		
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2758E+03 EXCESS= .0000E+00										OUTFLOW= .2758E+03	BASIN STORAGE= .3285E-03	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCDON2 MANE .82										2565.17	230.51	1.87
										5.00	2560.89	230.00
										1.87		
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2656E+03 EXCESS= .0000E+00										OUTFLOW= .2656E+03	BASIN STORAGE= .3058E-03	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCDON2 MANE .83										2471.39	231.01	1.80
										5.00	2467.47	230.00
										1.80		
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2556E+03 EXCESS= .0000E+00										OUTFLOW= .2556E+03	BASIN STORAGE= .2937E-03	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCDON2 MANE .83										2432.44	231.09	1.77
										5.00	2428.86	230.00
										1.77		
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2516E+03 EXCESS= .0000E+00										OUTFLOW= .2516E+03	BASIN STORAGE= .2918E-03	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCDON2 MANE .83										2408.58	230.88	1.75
										5.00	2403.63	230.00
										1.75		
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2487E+03 EXCESS= .0000E+00										OUTFLOW= .2487E+03	BASIN STORAGE= .3212E-03	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCDON2 MANE .84										2387.66	230.52	1.74
										5.00	2382.98	230.00
										1.74		
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2467E+03 EXCESS= .0000E+00										OUTFLOW= .2467E+03	BASIN STORAGE= .2967E-03	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCDON2 MANE .84										2357.46	230.40	1.72
										5.00	2353.39	230.00
										1.72		
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2435E+03 EXCESS= .0000E+00										OUTFLOW= .2435E+03	BASIN STORAGE= .3233E-03	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RCDON2 MANE 1.00										1168.71	231.97	.84
										5.00	1162.81	235.00
										.84		
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1196E+03 EXCESS= .0000E+00										OUTFLOW= .1196E+03	BASIN STORAGE= .3200E-03	PERCENT ERROR= .0
FOR PLAN = 1 RATIO= .00												
RC13B-1 MANE 5.00										353.60	225.00	2.27
										5.00	353.60	225.00
										2.27		
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3020E+02 EXCESS= .0000E+00										OUTFLOW= .3021E+02	BASIN STORAGE= .1566E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RC13B-1 MANE 5.00										346.83	225.00	2.23
										5.00	346.83	225.00
										2.23		
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2960E+02 EXCESS= .0000E+00										OUTFLOW= .2961E+02	BASIN STORAGE= .1548E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RC13B-1 MANE 5.00										335.54	225.00	2.15
										5.00	335.54	225.00
										2.15		
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2860E+02 EXCESS= .0000E+00										OUTFLOW= .2861E+02	BASIN STORAGE= .1518E-02	PERCENT ERROR= -.1
FOR PLAN = 1 RATIO= .00												
RC13B-1 MANE 5.00										324.25	225.00	2.08
										5.00	324.25	225.00
										2.08		

					PROPOSED	OUT						
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2760E+02	EXCESS=	.0000E+00	OUTFLOW=	.2762E+02	BASIN STORAGE=	.1489E-02	PERCENT ERROR=	-.1		
FOR PLAN = 1	RATIO=	.00										
RC13B-1	MANE	5.00	319.73	225.00	2.05	5.00	319.73	225.00	2.05			
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2721E+02	EXCESS=	.0000E+00	OUTFLOW=	.2722E+02	BASIN STORAGE=	.1476E-02	PERCENT ERROR=	-.1		
FOR PLAN = 1	RATIO=	.00										
RC13B-1	MANE	5.00	316.57	225.00	2.03	5.00	316.57	225.00	2.03			
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2693E+02	EXCESS=	.0000E+00	OUTFLOW=	.2694E+02	BASIN STORAGE=	.1468E-02	PERCENT ERROR=	-.1		
FOR PLAN = 1	RATIO=	.00										
RC13B-1	MANE	5.00	314.32	230.00	2.01	5.00	314.32	230.00	2.01			
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2673E+02	EXCESS=	.0000E+00	OUTFLOW=	.2675E+02	BASIN STORAGE=	.1462E-02	PERCENT ERROR=	-.1		
FOR PLAN = 1	RATIO=	.00										
RC13B-1	MANE	5.00	310.89	230.00	1.99	5.00	310.89	230.00	1.99			
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2641E+02	EXCESS=	.0000E+00	OUTFLOW=	.2643E+02	BASIN STORAGE=	.1452E-02	PERCENT ERROR=	-.1		
FOR PLAN = 1	RATIO=	.00										
RC13B-1	MANE	5.00	171.06	230.00	1.05	5.00	171.06	230.00	1.05			
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.1391E+02	EXCESS=	.0000E+00	OUTFLOW=	.1392E+02	BASIN STORAGE=	.1716E-02	PERCENT ERROR=	-.1		
FOR PLAN = 1	RATIO=	.00										
RC13B-2	MANE	5.00	640.80	230.00	2.18	5.00	640.80	230.00	2.18			
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.5392E+02	EXCESS=	.0000E+00	OUTFLOW=	.5398E+02	BASIN STORAGE=	.5817E-02	PERCENT ERROR=	-.1		
FOR PLAN = 1	RATIO=	.00										
RC13B-2	MANE	5.00	628.20	230.00	2.13	5.00	628.20	230.00	2.13			
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.5282E+02	EXCESS=	.0000E+00	OUTFLOW=	.5288E+02	BASIN STORAGE=	.5767E-02	PERCENT ERROR=	-.1		
FOR PLAN = 1	RATIO=	.00										
RC13B-2	MANE	5.00	607.17	230.00	2.06	5.00	607.17	230.00	2.06			
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.5100E+02	EXCESS=	.0000E+00	OUTFLOW=	.5105E+02	BASIN STORAGE=	.5683E-02	PERCENT ERROR=	-.1		
FOR PLAN = 1	RATIO=	.00										
RC13B-2	MANE	5.00	586.10	230.00	1.99	5.00	586.10	230.00	1.99			
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.4918E+02	EXCESS=	.0000E+00	OUTFLOW=	.4923E+02	BASIN STORAGE=	.5597E-02	PERCENT ERROR=	-.1		
FOR PLAN = 1	RATIO=	.00										
RC13B-2	MANE	5.00	578.31	230.00	1.96	5.00	578.31	230.00	1.96			
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.4845E+02	EXCESS=	.0000E+00	OUTFLOW=	.4850E+02	BASIN STORAGE=	.7165E-02	PERCENT ERROR=	-.1		
FOR PLAN = 1	RATIO=	.00										
RC13B-2	MANE	5.00	572.39	230.00	1.94	5.00	572.39	230.00	1.94			
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.4794E+02	EXCESS=	.0000E+00	OUTFLOW=	.4799E+02	BASIN STORAGE=	.7136E-02	PERCENT ERROR=	-.1		
FOR PLAN = 1	RATIO=	.00										
RC13B-2	MANE	5.00	568.15	230.00	1.92	5.00	568.15	230.00	1.92			
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.4758E+02	EXCESS=	.0000E+00	OUTFLOW=	.4763E+02	BASIN STORAGE=	.7115E-02	PERCENT ERROR=	-.1		
FOR PLAN = 1	RATIO=	.00										
RC13B-2	MANE	5.00	561.38	230.00	1.90	5.00	561.38	230.00	1.90			
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.4700E+02	EXCESS=	.0000E+00	OUTFLOW=	.4705E+02	BASIN STORAGE=	.6748E-02	PERCENT ERROR=	-.1		
FOR PLAN = 1	RATIO=	.00										
RC13B-2	MANE	5.00	295.27	235.00	.98	5.00	295.27	235.00	.98			
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2427E+02	EXCESS=	.0000E+00	OUTFLOW=	.2430E+02	BASIN STORAGE=	.7210E-02	PERCENT ERROR=	-.1		
FOR PLAN = 1	RATIO=	.00										
R19A	MANE	5.00	318.89	235.00	2.18	5.00	318.89	235.00	2.18			
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2936E+02	EXCESS=	.0000E+00	OUTFLOW=	.2938E+02	BASIN STORAGE=	.2006E-02	PERCENT ERROR=	-.1		
FOR PLAN = 1	RATIO=	.00										
R19A	MANE	5.00	312.72	235.00	2.13	5.00	312.72	235.00	2.13			

					PROPOSED	OUT									
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2875E+02	EXCESS=	.0000E+00	OUTFLOW=	.2877E+02	BASIN STORAGE=	.1983E-02	PERCENT ERROR=	-	.1				
FOR PLAN = 1	RATIO=	.00													
R19A	MANE	5.00	302.45	235.00	2.06	5.00	302.45	235.00	2.06						
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2774E+02	EXCESS=	.0000E+00	OUTFLOW=	.2776E+02	BASIN STORAGE=	.1945E-02	PERCENT ERROR=	-	.1				
FOR PLAN = 1	RATIO=	.00													
R19A	MANE	5.00	292.17	235.00	1.98	5.00	292.17	235.00	1.98						
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2673E+02	EXCESS=	.0000E+00	OUTFLOW=	.2675E+02	BASIN STORAGE=	.1906E-02	PERCENT ERROR=	-	.1				
FOR PLAN = 1	RATIO=	.00													
R19A	MANE	5.00	288.05	235.00	1.95	5.00	288.05	235.00	1.95						
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2633E+02	EXCESS=	.0000E+00	OUTFLOW=	.2635E+02	BASIN STORAGE=	.1891E-02	PERCENT ERROR=	-	.1				
FOR PLAN = 1	RATIO=	.00													
R19A	MANE	5.00	285.17	235.00	1.93	5.00	285.17	235.00	1.93						
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2605E+02	EXCESS=	.0000E+00	OUTFLOW=	.2606E+02	BASIN STORAGE=	.1880E-02	PERCENT ERROR=	-	.1				
FOR PLAN = 1	RATIO=	.00													
R19A	MANE	5.00	283.11	235.00	1.92	5.00	283.11	235.00	1.92						
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2585E+02	EXCESS=	.0000E+00	OUTFLOW=	.2586E+02	BASIN STORAGE=	.1872E-02	PERCENT ERROR=	-	.1				
FOR PLAN = 1	RATIO=	.00													
R19A	MANE	5.00	279.82	235.00	1.89	5.00	279.82	235.00	1.89						
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2553E+02	EXCESS=	.0000E+00	OUTFLOW=	.2554E+02	BASIN STORAGE=	.1860E-02	PERCENT ERROR=	-	.1				
FOR PLAN = 1	RATIO=	.00													
R19A	MANE	5.00	146.43	235.00	.96	5.00	146.43	235.00	.96						
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.1300E+02	EXCESS=	.0000E+00	OUTFLOW=	.1300E+02	BASIN STORAGE=	.2023E-02	PERCENT ERROR=	-	.1				
FOR PLAN = 1	RATIO=	.00													
RC13A-2	MANE	5.00	780.51	235.00	2.18	5.00	780.51	235.00	2.18						
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.7731E+02	EXCESS=	.0000E+00	OUTFLOW=	.7736E+02	BASIN STORAGE=	.8795E-02	PERCENT ERROR=	-	.1				
FOR PLAN = 1	RATIO=	.00													
RC13A-2	MANE	5.00	764.75	235.00	2.14	5.00	764.75	235.00	2.14						
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.7572E+02	EXCESS=	.0000E+00	OUTFLOW=	.7577E+02	BASIN STORAGE=	.8721E-02	PERCENT ERROR=	-	.1				
FOR PLAN = 1	RATIO=	.00													
RC13A-2	MANE	5.00	738.48	235.00	2.06	5.00	738.48	235.00	2.06						
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.7309E+02	EXCESS=	.0000E+00	OUTFLOW=	.7314E+02	BASIN STORAGE=	.8303E-02	PERCENT ERROR=	-	.1				
FOR PLAN = 1	RATIO=	.00													
RC13A-2	MANE	5.00	712.20	235.00	1.99	5.00	712.20	235.00	1.99						
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.7047E+02	EXCESS=	.0000E+00	OUTFLOW=	.7051E+02	BASIN STORAGE=	.8180E-02	PERCENT ERROR=	-	.1				
FOR PLAN = 1	RATIO=	.00													
RC13A-2	MANE	5.00	701.68	235.00	1.96	5.00	701.68	235.00	1.96						
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.6942E+02	EXCESS=	.0000E+00	OUTFLOW=	.6947E+02	BASIN STORAGE=	.8130E-02	PERCENT ERROR=	-	.1				
FOR PLAN = 1	RATIO=	.00													
RC13A-2	MANE	5.00	694.32	235.00	1.94	5.00	694.32	235.00	1.94						
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.6869E+02	EXCESS=	.0000E+00	OUTFLOW=	.6873E+02	BASIN STORAGE=	.8095E-02	PERCENT ERROR=	-	.1				
FOR PLAN = 1	RATIO=	.00													
RC13A-2	MANE	5.00	689.06	235.00	1.92	5.00	689.06	235.00	1.92						
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.6817E+02	EXCESS=	.0000E+00	OUTFLOW=	.6821E+02	BASIN STORAGE=	.7878E-02	PERCENT ERROR=	-	.1				
FOR PLAN = 1	RATIO=	.00													
RC13A-2	MANE	5.00	680.64	235.00	1.90	5.00	680.64	235.00	1.90						
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.6733E+02	EXCESS=	.0000E+00	OUTFLOW=	.6738E+02	BASIN STORAGE=	.7838E-02	PERCENT ERROR=	-	.1				
FOR PLAN = 1	RATIO=	.00													
RC13A-2	MANE	5.00	353.55	240.00	.98	5.00	353.55	240.00	.98						

										PROPOSED.OUT	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.3459E+02	EXCESS=	.0000E+00	OUTFLOW=	.3462E+02	BASIN STORAGE=	.6811E-02	PERCENT ERROR=	-.1	
FOR PLAN = 1	RATIO=	.00									
RCPIC-C	MANE	2.90	1036.21	237.50	2.15	5.00	1029.58	235.00	2.15		
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.1041E+03	EXCESS=	.0000E+00	OUTFLOW=	.1041E+03	BASIN STORAGE=	.2599E-02	PERCENT ERROR=	.0	
FOR PLAN = 1	RATIO=	.00									
RCPIC-C	MANE	2.92	1018.48	236.21	2.11	5.00	1009.34	235.00	2.11		
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.1020E+03	EXCESS=	.0000E+00	OUTFLOW=	.1020E+03	BASIN STORAGE=	.2441E-02	PERCENT ERROR=	.0	
FOR PLAN = 1	RATIO=	.00									
RCPIC-C	MANE	2.95	983.10	236.05	2.03	5.00	975.10	235.00	2.03		
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9842E+02	EXCESS=	.0000E+00	OUTFLOW=	.9843E+02	BASIN STORAGE=	.3029E-02	PERCENT ERROR=	.0	
FOR PLAN = 1	RATIO=	.00									
RCPIC-C	MANE	2.99	947.55	235.94	1.96	5.00	940.20	235.00	1.96		
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9487E+02	EXCESS=	.0000E+00	OUTFLOW=	.9488E+02	BASIN STORAGE=	.2774E-02	PERCENT ERROR=	.0	
FOR PLAN = 1	RATIO=	.00									
RCPIC-C	MANE	3.00	935.30	237.12	1.93	5.00	921.65	235.00	1.93		
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9346E+02	EXCESS=	.0000E+00	OUTFLOW=	.9347E+02	BASIN STORAGE=	.2840E-02	PERCENT ERROR=	.0	
FOR PLAN = 1	RATIO=	.00									
RCPIC-C	MANE	3.01	923.69	237.96	1.91	5.00	914.93	235.00	1.91		
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9247E+02	EXCESS=	.0000E+00	OUTFLOW=	.9248E+02	BASIN STORAGE=	.2450E-02	PERCENT ERROR=	.0	
FOR PLAN = 1	RATIO=	.00									
RCPIC-C	MANE	3.02	912.75	235.55	1.90	5.00	907.94	235.00	1.89		
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9176E+02	EXCESS=	.0000E+00	OUTFLOW=	.9177E+02	BASIN STORAGE=	.2737E-02	PERCENT ERROR=	.0	
FOR PLAN = 1	RATIO=	.00									
RCPIC-C	MANE	3.03	906.65	236.52	1.87	5.00	895.54	235.00	1.87		
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9064E+02	EXCESS=	.0000E+00	OUTFLOW=	.9064E+02	BASIN STORAGE=	.3045E-02	PERCENT ERROR=	.0	
FOR PLAN = 1	RATIO=	.00									
RCPIC-C	MANE	3.82	462.80	240.43	.96	5.00	461.30	240.00	.96		
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.4647E+02	EXCESS=	.0000E+00	OUTFLOW=	.4648E+02	BASIN STORAGE=	.2735E-02	PERCENT ERROR=	.0	
FOR PLAN = 1	RATIO=	.00									
RCCON18R	MANE	2.10	2025.98	234.81	2.11	5.00	2025.84	235.00	2.11		
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.2035E+03	EXCESS=	.0000E+00	OUTFLOW=	.2035E+03	BASIN STORAGE=	.9016E-03	PERCENT ERROR=	.0	
FOR PLAN = 1	RATIO=	.00									
RCCON18R	MANE	2.11	1985.99	233.85	2.07	5.00	1982.70	235.00	2.07		
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.1994E+03	EXCESS=	.0000E+00	OUTFLOW=	.1994E+03	BASIN STORAGE=	.8716E-03	PERCENT ERROR=	.0	
FOR PLAN = 1	RATIO=	.00									
RCCON18R	MANE	2.12	1916.18	233.69	2.00	5.00	1915.28	235.00	2.00		
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.1924E+03	EXCESS=	.0000E+00	OUTFLOW=	.1924E+03	BASIN STORAGE=	.7622E-03	PERCENT ERROR=	.0	
FOR PLAN = 1	RATIO=	.00									
RCCON18R	MANE	2.14	1850.58	237.90	1.93	5.00	1847.74	235.00	1.93		
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.1855E+03	EXCESS=	.0000E+00	OUTFLOW=	.1855E+03	BASIN STORAGE=	.7102E-03	PERCENT ERROR=	.0	
FOR PLAN = 1	RATIO=	.00									
RCCON18R	MANE	2.15	1823.83	234.59	1.90	5.00	1823.05	235.00	1.90		
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.1827E+03	EXCESS=	.0000E+00	OUTFLOW=	.1827E+03	BASIN STORAGE=	.9152E-03	PERCENT ERROR=	.0	
FOR PLAN = 1	RATIO=	.00									
RCCON18R	MANE	2.16	1809.04	237.24	1.88	5.00	1803.87	235.00	1.88		
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.1807E+03	EXCESS=	.0000E+00	OUTFLOW=	.1807E+03	BASIN STORAGE=	.8510E-03	PERCENT ERROR=	.0	
FOR PLAN = 1	RATIO=	.00									
RCCON18R	MANE	2.16	1793.44	237.68	1.86	5.00	1786.79	235.00	1.86		

										PROPOSED.OUT							
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1794E+03 EXCESS= .0000E+00										OUTFLOW= .1794E+03	BASIN STORAGE= .9037E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RCCON18R MANE										2.17	1768.17	234.09	1.84	5.00	1766.93	235.00	1.84
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1772E+03 EXCESS= .0000E+00										OUTFLOW= .1772E+03	BASIN STORAGE= .7374E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RCCON18R MANE										2.57	914.14	241.11	.94	5.00	913.08	240.00	.94
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9071E+02 EXCESS= .0000E+00										OUTFLOW= .9071E+02	BASIN STORAGE= .7244E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RCDON3 MANE										2.99	4683.42	236.06	2.04	5.00	4670.40	235.00	2.04
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4932E+03 EXCESS= .0000E+00										OUTFLOW= .4932E+03	BASIN STORAGE= .1358E-02	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RCDON3 MANE										3.00	4574.67	237.31	2.00	5.00	4572.21	235.00	2.00
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4827E+03 EXCESS= .0000E+00										OUTFLOW= .4826E+03	BASIN STORAGE= .1409E-02	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RCDON3 MANE										3.03	4426.78	236.38	1.93	5.00	4412.02	235.00	1.93
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4654E+03 EXCESS= .0000E+00										OUTFLOW= .4653E+03	BASIN STORAGE= .1506E-02	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RCDON3 MANE										3.06	4264.36	235.48	1.85	5.00	4253.14	235.00	1.85
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4481E+03 EXCESS= .0000E+00										OUTFLOW= .4481E+03	BASIN STORAGE= .1258E-02	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RCDON3 MANE										3.07	4204.50	236.34	1.83	5.00	4186.33	235.00	1.83
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4412E+03 EXCESS= .0000E+00										OUTFLOW= .4412E+03	BASIN STORAGE= .1350E-02	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RCDON3 MANE										3.08	4155.53	236.97	1.81	5.00	4135.11	235.00	1.81
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4364E+03 EXCESS= .0000E+00										OUTFLOW= .4364E+03	BASIN STORAGE= .1751E-02	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RCDON3 MANE										3.08	4118.34	237.49	1.79	5.00	4102.70	235.00	1.79
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4330E+03 EXCESS= .0000E+00										OUTFLOW= .4329E+03	BASIN STORAGE= .1394E-02	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RCDON3 MANE										3.09	4065.99	235.11	1.77	5.00	4062.61	235.00	1.77
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4274E+03 EXCESS= .0000E+00										OUTFLOW= .4274E+03	BASIN STORAGE= .1741E-02	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RCDON3 MANE										3.68	2050.84	239.21	.89	5.00	2046.31	240.00	.89
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2140E+03 EXCESS= .0000E+00										OUTFLOW= .2140E+03	BASIN STORAGE= .1324E-02	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RPIC-B MANE										1.74	439.87	237.27	2.03	5.00	439.01	235.00	2.03
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4783E+02 EXCESS= .0000E+00										OUTFLOW= .4783E+02	BASIN STORAGE= .2578E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RPIC-B MANE										1.75	432.13	236.45	1.99	5.00	430.53	235.00	1.99
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4685E+02 EXCESS= .0000E+00										OUTFLOW= .4685E+02	BASIN STORAGE= .2499E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RPIC-B MANE										1.76	417.58	236.27	1.92	5.00	416.38	235.00	1.92
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4522E+02 EXCESS= .0000E+00										OUTFLOW= .4522E+02	BASIN STORAGE= .2493E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RPIC-B MANE										1.78	403.10	236.14	1.85	5.00	402.16	235.00	1.85
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4360E+02 EXCESS= .0000E+00										OUTFLOW= .4360E+02	BASIN STORAGE= .2464E-03	PERCENT ERROR= .0					
FOR PLAN = 1 RATIO= .00																	
RPIC-B MANE										1.78	398.34	236.81	1.83	5.00	396.16	235.00	1.83

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4296E+02 EXCESS= .0000E+00 ^{PROPOSED.OUT}OUTFLOW= .4296E+02 BASIN STORAGE= .2533E-03 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RPIC-B MANE 1.78 393.51 237.29 1.81 5.00 392.22 235.00 1.81

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4251E+02 EXCESS= .0000E+00 OUTFLOW= .4250E+02 BASIN STORAGE= .2248E-03 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RPIC-B MANE 1.79 390.10 235.85 1.79 5.00 389.58 235.00 1.79

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4218E+02 EXCESS= .0000E+00 OUTFLOW= .4218E+02 BASIN STORAGE= .2523E-03 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RPIC-B MANE 1.79 386.39 236.40 1.77 5.00 385.05 235.00 1.77

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4167E+02 EXCESS= .0000E+00 OUTFLOW= .4167E+02 BASIN STORAGE= .2662E-03 PERCENT ERROR= .0
 FOR PLAN = 1 RATIO= .00
 RPIC-B MANE 2.03 203.87 238.08 .91 5.00 202.47 235.00 .91

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2143E+02 EXCESS= .0000E+00 OUTFLOW= .2143E+02 BASIN STORAGE= .2507E-03 PERCENT ERROR= .0

*** NORMAL END OF HEC-1 ***

APPENDIX B

Hydraulic Calculations and Information

TRAPEZOIDAL CHANNEL

Section A

Flow "Q" 44 cfs

Manning's "n" 0.025

Slope (%) 0.65

Bottom Width 24.0 ft

Side Slope (Lt) 9.5 H:1V

Side Slope (Rt) 5.0 H:1V

Radius 0.0 ft

OUTPUT:

Velocity 2.91 ft/sec

Depth 0.54 ft

Freeboard 0.63 ft

Total Depth 1.17 ft

Froude No. 0.75 ft

Superelevation 0.00 ft

Normal depth calculations using Manning's equation

$Fb = 1 + 0.025Vd^{1/3}$ Supercritical; $0.5 + V^2/2g$ Subcritical



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TRAPEZOIDAL CHANNEL

Section B

Flow "Q" 44 cfs

Manning's "n" 0.025

Slope (%) 1.20

Bottom Width 42.0 ft

Side Slope (Lt) 9.0 H:1V

Side Slope (Rt) 9.0 H:1V

Radius 0.0 ft

OUTPUT:

Velocity 2.97 ft/sec

Depth 0.33 ft

Freeboard 0.64 ft

Total Depth 0.97 ft

Froude No. 0.94 ft

Superelevation 0.00 ft

Normal depth calculations using Manning's equation

$Fb = 1 + 0.025Vd^{(1/3)}$ Supercritical; $0.5 + V^2/2g$ Subcritical



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TRAPEZOIDAL CHANNEL

Section C

Flow "Q" 59 cfs

Manning's "n" 0.040

Slope (%) 5.85

Bottom Width 42.0 ft

Side Slope (Lt) 3.0 H:1V

Side Slope (Rt) 2.0 H:1V

Radius 0.0 ft

OUTPUT:

Velocity 4.21 ft/sec

Depth 0.33 ft

Freeboard 1.07 ft

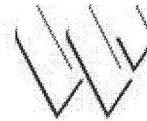
Total Depth 1.40 ft

Froude No. 1.30 ft

Superelevation 0.00 ft

Normal depth calculations using Manning's equation

$Fb = 1 + 0.025Vd^{1/3}$ Supercritical; $0.5 + V^2/2g$ Subcritical



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RIPRAP CHANNEL

Section C

Flow "Q"	59 cfs
Manning's "n"	0.034
Slope (%)	5.85
Bottom Width	42.0 ft
Side Slope (Lt)	3.0 H:1V
Side Slope (Rt)	2.0 H:1V
Specific Gravity	2.5

OUTPUT:

Velocity	4.65 ft/s
Depth	0.30 ft
Freeboard	1.08 ft
Total Depth	1.38 ft
Froude No.	1.51
Riprap Size D50	4.9 in



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TRAPEZOIDAL CHANNEL

Section D

Flow "Q" 59 cfs

Manning's "n" 0.040

Slope (%) 4.28

Bottom Width 42.0 ft

Side Slope (Lt) 3.0 H:1V

Side Slope (Rt) 3.0 H:1V

Radius 0.0 ft

OUTPUT:

Velocity 3.81 ft/sec

Depth 0.36 ft

Freeboard 1.07 ft

Total Depth 1.43 ft

Froude No. 1.13 ft

Superelevation 0.00 ft

Normal depth calculations using Manning's equation

$Fb = 1 + 0.025Vd^{(1/3)}$ Supercritical; $0.5 + V^2/2g$ Subcritical



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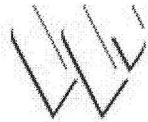
RIPRAP CHANNEL

Section D

Flow "Q"	59 cfs
Manning's "n"	0.033
Slope (%)	4.28
Bottom Width	42.0 ft
Side Slope (Lt)	3.0 H:1V
Side Slope (Rt)	3.0 H:1V
Specific Gravity	2.50

OUTPUT:

Velocity	4.29 ft/s
Depth	0.32 ft
Freeboard	1.07 ft
Total Depth	1.39 ft
Froude No.	1.35
Riprap Size D50	3.8 in



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TRAPEZOIDAL CHANNEL

Section E

Flow "Q" 60 cfs

Manning's "n" 0.025

Slope (%) 0.50

Bottom Width 10.0 ft

Side Slope (Lt) 2.0 H:1V

Side Slope (Rt) 8.0 H:1V

Radius 0.0 ft

OUTPUT:

Velocity 3.60 ft/sec

Depth 1.08 ft

Freeboard 0.70 ft

Total Depth 1.78 ft

Froude No. 0.71 ft

Superelevation 0.00 ft

Normal depth calculations using Manning's equation

$Fb = 1 + 0.025Vd^{(1/3)}$ Supercritical; $0.5 + V^2/2g$ Subcritical



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TRAPEZOIDAL CHANNEL

Section F

Flow "Q"	60 cfs
Manning's "n"	0.025
Slope (%)	0.73
Bottom Width	10.0 ft
Side Slope (Lt)	2.0 H:1V
Side Slope (Rt)	2.0 H:1V
Radius	0.0 ft

OUTPUT:

Velocity	4.64 ft/sec
Depth	1.07 ft
Freeboard	0.83 ft
Total Depth	1.90 ft
Froude No.	0.86 ft
Superelevation	0.00 ft

Normal depth calculations using Manning's equation

$Fb = 1 + 0.025Vd^{(1/3)}$ Supercritical; $0.5 + V^2/2g$ Subcritical



TRAPEZOIDAL CHANNEL

Section G

Flow "Q" 34 cfs

Manning's "n" 0.025

Slope (%) 0.61

Bottom Width 10.0 ft

Side Slope (Lt) 2.0 H:1V

Side Slope (Rt) 3.0 H:1V

Radius 0.0 ft

OUTPUT:

Velocity 3.55 ft/sec

Depth 0.80 ft

Freeboard 0.70 ft

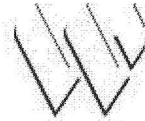
Total Depth 1.50 ft

Froude No. 0.76 ft

Superelevation 0.00 ft

Normal depth calculations using Manning's equation

$Fb = 1 + 0.025Vd^{1/3}$ Supercritical; $0.5 + V^2/2g$ Subcritical



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TRAPEZOIDAL CHANNEL

Section H (north half)

Flow "Q" 33 cfs

Manning's "n" 0.040

Slope (%) 6.15

Bottom Width 0.0 ft

Side Slope (Lt) 3.0 H:1V

Side Slope (Rt) 50.0 H:1V

Radius 0.0 ft

OUTPUT:

Velocity 3.95 ft/sec

Depth 0.56 ft

Freeboard 1.08 ft

Total Depth 1.64 ft

Froude No. 1.32 ft

Superelevation 0.00 ft

Normal depth calculations using Manning's equation

$Fb = 1 + 0.025Vd^{1/3}$ Supercritical; $0.5 + V^2/2g$ Subcritical



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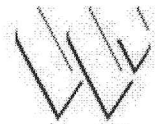
RIPRAP CHANNEL

Section H (north half)

Flow "Q"	33 cfs
Manning's "n"	0.034
Slope (%)	6.15
Bottom Width	0.0 ft
Side Slope (Lt)	3.0 H:1V
Side Slope (Rt)	50.0 H:1V
Specific Gravity	2.50

OUTPUT:

Velocity	4.46 ft/s
Depth	0.53 ft
Freeboard	1.09 ft
Total Depth	1.62 ft
Froude No.	1.53
Riprap Size D50	4.7 in



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TRAPEZOIDAL CHANNEL

Section H (south half)

Flow "Q" 33 cfs

Manning's "n" 0.040

Slope (%) 6.15

Bottom Width 0.0 ft

Side Slope (Lt) 2.0 H:1V

Side Slope (Rt) 50.0 H:1V

Radius 0.0 ft

OUTPUT:

Velocity 3.97 ft/sec

Depth 0.57 ft

Freeboard 1.08 ft

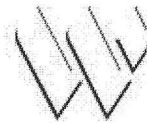
Total Depth 1.65 ft

Froude No. 1.31 ft

Superelevation 0.00 ft

Normal depth calculations using Manning's equation

$Fb = 1 + 0.025Vd^{(1/3)}$ Supercritical; $0.5 + V^2/2g$ Subcritical



G. C. WALLACE COMPANIES

ENGINEERS | PLANNERS | SURVEYORS

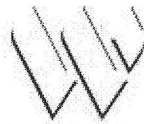
RIPRAP CHANNEL

Section H (south half)

Flow "Q"	33 cfs
Manning's "n"	0.034
Slope (%)	6.15
Bottom Width	0.0 ft
Side Slope (Lt)	2.0 H:1V
Side Slope (Rt)	50.0 H:1V
Specific Gravity	2.50

OUTPUT:

Velocity	4.48 ft/s
Depth	0.53 ft
Freeboard	1.09 ft
Total Depth	1.62 ft
Froude No.	1.53
Riprap Size D50	4.7 in



G. C. WALLACE COMPANIES
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Worksheet for Facility 25 - 54-inch RCP

Project Description

Friction Method	Manning Formula
Solve For	Full Flow Diameter

Input Data

Roughness Coefficient	0.013
Channel Slope	2.70 %
Normal Depth	3.69 ft
Diameter	3.69 ft
Discharge	191.00 ft ³ /s

Results

Diameter	3.69 ft
Normal Depth	3.69 ft
Flow Area	10.72 ft ²
Wetted Perimeter	11.61 ft
Hydraulic Radius	0.92 ft
Top Width	0.00 ft
Critical Depth	3.62 ft
Percent Full	100.0 %
Critical Slope	0.02411 ft/ft
Velocity	17.81 ft/s
Velocity Head	4.93 ft
Specific Energy	8.63 ft
Froude Number	0.00
Maximum Discharge	205.46 ft ³ /s
Discharge Full	191.00 ft ³ /s
Slope Full	0.02700 ft/ft
Flow Type	SubCritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

GVF Output Data

Upstream Depth	0.00 ft
Profile Description	
Profile Headloss	0.00 ft
Average End Depth Over Rise	0.00 %

Worksheet for Facility 25 - 54-inch RCP

GVF Output Data

Normal Depth Over Rise	100.00	%
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	3.69	ft
Critical Depth	3.62	ft
Channel Slope	2.70	%
Critical Slope	0.02411	ft/ft

Cross Section for Facility 25 - 54-inch RCP

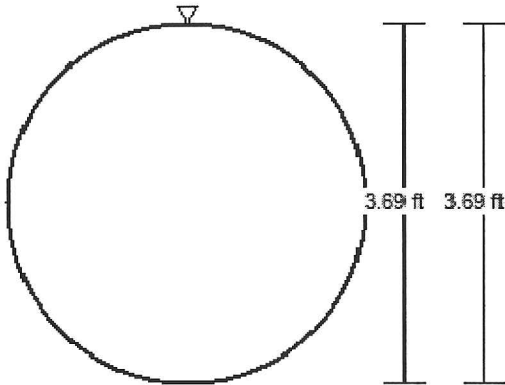
Project Description

Friction Method Manning Formula
Solve For Full Flow Diameter

Input Data

Roughness Coefficient	0.013
Channel Slope	2.70 %
Normal Depth	3.69 ft
Diameter	3.69 ft
Discharge	191.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Worksheet for Facility 26 - 54-inch RCP

Project Description

Friction Method	Manning Formula
Solve For	Full Flow Diameter

Input Data

Roughness Coefficient	0.013
Channel Slope	2.50 %
Normal Depth	3.54 ft
Diameter	3.54 ft
Discharge	164.00 ft ³ /s

Results

Diameter	3.54 ft
Normal Depth	3.54 ft
Flow Area	9.84 ft ²
Wetted Perimeter	11.12 ft
Hydraulic Radius	0.89 ft
Top Width	0.00 ft
Critical Depth	3.45 ft
Percent Full	100.0 %
Critical Slope	0.02216 ft/ft
Velocity	16.66 ft/s
Velocity Head	4.31 ft
Specific Energy	7.85 ft
Froude Number	0.00
Maximum Discharge	176.42 ft ³ /s
Discharge Full	164.00 ft ³ /s
Slope Full	0.02500 ft/ft
Flow Type	SubCritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

GVF Output Data

Upstream Depth	0.00 ft
Profile Description	
Profile Headloss	0.00 ft
Average End Depth Over Rise	0.00 %

Worksheet for Facility 26 - 54-inch RCP

GVF Output Data

Normal Depth Over Rise	100.00	%
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	3.54	ft
Critical Depth	3.45	ft
Channel Slope	2.50	%
Critical Slope	0.02216	ft/ft

Cross Section for Facility 26 - 54-inch RCP

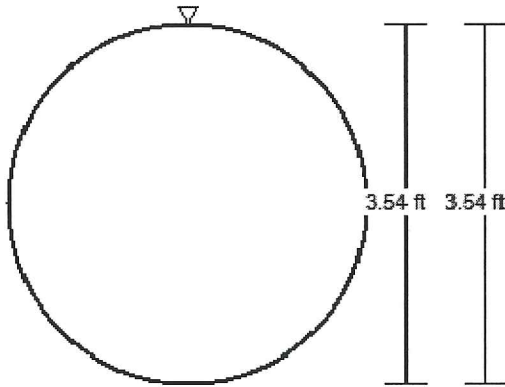
Project Description

Friction Method Manning Formula
Solve For Full Flow Diameter

Input Data

Roughness Coefficient	0.013
Channel Slope	2.50 %
Normal Depth	3.54 ft
Diameter	3.54 ft
Discharge	164.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Worksheet for Facility 27- 36-inch RCP

Project Description

Friction Method Manning Formula
Solve For Full Flow Diameter

Input Data

Roughness Coefficient	0.013
Channel Slope	4.50 %
Normal Depth	2.09 ft
Diameter	2.09 ft
Discharge	54.00 ft ³ /s

Results

Diameter	2.09 ft
Normal Depth	2.09 ft
Flow Area	3.43 ft ²
Wetted Perimeter	6.57 ft
Hydraulic Radius	0.52 ft
Top Width	0.00 ft
Critical Depth	2.07 ft
Percent Full	100.0 %
Critical Slope	0.04124 ft/ft
Velocity	15.73 ft/s
Velocity Head	3.85 ft
Specific Energy	5.94 ft
Froude Number	0.00
Maximum Discharge	58.09 ft ³ /s
Discharge Full	54.00 ft ³ /s
Slope Full	0.04500 ft/ft
Flow Type	SubCritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

GVF Output Data

Upstream Depth	0.00 ft
Profile Description	
Profile Headloss	0.00 ft
Average End Depth Over Rise	0.00 %

Worksheet for Facility 27- 36-inch RCP

GVF Output Data

Normal Depth Over Rise	100.00	%
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	2.09	ft
Critical Depth	2.07	ft
Channel Slope	4.50	%
Critical Slope	0.04124	ft/ft

Cross Section for Facility 27- 36-inch RCP

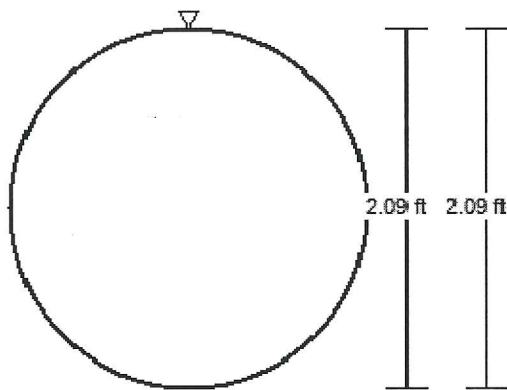
Project Description

Friction Method Manning Formula
Solve For Full Flow Diameter

Input Data

Roughness Coefficient	0.013
Channel Slope	4.50 %
Normal Depth	2.09 ft
Diameter	2.09 ft
Discharge	54.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Worksheet for Facility 28 - 11x9 RCB

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.015
Channel Slope	1.50 %
Height	9.00 ft
Bottom Width	11.00 ft
Discharge	2128.00 ft³/s

Results

Normal Depth	7.41 ft
Flow Area	81.51 ft²
Wetted Perimeter	25.82 ft
Hydraulic Radius	3.16 ft
Top Width	11.00 ft
Critical Depth	10.52 ft
Percent Full	82.3 %
Critical Slope	0.00622 ft/ft
Velocity	26.11 ft/s
Velocity Head	10.59 ft
Specific Energy	18.00 ft
Froude Number	1.69
Discharge Full	2197.70 ft³/s
Slope Full	0.01600 ft/ft
Flow Type	Supercritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

GVF Output Data

Upstream Depth	0.00 ft
Profile Description	
Profile Headloss	0.00 ft
Average End Depth Over Rise	0.00 %
Normal Depth Over Rise	82.33 %
Downstream Velocity	Infinity ft/s

Worksheet for Facility 28 - 11x9 RCB

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	7.41	ft
Critical Depth	10.52	ft
Channel Slope	1.50	%
Critical Slope	0.00622	ft/ft

Cross Section for Facility 28 - 11x9 RCB

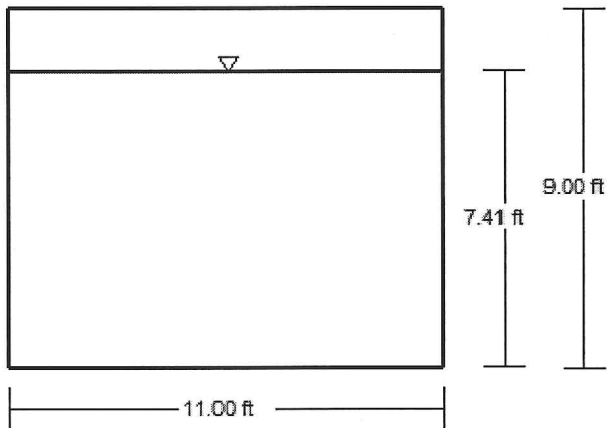
Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.015
Channel Slope	1.50 %
Normal Depth	7.41 ft
Height	9.00 ft
Bottom Width	11.00 ft
Discharge	2128.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Worksheet for Facility 29 - 66-inch RCP

Project Description

Friction Method Manning Formula
Solve For Full Flow Diameter

Input Data

Roughness Coefficient	0.013
Channel Slope	2.60 %
Normal Depth	4.64 ft
Diameter	4.64 ft
Discharge	344.00 ft³/s

Results

Diameter	4.64 ft
Normal Depth	4.64 ft
Flow Area	16.91 ft²
Wetted Perimeter	14.58 ft
Hydraulic Radius	1.16 ft
Top Width	0.00 ft
Critical Depth	4.55 ft
Percent Full	100.0 %
Critical Slope	0.02329 ft/ft
Velocity	20.35 ft/s
Velocity Head	6.43 ft
Specific Energy	11.07 ft
Froude Number	0.00
Maximum Discharge	370.05 ft³/s
Discharge Full	344.00 ft³/s
Slope Full	0.02600 ft/ft
Flow Type	SubCritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

GVF Output Data

Upstream Depth	0.00 ft
Profile Description	
Profile Headloss	0.00 ft
Average End Depth Over Rise	0.00 %

Worksheet for Facility 29 - 66-inch RCP

GVF Output Data

Normal Depth Over Rise	100.00	%
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	4.64	ft
Critical Depth	4.55	ft
Channel Slope	2.60	%
Critical Slope	0.02329	ft/ft

Cross Section for Facility 29 - 66-inch RCP

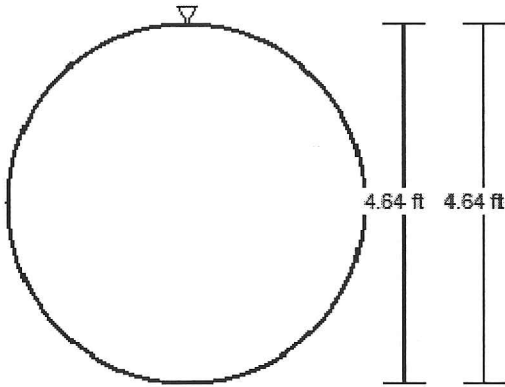
Project Description

Friction Method Manning Formula
Solve For Full Flow Diameter

Input Data

Roughness Coefficient	0.013
Channel Slope	2.60 %
Normal Depth	4.64 ft
Diameter	4.64 ft
Discharge	344.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Worksheet for Facility 30 - 48-inch RCP

Project Description

Friction Method	Manning Formula
Solve For	Full Flow Diameter

Input Data

Roughness Coefficient	0.013
Channel Slope	2.50 %
Normal Depth	3.13 ft
Diameter	3.13 ft
Discharge	118.00 ft ³ /s

Results

Diameter	3.13 ft
Normal Depth	3.13 ft
Flow Area	7.69 ft ²
Wetted Perimeter	9.83 ft
Hydraulic Radius	0.78 ft
Top Width	0.00 ft
Critical Depth	3.04 ft
Percent Full	100.0 %
Critical Slope	0.02208 ft/ft
Velocity	15.34 ft/s
Velocity Head	3.66 ft
Specific Energy	6.79 ft
Froude Number	0.00
Maximum Discharge	126.95 ft ³ /s
Discharge Full	118.02 ft ³ /s
Slope Full	0.02499 ft/ft
Flow Type	SubCritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

GVF Output Data

Upstream Depth	0.00 ft
Profile Description	
Profile Headloss	0.00 ft
Average End Depth Over Rise	0.00 %

Worksheet for Facility 30 - 48-inch RCP

GVF Output Data

Normal Depth Over Rise	100.00	%
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	3.13	ft
Critical Depth	3.04	ft
Channel Slope	2.50	%
Critical Slope	0.02208	ft/ft

Cross Section for Facility 30 - 48-inch RCP

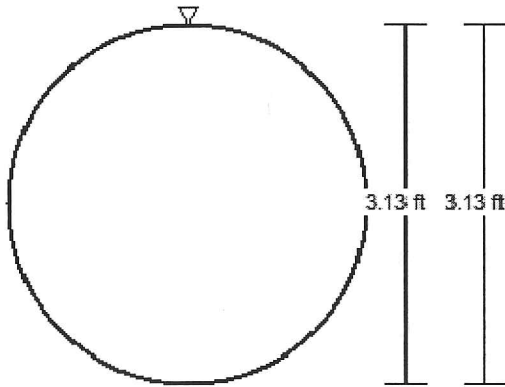
Project Description

Friction Method Manning Formula
Solve For Full Flow Diameter

Input Data

Roughness Coefficient	0.013
Channel Slope	2.50 %
Normal Depth	3.13 ft
Diameter	3.13 ft
Discharge	118.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Cross Section for Facility 30 - 48-inch RCP

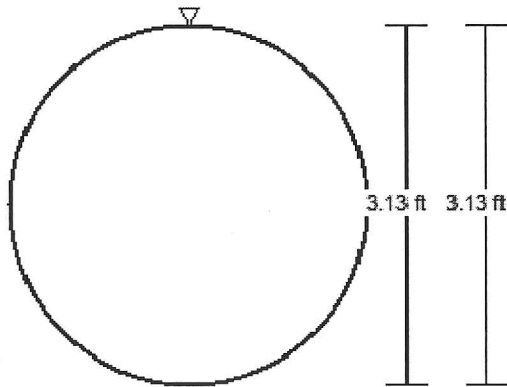
Project Description

Friction Method Manning Formula
Solve For Full Flow Diameter

Input Data

Roughness Coefficient	0.013
Channel Slope	2.50 %
Normal Depth	3.13 ft
Diameter	3.13 ft
Discharge	118.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Worksheet for Facility 31 - 11x8 RCB

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.015
Channel Slope	1.50 %
Height	8.00 ft
Bottom Width	11.00 ft
Discharge	1910.00 ft ³ /s

Results

Normal Depth	6.81 ft
Flow Area	74.96 ft ²
Wetted Perimeter	24.63 ft
Hydraulic Radius	3.04 ft
Top Width	11.00 ft
Critical Depth	9.79 ft
Percent Full	85.2 %
Critical Slope	0.00599 ft/ft
Velocity	25.48 ft/s
Velocity Head	10.09 ft
Specific Energy	16.90 ft
Froude Number	1.72
Discharge Full	1868.81 ft ³ /s
Slope Full	0.01436 ft/ft
Flow Type	Supercritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

GVF Output Data

Upstream Depth	0.00 ft
Profile Description	
Profile Headloss	0.00 ft
Average End Depth Over Rise	0.00 %
Normal Depth Over Rise	85.18 %
Downstream Velocity	Infinity ft/s

Worksheet for Facility 31 - 11x8 RCB

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	6.81	ft
Critical Depth	9.79	ft
Channel Slope	1.50	%
Critical Slope	0.00599	ft/ft

Cross Section for Facility 31 - 11x8 RCB

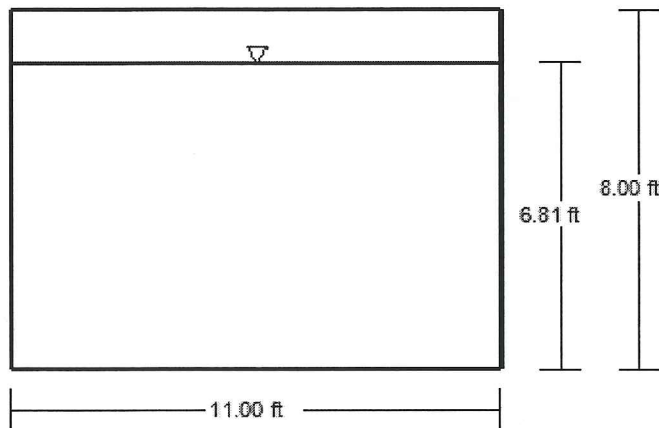
Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.015
Channel Slope	1.50 %
Normal Depth	6.81 ft
Height	8.00 ft
Bottom Width	11.00 ft
Discharge	1910.00 ft ³ /s

Cross Section Image



V: 1
H: 1

WSPGW Stations Referenced from Queens Borough Culvert Study	MAIN 1 WSPGW Stations
-3625.00	-12270.67
-3550.00	-12195.67
-3500.00	-12145.67
-3401.01	-12046.68
-3350.81	-11996.48
-3325.95	-11971.62
-3315.95	-11961.62
-3225.64	-11871.31
-3223.32	-11868.99
-3152.70	-11798.37
-3135.29	-11780.96
-3049.99	-11695.66
-2906.52	-11552.19
-2433.63	-11079.30
-2318.22	-10963.89
-2200.00	-10845.67
-1733.86	-10379.53
-1565.00	-10210.67
-1000.00	-9645.67

WSPGW ANALYSIS

MAIN 1

2619.400

T2 GCW INC. PROJECT# 840.050

T3 FILENAME: MAIN1.WSW JAM

SO -12270.6702614.000 1

2619.400

[illegible]

MAIN1.WSW														
CD	3	5	0	.000	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
CD	4	5	0	.000	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
CD	5	5	0	.000	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
CD	6	5	0	.000	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
CD	7	5	0	.000	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
PTS	114			.000	30.000	18.200	25.000	26.100	25.000	33.300	26.000	38.300	26.000	
PTS				43.800	25.000	51.800	24.000	61.800	20.000	77.300	17.000	92.800	14.000	
PTS				113.100	20.000	132.400	25.000	140.900	29.000	151.700	30.000			
PTS	211			.000	35.000	26.300	30.000	37.200	25.000	44.700	25.000	45.700	26.000	
PTS				48.500	26.000	51.670	22.000	72.200	17.000	92.000	18.000	123.100	32.800	
PTS				147.000	35.000									
PTS	3	7		.000	35.000	21.900	30.000	47.700	30.000	71.200	18.400	90.600	17.500	
PTS				111.000	19.000	146.500	37.000							
PTS	4	9		.000	35.000	10.420	30.000	19.300	25.000	24.900	22.000	38.600	20.800	
PTS				83.700	20.800	87.600	25.000	98.900	30.000	100.600	35.000			
PTS	5	8		.000	48.000	19.090	48.000	50.850	45.000	111.110	21.000	159.240	21.000	
PTS				159.240	21.000	186.970	35.980	248.780	40.000					
PTS	6	6		.000	49.000	11.030	48.000	54.930	38.000	84.460	22.000	136.390	22.000	
PTS				173.210	40.000									
Q				2130.000	.0									

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1.WSW JAM

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope				SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch	
-12270.670	2614.000	7.896	2621.896	4673.00	17.79	4.92	2626.81	.00	9.43	63.36		1		0 .0
TRANS STR	.0400				.0179	1.34	7.90	1.54		.035				IR-OPEN
-12195.670	2617.000	9.000	2626.000	4673.00	12.16	2.29	2628.29	.00	9.00	73.79		2		0 .0
TRANS STR	.0100				.0066	.33	9.00	.94		.035				IR-OPEN
-12145.670	2617.500	10.039	2627.539	4673.00	8.78	1.20	2628.74	.00	7.49	75.16		3		0 .0
TRANS STR	.0328						10.039	.582		.040				IR-OPEN
-12046.680	2620.750	2.538	2623.288	4673.00	32.08	15.98	2639.26	.00	5.81	63.65		4		0 .0
TRANS STR	.0110				.0369	1.85	2.54	3.74		.015				IR-OPEN
-11996.480	2621.300	2.585	2623.885	4673.00	33.62	17.55	2641.44	.00	6.03	59.41		5		0 .0
TRANS STR	.0141				.0409	1.02	2.59	3.87		.015				IR-OPEN
-11971.620	2621.650	2.384	2624.034	4673.00	34.65	18.64	2642.68	.00	5.85	61.21		6		0 .0
TRANS STR	.0160				.0337	.34	2.38	4.11		.015				IR-OPEN
-11961.620	2621.810	6.099	2627.909	4673.00	31.93	15.83	2643.74	.00	10.56	25.00	12.000	25.000	.00	1 1.0
90.311	.0152				.0248	2.24	6.10	2.33	7.23	.015	.00	.00		BOX
-11871.310	2623.180	5.903	2629.083	4673.00	32.99	16.89	2645.98	.00	10.56	25.00	12.000	25.000	.00	1 1.0
2.319	-.0776				.0262	.06	5.90	2.44	.00	.015	.00	.00		BOX
-11868.990	2623.000	5.853	2628.853	4673.00	33.27	17.19	2646.04	12.00	10.56	25.00	12.000	25.000	.00	1 1.0
70.620	.0283				.0263	1.86	12.00	2.47	5.71	.015	.00	.00		BOX

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1.WSW JAM

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope				SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch	
-11798.370	2625.000	5.882	2630.882	4673.00	33.10	17.02	2647.90	.00	10.56	25.00	12.000	25.000	.00	1 1.0
17.410	.0276				.0261	.45	5.88	2.46	5.77	.015	.00	.00		BOX
-11780.960	2625.480	5.887	2631.367	4673.00	33.08	16.99	2648.35	12.00	10.56	25.00	12.000	25.000	.00	1 1.0
85.300	.0279				.0259	2.21	12.00	2.45	5.74	.015	.00	.00		BOX
-11695.660	2627.860	5.923	2633.783	4673.00	32.87	16.78	2650.56	.00	10.56	25.00	12.000	25.000	.00	1 1.0
143.470	.0279				.0252	3.61	5.92	2.43	5.74	.015	.00	.00		BOX
-11552.190	2631.860	6.008	2637.868	4673.00	32.41	16.31	2654.18	.40	10.56	25.00	12.000	25.000	.00	1 1.0
204.461	.0278				.0237	4.84	6.41	2.38	5.75	.015	.00	.00		BOX
-11347.730	2637.552	6.213	2643.765	4673.00	31.34	15.25	2659.02	.38	10.56	25.00	12.000	25.000	.00	1 1.0
164.742	.0278				.0213	3.50	6.59	2.26	5.75	.015	.00	.00		BOX
-11182.990	2642.138	6.516	2648.655	4673.00	29.88	13.86	2662.52	.34	10.56	25.00	12.000	25.000	.00	1 1.0
103.688	.0278				.0188	1.94	6.86	2.11	5.75	.015	.00	.00		BOX
-11079.300	2645.025	6.834	2651.859	4673.00	28.49	12.60	2664.46	12.00	10.56	25.00	12.000	25.000	.00	1 1.0
59.925	.0278				.0167	1.00	12.00	1.96	5.75	.015	.00	.00		BOX
-11019.380	2646.693	7.102	2653.795	4673.00	27.42	11.67	2665.47	12.00	10.56	25.00	12.000	25.000	.00	1 1.0
55.485	.0278				.0150	.83	12.00	1.85	5.75	.015	.00	.00		BOX
-10963.890	2648.238	7.449	2655.687	4673.00	26.14	10.61	2666.30	.00	10.56	25.00	12.000	25.000	.00	1 1.0
26.600	.0278				.0135	.36	7.45	1.72	5.75	.015	.00	.00		BOX

MAIN1.OUT

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1.WSW JAM

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-10937.290	2648.979	7.669	2656.648	4673.00	25.39	10.01	2666.66	.00	10.56	25.00	12.000	25.000	.00	1 1.0
34.373	.0278					.0123	.42	7.67	1.65	5.75	.015	.00	.00	BOX
-10902.920	2649.936	8.044	2657.979	4673.00	24.21	9.10	2667.08	.00	10.56	25.00	12.000	25.000	.00	1 1.0
25.571	.0278					.0109	.28	8.04	1.54	5.75	.015	.00	.00	BOX
-10877.340	2650.648	8.436	2659.084	4673.00	23.08	8.27	2667.36	.00	10.56	25.00	12.000	25.000	.00	1 1.0
18.653	.0278					.0096	.18	8.44	1.43	5.75	.015	.00	.00	BOX
-10858.690	2651.167	8.848	2660.015	4673.00	22.01	7.52	2667.54	.00	10.56	25.00	12.000	25.000	.00	1 1.0
13.021	.0278					.0085	.11	8.85	1.33	5.75	.015	.00	.00	BOX
-10845.670	2651.530	9.280	2660.810	4673.00	20.98	6.84	2667.65	.00	10.56	25.00	12.000	25.000	.00	1 1.0
64.175	.0080					.0080	.51	9.28	1.24	9.28	.015	.00	.00	BOX
-10781.500	2652.043	9.280	2661.323	4673.00	20.98	6.84	2668.16	.00	10.56	25.00	12.000	25.000	.00	1 1.0
401.965	.0080					.0077	3.11	9.28	1.24	9.28	.015	.00	.00	BOX
-10379.530	2655.259	9.526	2664.785	4673.00	20.44	6.49	2671.27	12.00	10.56	25.00	12.000	25.000	.00	1 1.0
43.904	.0080					.0074	.33	12.00	1.19	9.28	.015	.00	.00	BOX
-10335.630	2655.610	9.599	2665.209	4673.00	20.28	6.39	2671.60	12.00	10.56	25.00	12.000	25.000	.00	1 1.0
105.124	.0080					.0069	.73	12.00	1.18	9.28	.015	.00	.00	BOX
-10230.500	2656.451	10.068	2666.519	4673.00	19.34	5.81	2672.33	12.00	10.56	25.00	12.000	25.000	.00	1 1.0
19.832	.0080					.0062	.12	12.00	1.10	9.28	.015	.00	.00	BOX

♀ FILE: MAIN1.WSW

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Program Package Serial Number: 7044

WATER SURFACE PROFILE LISTING

Date: 3- 3-2016 Time:10: 3:30

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1.WSW JAM

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-10210.670	2656.610	10.560	2667.170	4673.00	18.44	5.28	2672.45	.00	10.56	25.00	12.000	25.000	.00	1 1.0
77.532	.0050					.0051	.40	10.56	1.02	11.20	.015	.00	.00	BOX
-10133.140	2656.999	11.075	2668.074	4673.00	17.58	4.80	2672.87	.00	10.56	25.00	12.000	25.000	.00	1 1.0
12.322	.0050					.0051	.06	11.08	.95	11.20	.015	.00	.00	BOX
----- WARNING - Flow depth near top of box conduit -----														
-10120.820	2657.060	11.082	2668.142	4673.00	17.57	4.79	2672.94	.00	10.56	25.00	12.000	25.000	.00	1 1.0
HYDRAULIC JUMP ----- WARNING - Flow depth near top of box conduit -----														
-10120.820	2657.060	10.052	2667.113	4673.00	19.37	5.83	2672.94	.00	10.56	25.00	12.000	25.000	.00	1 1.0
41.956	.0050					.0068	.29	10.05	1.10	11.20	.015	.00	.00	BOX
-10078.860	2657.270	9.724	2666.995	4673.00	20.02	6.23	2673.22	.00	10.56	25.00	12.000	25.000	.00	1 1.0
66.513	.0050					.0076	.50	9.72	1.15	11.20	.015	.00	.00	BOX
-10012.350	2657.603	9.272	2666.875	4673.00	21.00	6.85	2673.72	.00	10.56	25.00	12.000	25.000	.00	1 1.0
71.908	.0050					.0085	.61	9.27	1.24	11.20	.015	.00	.00	BOX
-9940.438	2657.963	8.840	2666.804	4673.00	22.02	7.53	2674.34	.00	10.56	25.00	12.000	25.000	.00	1 1.0
73.994	.0050					.0096	.71	8.84	1.33	11.20	.015	.00	.00	BOX

♀ FILE: MAIN1.WSW

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Program Package Serial Number: 7044

WATER SURFACE PROFILE LISTING

Date: 3- 3-2016 Time:10: 3:30

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1.WSW JAM

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****

MAIN1.OUT

-9866.444	2658.334	8.429	2666.763	4673.00	23.10	8.29	2675.05	.00	10.56	25.00	12.000	25.000	.00	1	1.0
74.374	.0050	-	-	-	-	.0109	.81	8.43	1.43	11.20	.015	.00	.00	BOX	
-9792.070	2658.707	8.037	2666.743	4673.00	24.23	9.11	2675.86	.00	10.56	25.00	12.000	25.000	.00	1	1.0
73.785	.0050	-	-	-	-	.0123	.91	8.04	1.54	11.20	.015	.00	.00	BOX	
-9718.285	2659.076	7.663	2666.739	4673.00	25.41	10.03	2676.76	.00	10.56	25.00	12.000	25.000	.00	1	1.0
72.615	.0050	-	-	-	-	.0139	1.01	7.66	1.65	11.20	.015	.00	.00	BOX	
-9645.670	2659.440	7.306	2666.746	4673.00	26.65	11.03	2677.77	.00	10.56	25.00	12.000	25.000	.00	1	1.0
29.035	.0051	-	-	-	-	.0151	.44	7.31	1.77	11.11	.015	.00	.00	BOX	
-9616.635	2659.588	7.168	2666.756	4673.00	27.16	11.46	2678.21	.00	10.56	25.00	12.000	25.000	.00	1	1.0
70.965	.0051	-	-	-	-	.0165	1.17	7.17	1.82	11.11	.015	.00	.00	BOX	
-9545.670	2659.950	6.834	2666.784	4673.00	28.49	12.60	2679.39	.00	10.56	25.00	12.000	25.000	.00	1	1.0
145.000	.0194	-	-	-	-	.0172	2.49	6.83	1.96	6.58	.015	.00	.00	BOX	
-9400.670	2662.767	6.961	2669.728	4673.00	27.97	12.15	2681.88	.00	10.56	25.00	12.000	25.000	.00	1	1.0
JUNCT STR	.0194	-	-	-	-	.0215	.11	6.96	1.91	-	.015	.00	.00	BOX	
-9395.670	2662.864	5.401	2668.265	4177.00	32.23	16.13	2684.39	.00	9.80	25.00	12.000	25.000	.00	1	1.0
56.390	.0194	-	-	-	-	.0268	1.51	5.40	2.49	6.04	.015	.00	.00	BOX	
-9339.280	2663.960	5.319	2669.278	4177.00	32.72	16.63	2685.91	.00	9.80	25.00	12.000	25.000	.00	1	1.0
143.610	.0194	-	-	-	-	.0293	4.21	5.32	2.55	6.04	.015	.00	.00	BOX	

FILE: MAIN1.WSW W S P G W - CIVILDESIGN Version 14.08
 Program Package Serial Number: 7044
 WATER SURFACE PROFILE LISTING
 Date: 3- 3-2016 Time:10: 3:30

THE SEVENTY
 GCW INC. PROJECT# 840.050
 FILENAME: MAIN1.WSW JAM

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip	
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch	
-9195.670	2666.750	5.071	2671.821	4177.00	34.32	18.29	2690.11	.00	9.80	25.00	12.000	25.000	.00	1	1.0
WALL ENTRANCE															
-9195.670	2666.750	4.619	2671.369	4177.00	36.17	20.31	2691.68	.00	9.54	25.00	12.000	25.000	.00	0	.0
TRANS STR	.0597					.0211	.63	4.62	2.97		.015	.00	.00	BOX	
-9165.730	2668.537	9.477	2678.014	4177.00	31.48	15.39	2693.40	.00	12.00	14.00	12.000	14.000	.00	0	.0
13.507	.0597					.0152	.21	9.48	1.80	5.73	.015	.00	.00	BOX	
-9152.224	2669.344	9.762	2679.106	4177.00	30.56	14.50	2693.61	.00	12.00	14.00	12.000	14.000	.00	0	.0
18.337	.0597					.0138	.25	9.76	1.72	5.73	.015	.00	.00	BOX	
-9133.887	2670.438	10.239	2680.677	4177.00	29.14	13.19	2693.86	.00	12.00	14.00	12.000	14.000	.00	0	.0
14.717	.0597					.0122	.18	10.24	1.60	5.73	.015	.00	.00	BOX	
-9119.170	2671.317	10.738	2682.055	4177.00	27.78	11.99	2694.04	12.00	12.00	14.00	12.000	14.000	.00	0	.0
88.330	.0100					.0116	1.03	12.00	1.49	11.34	.015	.00	.00	BOX	
-9030.840	2672.200	10.624	2682.824	4177.00	28.08	12.25	2695.07	.00	12.00	14.00	12.000	14.000	.00	0	.0
48.862	.0100					.0119	.58	10.62	1.52	11.34	.015	.00	.00	BOX	
-8981.978	2672.689	10.555	2683.243	4177.00	28.27	12.41	2695.65	.00	12.00	14.00	12.000	14.000	.00	0	.0
272.338	.0100					.0128	3.47	10.55	1.53	11.34	.015	.00	.00	BOX	
-8709.640	2675.412	10.063	2685.475	4177.00	29.65	13.65	2699.12	.00	12.00	14.00	12.000	14.000	.00	0	.0
41.260	.0100					.0137	.56	10.06	1.65	11.34	.015	.00	.00	BOX	

FILE: MAIN1.WSW W S P G W - CIVILDESIGN Version 14.08
 Program Package Serial Number: 7044
 WATER SURFACE PROFILE LISTING
 Date: 3- 3-2016 Time:10: 3:30

THE SEVENTY
 GCW INC. PROJECT# 840.050
 FILENAME: MAIN1.WSW JAM

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip	
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch	
-8668.380	2675.825	9.977	2685.802	4177.00	29.91	13.89	2699.69	12.00	12.00	14.00	12.000	14.000	.00	0	.0

MAIN1.OUT

33.580	.0100					.0140	.47	12.00	1.67	11.34	.015	.00	.00	BOX
-8634.800	2676.161	9.904	2686.064	4177.00	30.13	14.09	2700.16	.00	12.00	14.00	12.000	14.000	.00	0 .0
90.340	.0100					.0145	1.31	9.90	1.69	11.34	.015	.00	.00	BOX
-8544.460	2677.064	9.694	2686.758	4177.00	30.78	14.71	2701.47	12.00	12.00	14.00	12.000	14.000	.00	0 .0
52.210	.0100					.0151	.79	12.00	1.74	11.34	.015	.00	.00	BOX
-8492.250	2677.586	9.566	2687.152	4177.00	31.19	15.10	2702.26	.00	12.00	14.00	12.000	14.000	.00	0 .0
37.142	.0100					.0156	.58	9.57	1.78	11.34	.015	.00	.00	BOX
-8455.108	2677.957	9.472	2687.429	4177.00	31.50	15.41	2702.84	.00	12.00	14.00	12.000	14.000	.00	0 .0
161.290	.0100					.0168	2.71	9.47	1.80	11.34	.015	.00	.00	BOX
-8293.818	2679.570	9.031	2688.601	4177.00	33.04	16.95	2705.55	.00	12.00	14.00	12.000	14.000	.00	0 .0
141.259	.0100					.0190	2.69	9.03	1.94	11.34	.015	.00	.00	BOX
-8152.559	2680.983	8.611	2689.594	4177.00	34.65	18.64	2708.24	.00	12.00	14.00	12.000	14.000	.00	0 .0
126.933	.0100					.0215	2.73	8.61	2.08	11.34	.015	.00	.00	BOX
-8025.626	2682.252	8.210	2690.462	4177.00	36.34	20.51	2710.97	.00	12.00	14.00	12.000	14.000	.00	0 .0
115.986	.0100					.0244	2.83	8.21	2.24	11.34	.015	.00	.00	BOX
-7909.640	2683.412	7.828	2691.240	4177.00	38.11	22.56	2713.80	.00	12.00	14.00	12.000	14.000	.00	0 .0
26.177	.0102					.0263	.69	7.83	2.40	11.25	.015	.00	.00	BOX

♀ FILE: MAIN1.WSW W S P G W - CIVILDESIGN Version 14.08
 Program Package Serial Number: 7044 WATER SURFACE PROFILE LISTING Date: 3- 3-2016 Time:10: 3:30
 THE SEVENTY GCW INC. PROJECT# 840.050
 FILENAME: MAIN1.WSW JAM

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope				SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch	
-7883.463	2683.679	7.741	2691.421	4177.00	38.54	23.06	2714.49	.00	12.00	14.00	12.000	14.000	.00	0 .0
106.553	.0102				.0285	3.03	7.74	2.44	11.25	.015	.00	.00	BOX	
-7776.910	2684.766	7.381	2692.147	4177.00	40.42	25.37	2717.52	.00	12.00	14.00	12.000	14.000	.00	0 .0
31.890	.0463				.0298	.95	7.38	2.62	6.30	.015	.00	.00	BOX	
-7745.020	2686.243	7.473	2693.716	4177.00	39.93	24.75	2718.47	1.33	12.00	14.00	12.000	14.000	.00	0 .0
51.663	.0463				.0284	1.47	8.80	2.57	6.30	.015	.00	.00	BOX	
-7693.357	2688.635	7.644	2696.279	4177.00	39.03	23.66	2719.94	1.27	12.00	14.00	12.000	14.000	.00	0 .0
87.407	.0463				.0260	2.27	8.92	2.49	6.30	.015	.00	.00	BOX	
-7605.950	2692.682	8.017	2700.698	4177.00	37.22	21.51	2722.21	.00	12.00	14.00	12.000	14.000	.00	0 .0
JUNCT STR	.0695				.0457	3.97	9.17	2.32		.015	.00	.00	BOX	
-7519.010	2698.724	2.413	2701.137	2476.00	41.04	26.15	2727.29	1.82	6.73	25.00	9.000	25.000	.00	0 .0
WALL EXIT														
-7519.010	2698.724	4.391	2703.115	2476.00	40.27	25.19	2728.30	.98	9.00	14.00	9.000	14.000	.00	0 .0
26.372	.0757				.0428	1.13	5.37	3.39	3.63	.015	.00	.00	BOX	
-7492.638	2700.720	4.476	2705.196	2476.00	39.51	24.24	2729.44	.95	9.00	14.00	9.000	14.000	.00	0 .0
54.218	.0757				.0391	2.12	5.42	3.29	3.63	.015	.00	.00	BOX	
-7438.420	2704.825	4.694	2709.519	2476.00	37.67	22.04	2731.56	.86	9.00	14.00	9.000	14.000	.00	0 .0
42.758	.0757				.0342	1.46	5.55	3.06	3.63	.015	.00	.00	BOX	

♀ FILE: MAIN1.WSW W S P G W - CIVILDESIGN Version 14.08
 Program Package Serial Number: 7044 WATER SURFACE PROFILE LISTING Date: 3- 3-2016 Time:10: 3:30
 THE SEVENTY GCW INC. PROJECT# 840.050
 FILENAME: MAIN1.WSW JAM

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope				SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch	
-7395.662	2708.062	4.924	2712.985	2476.00	35.92	20.04	2733.02	.78	9.00	14.00	9.000	14.000	.00	0 .0
34.562	.0757				.0300	1.04	5.70	2.85	3.63	.015	.00	.00	BOX	
-7361.100	2710.678	5.164	2715.842	2476.00	34.25	18.21	2734.06	.88	9.00	14.00	9.000	14.000	.00	0 .0

MAIN1.OUT

3.412	.0376							.0279	.10	6.04	2.66	4.64	.015	.00	.00	BOX
-7357.688	2710.806	5.169	2715.975	2476.00	34.21	18.18	2734.15	.87	9.00	14.00	9.000	14.000	.00	0	.0	
122.568	.0376							.0262	3.21	6.04	2.65	4.64	.015	.00	.00	BOX
-7235.120	2715.415	5.421	2720.836	2476.00	32.62	16.52	2737.36	.00	9.00	14.00	9.000	14.000	.00	0	.0	
37.062	.0376							.0238	.88	5.42	2.47	4.64	.015	.00	.00	BOX
-7198.058	2716.808	5.524	2722.333	2476.00	32.01	15.91	2738.25	.00	9.00	14.00	9.000	14.000	.00	0	.0	
74.548	.0376							.0218	1.63	5.52	2.40	4.64	.015	.00	.00	BOX
-7123.510	2719.611	5.794	2725.405	2476.00	30.52	14.47	2739.87	.00	9.00	14.00	9.000	14.000	.00	0	.0	
12.280	.0376							.0201	.25	5.79	2.23	4.64	.015	.00	.00	BOX
-7111.230	2720.073	5.849	2725.921	2476.00	30.24	14.20	2740.12	.00	9.00	14.00	9.000	14.000	.00	0	.0	
53.094	.0376							.0187	.99	5.85	2.20	4.64	.015	.00	.00	BOX
-7058.136	2722.069	6.134	2728.203	2476.00	28.83	12.91	2741.11	.00	9.00	14.00	9.000	14.000	.00	0	.0	
41.235	.0376							.0164	.68	6.13	2.05	4.64	.015	.00	.00	BOX
-7016.901	2723.619	6.434	2730.053	2476.00	27.49	11.73	2741.79	.00	9.00	14.00	9.000	14.000	.00	0	.0	
32.483	.0376							.0144	.47	6.43	1.91	4.64	.015	.00	.00	BOX

FILE: MAIN1.WSW W S P G W - CIVILDESIGN Version 14.08
 Program Package Serial Number: 7044 WATER SURFACE PROFILE LISTING
 Date: 3- 3-2016 Time:10: 3:30

THE SEVENTY
 GCW INC. PROJECT# 840.050
 FILENAME: MAIN1.WSW JAM

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope				SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch	
-6984.418	2724.841	6.748	2731.588	2476.00	26.21	10.67	2742.26	.00	9.00	14.00	9.000	14.000	.00	0
25.718	.0376					.0127	.33	6.75	1.78	4.64	.015	.00	BOX	
-6958.700	2725.808	7.077	2732.885	2476.00	24.99	9.70	2742.58	.00	9.00	14.00	9.000	14.000	.00	0
20.298	.0376					.0112	.23	7.08	1.66	4.64	.015	.00	BOX	
-6938.402	2726.571	7.422	2733.993	2476.00	23.83	8.82	2742.81	.00	9.00	14.00	9.000	14.000	.00	0
15.832	.0376					.0099	.16	7.42	1.54	4.64	.015	.00	BOX	
-6922.570	2727.166	7.785	2734.951	2476.00	22.72	8.01	2742.97	.00	9.00	14.00	9.000	14.000	.00	0
87.450	.0100					.0091	.80	7.78	1.43	7.55	.015	.00	BOX	
-6835.120	2728.041	7.860	2735.901	2476.00	22.50	7.86	2743.76	.00	9.00	14.00	9.000	14.000	.00	0
86.140	.0100					.0089	.76	7.86	1.41	7.55	.015	.00	BOX	
-6748.980	2728.902	7.961	2736.863	2476.00	22.22	7.66	2744.53	.00	9.00	14.00	9.000	14.000	.00	0
JUNCT STR	.0100					.0091	.05	7.96	1.39		.015	.00	BOX	
-6743.980	2728.952	7.647	2736.599	2450.00	22.88	8.13	2744.73	.00	9.00	14.00	9.000	14.000	.00	0
308.860	.0100					.0090	2.79	7.65	1.46	7.49	.015	.00	BOX	
-6435.121	2732.041	7.948	2739.989	2450.00	22.02	7.53	2747.52	.00	9.00	14.00	9.000	14.000	.00	0
58.804	.0100					.0084	.49	7.95	1.38	7.49	.015	.00	BOX	
-6376.317	2732.629	8.056	2740.686	2450.00	21.72	7.33	2748.01	.00	9.00	14.00	9.000	14.000	.00	0
122.954	.0100					.0078	.96	8.06	1.35	7.49	.015	.00	BOX	

FILE: MAIN1.WSW W S P G W - CIVILDESIGN Version 14.08
 Program Package Serial Number: 7044 WATER SURFACE PROFILE LISTING
 Date: 3- 3-2016 Time:10: 3:30

THE SEVENTY
 GCW INC. PROJECT# 840.050
 FILENAME: MAIN1.WSW JAM

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope				SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch	
-6253.363	2733.859	8.450	2742.308	2450.00	20.71	6.66	2748.97	.00	9.00	14.00	9.000	14.000	.00	0
61.743	.0100					.0069	.42	8.45	1.26	7.49	.015	.00	BOX	
WARNING - Flow depth near top of box conduit														
-6191.620	2734.476	8.862	2743.338	2450.00	19.75	6.06	2749.39	.00	9.00	14.00	9.000	14.000	.00	0
12.660	.0100					.0063	.08	8.86	1.17	7.51	.015	.00	BOX	

MAIN1.OUT

----- WARNING - Flow depth near top of box conduit -----

-6178.960	2734.602	9.000	2743.602	2450.00	19.44	5.87	2749.47	.00	9.00	14.00	9.000	14.000	.00	0	.0
JUNCT STR	.0098					.0064	.03	9.00	1.14		.015	.00	.00	BOX	

----- WARNING - Flow depth near top of box conduit -----

-6173.960	2734.651	11.911	2746.562	2130.00	15.78	3.87	2750.43	.00	8.56	15.00	9.000	15.000	.00	0	.0
25.340	.0099					.0064	.16	11.91	.93	6.33	.015	.00	.00	BOX	
-6148.620	2734.902	11.822	2746.724	2130.00	15.78	3.87	2750.59	.00	8.56	15.00	9.000	15.000	.00	0	.0
10.330	.0099					.0064	.07	11.82	.93	6.34	.015	.00	.00	BOX	
-6138.290	2735.004	11.786	2746.790	2130.00	15.78	3.87	2750.66	.00	8.56	15.00	9.000	15.000	.00	0	.0
80.110	.0099					.0064	.51	.00	.93	6.33	.015	.00	.00	BOX	

♀ FILE: MAIN1.WSW

W S P G W - CIVILDESIGN Version 14.08
Program Package Serial Number: 7044

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WATER SURFACE PROFILE LISTING

Date: 3- 3-2016 Time:10: 3:30

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1.WSW JAM

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-6058.180	2735.797	12.026	2747.823	2130.00	15.78	3.87	2751.69	.00	8.56	15.00	9.000	15.000	.00	0 .0
244.970	.0099					.0064	1.57	12.03	.93	6.33	.015	.00	.00	BOX
-5813.210	2738.222	11.166	2749.388	2130.00	15.78	3.87	2753.25	.00	8.56	15.00	9.000	15.000	.00	0 .0
54.020	.0099					.0064	.35	.00	.93	6.33	.015	.00	.00	BOX
-5759.190	2738.757	11.408	2750.165	2130.00	15.78	3.87	2754.03	.00	8.56	15.00	9.000	15.000	.00	0 .0
TRANS STR	.0099					.0032	.04	11.41	.93		.015	.00	.00	BOX
-5747.190	2738.876	13.460	2752.336	2130.00	11.83	2.17	2754.51	.00	7.06	20.00	9.000	20.000	.00	0 .0
49.000	.0099					.0032	.15	13.46	.70	4.89	.015	.00	.00	BOX
-5698.190	2739.361	13.129	2752.490	2130.00	11.83	2.17	2754.66	.00	7.06	20.00	9.000	20.000	.00	0 .0

♀

MAIN1_FAC3-5.WSW

T1 THE SEVENTY

T2 GCW INC. PROJECT# 840.050

T3 FILENAME: MAIN1_FAC3-5.WSW RRD

SO	-6176.4602735.940	72		2746.562			
R	-6125.5202738.258	72	.013		35.000	.000	1
R	-5952.9902747.740	72	.013		23.000	.000	1
R	-5743.8102759.237	72	.013		13.000	.000	1
R	-5587.2202760.774	72	.013		.000	.000	1
JX	-5582.2202760.823	72 48		20.000	2760.800	50.0	0.000
R	-5379.4202762.815	72	.013		-58.000	.000	1
R	-5286.5602763.873	72	.013		.000	.000	0
SH	-5286.5602763.873	72		2773.753			
CD	18	4		1.500			
CD	24	4		2.000			
CD	30	4		2.500			
CD	36	4		3.000			
CD	42	4		3.500			
CD	48	4		4.000			
CD	54	4		4.500			
CD	60	4		5.000			
CD	72	4		6.000			
Q				344.000	.0		

THE SEVENTY
GCW INC. PROJECT# 840.050

FILENAME: MAIN1_FAC3-5.WSW RRD

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-6176.460	2735.940	10.622	2746.562	364.00	12.87	2.57	2749.14	.00	5.15	.00	6.000	.000	.00	0 .0
4.306	.0455					.0074	.03	.00	.00	2.65	.013	.00	.00	PIPE
-6172.154	2736.136	10.495	2746.631	364.00	12.87	2.57	2749.20	.00	5.15	.00	6.000	.000	.00	0 .0
HYDRAULIC JUMP														
-6172.154	2736.136	2.635	2738.771	364.00	30.45	14.40	2753.17	2.06	5.15	5.96	6.000	.000	.00	0 .0
46.634	.0455					.0465	2.17	4.69	3.79	2.65	.013	.00	.00	PIPE
-6125.520	2738.258	2.631	2740.890	364.00	30.51	14.45	2755.34	.40	5.15	5.95	6.000	.000	.00	0 .0
104.458	.0550					.0440	4.59	3.03	3.80	2.51	.013	.00	.00	PIPE
-6021.062	2743.999	2.723	2746.722	364.00	29.17	13.21	2759.93	.37	5.15	5.97	6.000	.000	.00	0 .0
68.071	.0550					.0388	2.64	3.09	3.56	2.51	.013	.00	.00	PIPE
-5952.991	2747.740	2.825	2750.565	364.00	27.81	12.01	2762.57	.16	5.15	5.99	6.000	.000	.00	0 .0
28.109	.0550					.0351	.99	2.98	3.32	2.51	.013	.00	.00	PIPE
-5924.882	2749.285	2.883	2752.168	364.00	27.08	11.39	2763.56	.15	5.15	6.00	6.000	.000	.00	0 .0
39.964	.0550					.0318	1.27	3.03	3.19	2.51	.013	.00	.00	PIPE
-5884.918	2751.481	2.993	2754.475	364.00	25.82	10.36	2764.83	.13	5.15	6.00	6.000	.000	.00	0 .0
30.694	.0550					.0280	.86	3.13	2.97	2.51	.013	.00	.00	PIPE
-5854.224	2753.168	3.107	2756.276	364.00	24.62	9.41	2765.69	.12	5.15	6.00	6.000	.000	.00	0 .0
24.267	.0550					.0247	.60	3.23	2.76	2.51	.013	.00	.00	PIPE

THE SEVENTY
GCW INC. PROJECT# 840.050

FILENAME: MAIN1_FAC3-5.WSW RRD

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-5829.957	2754.502	3.228	2757.730	364.00	23.48	8.56	2766.29	.11	5.15	5.98	6.000	.000	.00	0 .0
19.644	.0550					.0218	.43	3.34	2.57	2.51	.013	.00	.00	PIPE
-5810.313	2755.582	3.354	2758.936	364.00	22.38	7.78	2766.72	.10	5.15	5.96	6.000	.000	.00	0 .0
16.041	.0550					.0192	.31	3.45	2.39	2.51	.013	.00	.00	PIPE
-5794.272	2756.463	3.488	2759.951	364.00	21.34	7.07	2767.02	.09	5.15	5.92	6.000	.000	.00	0 .0
13.222	.0550					.0170	.22	3.58	2.22	2.51	.013	.00	.00	PIPE
-5781.050	2757.190	3.629	2760.819	364.00	20.35	6.43	2767.25	.08	5.15	5.87	6.000	.000	.00	0 .0
10.886	.0550					.0150	.16	3.71	2.05	2.51	.013	.00	.00	PIPE
-5770.164	2757.789	3.779	2761.568	364.00	19.40	5.85	2767.41	.07	5.15	5.79	6.000	.000	.00	0 .0
8.948	.0550					.0133	.12	3.85	1.90	2.51	.013	.00	.00	PIPE
-5761.216	2758.280	3.938	2762.218	364.00	18.50	5.31	2767.53	.07	5.15	5.70	6.000	.000	.00	0 .0
7.240	.0550					.0119	.09	4.00	1.75	2.51	.013	.00	.00	PIPE
-5753.976	2758.678	4.109	2762.787	364.00	17.64	4.83	2767.62	.06	5.15	5.57	6.000	.000	.00	0 .0
5.770	.0550					.0106	.06	4.17	1.62	2.51	.013	.00	.00	PIPE
-5748.207	2758.995	4.292	2763.287	364.00	16.82	4.39	2767.68	.05	5.15	5.41	6.000	.000	.00	0 .0
4.396	.0550					.0094	.04	4.34	1.48	2.51	.013	.00	.00	PIPE
-5743.810	2759.237	4.491	2763.729	364.00	16.03	3.99	2767.72	.00	5.15	5.21	6.000	.000	.00	0 .0
88.742	.0098					.0086	.76	4.49	1.35	4.32	.013	.00	.00	PIPE

MAIN1_FAC3-5.OUT

THE SEVENTY

GCW INC. PROJECT# 840.050

FILENAME: MAIN1_FAC3-5.WSW RRD

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-5655.068	2760.108	4.642	2764.750	364.00	15.51	3.73	2768.48	.00	5.15	5.02	6.000	.000	.00	0 .0
53.658	.0098					.0079	.42	4.64	1.26	4.32	.013	.00	.00	PIPE
-5601.410	2760.635	4.878	2765.513	364.00	14.78	3.39	2768.91	.00	5.15	4.68	6.000	.000	.00	0 .0
14.190	.0098					.0072	.10	4.88	1.14	4.32	.013	.00	.00	PIPE
-5587.220	2760.774	5.150	2765.924	364.00	14.09	3.08	2769.01	.00	5.15	4.18	6.000	.000	.00	0 .0
JUNCT STR	.0098					.0078	.04	5.28	1.00		.014	.00	.00	PIPE
-5582.220	2760.823	6.201	2767.024	344.00	12.17	2.30	2769.32	.00	5.03	.00	6.000	.000	.00	0 .0
202.800	.0098					.0066	1.34	.00	.00	4.13	.013	.00	.00	PIPE
-5379.420	2762.815	6.031	2768.846	344.00	12.17	2.30	2771.15	.00	5.03	.00	6.000	.000	.00	0 .0
6.556	.0114					.0066	.04	6.03	.00	3.92	.013	.00	.00	PIPE
-5372.864	2762.890	6.000	2768.890	344.00	12.17	2.30	2771.19	.00	5.03	.00	6.000	.000	.00	0 .0
53.905	.0114					.0061	.33	6.00	.00	3.92	.013	.00	.00	PIPE
-5318.959	2763.504	5.555	2769.059	344.00	12.59	2.46	2771.52	.00	5.03	3.14	6.000	.000	.00	0 .0
HYDRAULIC JUMP														
-5318.959	2763.504	4.533	2768.037	344.00	15.01	3.50	2771.54	.00	5.03	5.16	6.000	.000	.00	0 .0
3.125	.0114					.0078	.02	4.53	1.25	3.92	.013	.00	.00	PIPE
-5315.834	2763.540	4.551	2768.091	344.00	14.95	3.47	2771.56	.00	5.03	5.14	6.000	.000	.00	0 .0
22.388	.0114					.0074	.16	4.55	1.24	3.92	.013	.00	.00	PIPE

♀ FILE: MAIN1_FAC3-5.WSW

W S P G W - CIVILDESIGN Version 14.08

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Program Package Serial Number: 7044

WATER SURFACE PROFILE LISTING

Date: 3- 3-2016 Time:10: 8: 0

THE SEVENTY

GCW INC. PROJECT# 840.050

FILENAME: MAIN1_FAC3-5.WSW RRD

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-5293.446	2763.795	4.776	2768.571	344.00	14.25	3.15	2771.73	.00	5.03	4.84	6.000	.000	.00	0 .0
6.886	.0114					.0067	.05	4.78	1.12	3.92	.013	.00	.00	PIPE
-5286.560	2763.873	5.031	2768.904	344.00	13.59	2.87	2771.77	.00	5.03	4.42	6.000	.000	.00	0 .0

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MAIN1_FAC4.WSW

T1 THE SEVENTY					
T2	GCW INC. PROJECT# 840.050				
T3	FILENAME: MAIN1_FAC4.WSW RRD				
SO	-5582.3902760.799 48		2767.024		
R	-5294.8702762.238 48	.013		-58.000	.000 1
R	-5198.7702762.718 48	.013		.000	.000 0
SH	-5198.7702762.718 48		2764.678		
CD	18 4	1.500			
CD	24 4	2.000			
CD	30 4	2.500			
CD	36 4	3.000			
CD	42 4	3.500			
CD	48 4	4.000			
CD	54 4	4.500			
CD	60 4	5.000			
CD	72 4	6.000			
Q	23.000	.0			

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC4.WSW RRD

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-5582.390	2760.799	6.225	2767.024	23.00	1.83	.05	2767.08	.00	1.41	.00	4.000	.000	.00	0 .0
287.520	.0050					.0003	.07	.00	.00	1.29	.013	.00	.00	PIPE
-5294.870	2762.238	4.871	2767.109	23.00	1.83	.05	2767.16	.00	1.41	.00	4.000	.000	.00	0 .0
96.100	.0050					.0003	.02	4.87	.00	1.29	.013	.00	.00	PIPE
-5198.770	2762.718	4.415	2767.133	23.00	1.83	.05	2767.19	.00	1.41	.00	4.000	.000	.00	0 .0

MAIN1_FAC6.WSW

T1 THE SEVENTY

T2 GCW INC. PROJECT# 840.050

T3 FILENAME: MAIN1_FAC6.WSW RRD

SO	-6176.4602735.570	72		2746.562			
R	-6144.3102736.331	72	.013		60.000	.000	1
R	-5744.3102751.051	72	.013		-70.000	.000	1
R	-5616.7902752.326	72	.013		.000	.000	0
SH	-5616.7902752.326	72		2758.140			
CD	18	4					
			1.500				
CD	24	4					
			2.000				
CD	30	4					
			2.500				
CD	36	4					
			3.000				
CD	42	4					
			3.500				
CD	48	4					
			4.000				
CD	54	4					
			4.500				
CD	60	4					
			5.000				
CD	72	4					
			6.000				
Q							
	191.000	.0					

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC6.WSW RRD

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-6176.460	2735.570	10.992	2746.562	191.00	6.76	.71	2747.27	.00	3.77	.00	6.000	.000	.00	0 .0
32.150	.0237					.0020	.07	.00	.00	2.23	.013	.00	.00	PIPE
-6144.310	2736.331	10.447	2746.779	191.00	6.76	.71	2747.49	.00	3.77	.00	6.000	.000	.00	0 .0
115.765	.0368					.0020	.24	.00	.00	1.98	.013	.00	.00	PIPE
-6028.545	2740.591	6.494	2747.085	191.00	6.76	.71	2747.79	.00	3.77	.00	6.000	.000	.00	0 .0
HYDRAULIC JUMP														
-6028.545	2740.591	2.060	2742.651	191.00	22.24	7.68	2750.33	.27	3.77	5.70	6.000	.000	.00	0 .0
62.479	.0368					.0305	1.90	2.33	3.19	1.98	.013	.00	.00	PIPE
-5966.065	2742.890	2.102	2744.992	191.00	21.62	7.26	2752.25	.25	3.77	5.72	6.000	.000	.00	0 .0
62.731	.0368					.0275	1.72	2.36	3.07	1.98	.013	.00	.00	PIPE
-5903.334	2745.199	2.177	2747.376	191.00	20.62	6.60	2753.98	.23	3.77	5.77	6.000	.000	.00	0 .0
41.063	.0368					.0241	.99	2.41	2.87	1.98	.013	.00	.00	PIPE
-5862.271	2746.710	2.255	2748.965	191.00	19.66	6.00	2754.96	.21	3.77	5.81	6.000	.000	.00	0 .0
29.630	.0368					.0211	.63	2.47	2.68	1.98	.013	.00	.00	PIPE
-5832.641	2747.800	2.336	2750.136	191.00	18.74	5.45	2755.59	.19	3.77	5.85	6.000	.000	.00	0 .0
22.494	.0368					.0185	.42	2.53	2.50	1.98	.013	.00	.00	PIPE
-5810.147	2748.628	2.421	2751.049	191.00	17.87	4.96	2756.01	.18	3.77	5.89	6.000	.000	.00	0 .0
17.623	.0368					.0163	.29	2.60	2.34	1.98	.013	.00	.00	PIPE

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC6.WSW RRD

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-5792.524	2749.277	2.510	2751.787	191.00	17.04	4.51	2756.29	.16	3.77	5.92	6.000	.000	.00	0 .0
14.117	.0368					.0143	.20	2.67	2.18	1.98	.013	.00	.00	PIPE
-5778.407	2749.796	2.602	2752.398	191.00	16.24	4.10	2756.50	.15	3.77	5.95	6.000	.000	.00	0 .0
11.405	.0368					.0126	.14	2.75	2.04	1.98	.013	.00	.00	PIPE
-5767.002	2750.216	2.698	2752.914	191.00	15.49	3.73	2756.64	.14	3.77	5.97	6.000	.000	.00	0 .0
9.224	.0368					.0110	.10	2.83	1.90	1.98	.013	.00	.00	PIPE
-5757.779	2750.555	2.799	2753.354	191.00	14.77	3.39	2756.74	.12	3.77	5.99	6.000	.000	.00	0 .0
7.487	.0368					.0097	.07	2.92	1.77	1.98	.013	.00	.00	PIPE
-5750.292	2750.831	2.904	2753.735	191.00	14.08	3.08	2756.81	.11	3.77	6.00	6.000	.000	.00	0 .0
5.981	.0368					.0085	.05	3.02	1.65	1.98	.013	.00	.00	PIPE
-5744.311	2751.051	3.015	2754.066	191.00	13.43	2.80	2756.86	.00	3.77	6.00	6.000	.000	.00	0 .0
45.678	.0100					.0076	.35	3.01	1.54	2.83	.013	.00	.00	PIPE
-5698.632	2751.508	3.102	2754.610	191.00	12.95	2.60	2757.21	.00	3.77	6.00	6.000	.000	.00	0 .0
36.952	.0100					.0068	.25	3.10	1.46	2.83	.013	.00	.00	PIPE
-5661.681	2751.877	3.222	2755.099	191.00	12.35	2.37	2757.47	.00	3.77	5.98	6.000	.000	.00	0 .0
22.494	.0100					.0060	.14	3.22	1.35	2.83	.013	.00	.00	PIPE
-5639.187	2752.102	3.348	2755.450	191.00	11.77	2.15	2757.60	.00	3.77	5.96	6.000	.000	.00	0 .0
13.408	.0100					.0053	.07	3.35	1.26	2.83	.013	.00	.00	PIPE

THE SEVENTY

GCW INC. PROJECT# 840.050

FILENAME: MAIN1_FAC6.WSW RRD

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*****
Station  Invert  Depth  Water  Q      Vel  Vel  Energy  Super  Critical  Flow Top  Height/  Base Wt  ZL  No Wth
          Elev   (FT)   Elev   (CFS) (FPS) Head Grd.El. Elev  Depth  Width  Dia.-Ft or I.D.  ZL  Prs/Pip
L/Elem  Ch Slope *****
*****
-5625.779 2752.236 3.481 2755.717 191.00 11.22 1.96 2757.67 .00 3.77 5.92 6.000 .000 .00 0 .0
        6.968 .0100
-5618.811 2752.306 3.622 2755.928 191.00 10.70 1.78 2757.71 .00 3.77 5.87 6.000 .000 .00 0 .0
        2.021 .0100
-5616.790 2752.326 3.773 2756.099 191.00 10.20 1.62 2757.71 .00 3.77 5.80 6.000 .000 .00 0 .0
        -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|-
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MAIN1_FAC8A.WSW

T1 THE SEVENTY

T2 GCW INC. PROJECT# 840.050

T3 FILENAME: MAIN1_FAC8A.WSW SHT

SO 6760.4802731.530 48

2736.863

R 6836.4802742.000 48 .013

0.000 .000 0

SH 6836.4802742.000 48

.000

CD 18 4 1.500

CD 24 4 2.000

CD 30 4 2.500

CD 36 4 3.000

CD 42 4 3.500

CD 48 4 4.000

CD 54 4 4.500

CD 60 4 5.000

CD 72 4 6.000

Q 34.000 .0

Date: 3- 3-2016 Time:10: 8:56

THE SEVENTY
GCW INC. PROJECT# 840.050

FILENAME: MAIN1_FAC8A.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
6760.480	2731.530	5.333	2736.863	34.00	2.71	.11	2736.98	.00	1.73	.00	4.000	.000	.00	0 .0
9.716	.1378					.0006	.01	5.33	.00	.68	.013	.00	.00	PIPE
6770.196	2732.868	4.000	2736.868	34.00	2.71	.11	2736.98	.00	1.73	.00	4.000	.000	.00	0 .0
2.612	.1378					.0005	.00	4.00	.00	.68	.013	.00	.00	PIPE
6772.808	2733.228	3.629	2736.857	34.00	2.84	.13	2736.98	.00	1.73	2.32	4.000	.000	.00	0 .0
.630	.1378					.0005	.00	3.63	.22	.68	.013	.00	.00	PIPE
6773.438	2733.315	3.539	2736.854	34.00	2.89	.13	2736.98	.00	1.73	2.56	4.000	.000	.00	0 .0
HYDRAULIC JUMP														
6773.438	2733.315	.747	2734.063	34.00	20.95	6.82	2740.88	.00	1.73	3.12	4.000	.000	.00	0 .0
6.132	.1378					.0931	.57	.75	5.12	.68	.013	.00	.00	PIPE
6779.571	2734.160	.759	2734.919	34.00	20.46	6.50	2741.42	.00	1.73	3.14	4.000	.000	.00	0 .0
10.557	.1378					.0843	.89	.76	4.95	.68	.013	.00	.00	PIPE
6790.128	2735.614	.785	2736.399	34.00	19.50	5.91	2742.31	.00	1.73	3.18	4.000	.000	.00	0 .0
7.956	.1378					.0737	.59	.79	4.64	.68	.013	.00	.00	PIPE
6798.083	2736.710	.812	2737.522	34.00	18.60	5.37	2742.89	.00	1.73	3.22	4.000	.000	.00	0 .0
6.283	.1378					.0644	.40	.81	4.35	.68	.013	.00	.00	PIPE
6804.367	2737.575	.839	2738.415	34.00	17.73	4.88	2743.30	.00	1.73	3.26	4.000	.000	.00	0 .0
5.088	.1378					.0562	.29	.84	4.07	.68	.013	.00	.00	PIPE

Date: 3- 3-2016 Time:10: 8:56

THE SEVENTY
GCW INC. PROJECT# 840.050

FILENAME: MAIN1_FAC8A.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
6809.455	2738.276	.868	2739.145	34.00	16.91	4.44	2743.58	.00	1.73	3.30	4.000	.000	.00	0 .0
4.226	.1378					.0492	.21	.87	3.81	.68	.013	.00	.00	PIPE
6813.681	2738.859	.897	2739.756	34.00	16.12	4.03	2743.79	.00	1.73	3.34	4.000	.000	.00	0 .0
3.542	.1378					.0430	.15	.90	3.57	.68	.013	.00	.00	PIPE
6817.223	2739.347	.928	2740.275	34.00	15.37	3.67	2743.94	.00	1.73	3.38	4.000	.000	.00	0 .0
3.009	.1378					.0376	.11	.93	3.35	.68	.013	.00	.00	PIPE
6820.232	2739.761	.960	2740.721	34.00	14.65	3.33	2744.06	.00	1.73	3.42	4.000	.000	.00	0 .0
2.575	.1378					.0329	.08	.96	3.13	.68	.013	.00	.00	PIPE
6822.807	2740.116	.993	2741.109	34.00	13.97	3.03	2744.14	.00	1.73	3.46	4.000	.000	.00	0 .0
2.216	.1378					.0287	.06	.99	2.93	.68	.013	.00	.00	PIPE
6825.023	2740.421	1.027	2741.448	34.00	13.32	2.76	2744.20	.00	1.73	3.49	4.000	.000	.00	0 .0
1.914	.1378					.0251	.05	1.03	2.75	.68	.013	.00	.00	PIPE
6826.937	2740.685	1.062	2741.747	34.00	12.70	2.51	2744.25	.00	1.73	3.53	4.000	.000	.00	0 .0
1.647	.1378					.0220	.04	1.06	2.57	.68	.013	.00	.00	PIPE
6828.584	2740.912	1.099	2742.011	34.00	12.11	2.28	2744.29	.00	1.73	3.57	4.000	.000	.00	0 .0
1.426	.1378					.0192	.03	1.10	2.41	.68	.013	.00	.00	PIPE
6830.010	2741.108	1.137	2742.246	34.00	11.55	2.07	2744.32	.00	1.73	3.61	4.000	.000	.00	0 .0
1.226	.1378					.0168	.02	1.14	2.25	.68	.013	.00	.00	PIPE

Date: 3- 3-2016 Time:10: 8:56

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC8A.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
6831.236	2741.277	1.177	2742.454	34.00	11.01	1.88	2744.34	.00	1.73	3.65	4.000	.000	.00	0 .0
1.058	.1378					.0147	.02	1.18	2.11	.68	.013	.00	.00	PIPE
6832.293	2741.423	1.218	2742.641	34.00	10.50	1.71	2744.35	.00	1.73	3.68	4.000	.000	.00	0 .0
.901	.1378					.0129	.01	1.22	1.97	.68	.013	.00	.00	PIPE
6833.195	2741.547	1.261	2742.808	34.00	10.01	1.56	2744.36	.00	1.73	3.72	4.000	.000	.00	0 .0
.770	.1378					.0113	.01	1.26	1.84	.68	.013	.00	.00	PIPE
6833.965	2741.654	1.305	2742.959	34.00	9.54	1.41	2744.37	.00	1.73	3.75	4.000	.000	.00	0 .0
.646	.1378					.0099	.01	1.31	1.73	.68	.013	.00	.00	PIPE
6834.610	2741.742	1.351	2743.094	34.00	9.10	1.29	2744.38	.00	1.73	3.78	4.000	.000	.00	0 .0
.534	.1378					.0087	.00	1.35	1.61	.68	.013	.00	.00	PIPE
6835.144	2741.816	1.399	2743.215	34.00	8.68	1.17	2744.38	.00	1.73	3.82	4.000	.000	.00	0 .0
.432	.1378					.0076	.00	1.40	1.51	.68	.013	.00	.00	PIPE
6835.576	2741.875	1.449	2743.325	34.00	8.27	1.06	2744.39	.00	1.73	3.85	4.000	.000	.00	0 .0
.340	.1378					.0067	.00	1.45	1.41	.68	.013	.00	.00	PIPE
6835.916	2741.922	1.501	2743.424	34.00	7.89	.97	2744.39	.00	1.73	3.87	4.000	.000	.00	0 .0
.256	.1378					.0058	.00	1.50	1.32	.68	.013	.00	.00	PIPE
6836.172	2741.958	1.555	2743.513	34.00	7.52	.88	2744.39	.00	1.73	3.90	4.000	.000	.00	0 .0
.172	.1378					.0051	.00	1.56	1.23	.68	.013	.00	.00	PIPE

FILE: MAIN1_FAC8A.WSW

W S P G W - CIVILDESIGN Version 14.08

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Program Package Serial Number: 7044

WATER SURFACE PROFILE LISTING

Date: 3- 3-2016 Time:10: 8:56

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC8A.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
6836.344	2741.981	1.612	2743.594	34.00	7.17	.80	2744.39	.00	1.73	3.92	4.000	.000	.00	0 .0
.102	.1378					.0045	.00	1.61	1.15	.68	.013	.00	.00	PIPE
6836.446	2741.995	1.671	2743.667	34.00	6.84	.73	2744.39	.00	1.73	3.95	4.000	.000	.00	0 .0
.034	.1378					.0040	.00	1.67	1.07	.68	.013	.00	.00	PIPE
6836.480	2742.000	1.734	2743.733	34.00	6.51	.66	2744.39	.00	1.73	3.96	4.000	.000	.00	0 .0

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MAIN1_FAC8B.WSW

T1	THE SEVENTY				
T2	GCW INC. PROJECT# 840.050				
T3	FILENAME: MAIN1_FAC8B.WSW SHT				
SO	-6732.4802731.530	48	2736.863		
R	-6656.4802742.000	48	.013	0.000	.000 1
SH	-6656.4802742.000	48	.000		
CD	18	4	1.500		
CD	24	4	2.000		
CD	30	4	2.500		
CD	36	4	3.000		
CD	42	4	3.500		
CD	48	4	4.000		
CD	54	4	4.500		
CD	60	4	5.000		
CD	72	4	6.000		
Q	60.000	.0			

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC8B.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-6732.480	2731.530	5.333	2736.863	60.00	4.77	.35	2737.22	.00	2.33	.00	4.000	.000	.00	0 .0
3.274	.1378					.0017	.01	5.33	.00	.91	.013	.00	.00	PIPE
-6729.206	2731.981	4.888	2736.869	60.00	4.77	.35	2737.22	.00	2.33	.00	4.000	.000	.00	0 .0
HYDRAULIC JUMP														
-6729.206	2731.981	1.021	2733.003	60.00	23.70	8.72	2741.73	.00	2.33	3.49	4.000	.000	.00	0 .0
.925	.1378					.0850	.08	1.02	4.90	.91	.013	.00	.00	PIPE
-6728.280	2732.109	1.024	2733.133	60.00	23.60	8.65	2741.78	.00	2.33	3.49	4.000	.000	.00	0 .0
12.813	.1378					.0791	1.01	1.02	4.87	.91	.013	.00	.00	PIPE
-6715.467	2733.874	1.059	2734.933	60.00	22.50	7.86	2742.80	.00	2.33	3.53	4.000	.000	.00	0 .0
9.890	.1378					.0692	.68	1.06	4.56	.91	.013	.00	.00	PIPE
-6705.577	2735.236	1.096	2736.333	60.00	21.46	7.15	2743.48	.00	2.33	3.57	4.000	.000	.00	0 .0
7.927	.1378					.0606	.48	1.10	4.27	.91	.013	.00	.00	PIPE
-6697.650	2736.328	1.134	2737.462	60.00	20.46	6.50	2743.96	.00	2.33	3.61	4.000	.000	.00	0 .0
6.500	.1378					.0530	.34	1.13	4.00	.91	.013	.00	.00	PIPE
-6691.151	2737.224	1.174	2738.398	60.00	19.50	5.91	2744.31	.00	2.33	3.64	4.000	.000	.00	0 .0
5.431	.1378					.0464	.25	1.17	3.74	.91	.013	.00	.00	PIPE
-6685.720	2737.972	1.215	2739.187	60.00	18.60	5.37	2744.56	.00	2.33	3.68	4.000	.000	.00	0 .0
4.594	.1378					.0406	.19	1.22	3.50	.91	.013	.00	.00	PIPE

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC8B.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-6681.126	2738.604	1.257	2739.862	60.00	17.73	4.88	2744.74	.00	2.33	3.71	4.000	.000	.00	0 .0
3.913	.1378					.0356	.14	1.26	3.27	.91	.013	.00	.00	PIPE
-6677.213	2739.144	1.301	2740.445	60.00	16.91	4.44	2744.88	.00	2.33	3.75	4.000	.000	.00	0 .0
3.344	.1378					.0312	.10	1.30	3.06	.91	.013	.00	.00	PIPE
-6673.869	2739.604	1.348	2740.952	60.00	16.12	4.03	2744.99	.00	2.33	3.78	4.000	.000	.00	0 .0
2.896	.1378					.0273	.08	1.35	2.86	.91	.013	.00	.00	PIPE
-6670.973	2740.003	1.395	2741.398	60.00	15.37	3.67	2745.07	.00	2.33	3.81	4.000	.000	.00	0 .0
2.490	.1378					.0239	.06	1.40	2.68	.91	.013	.00	.00	PIPE
-6668.483	2740.346	1.445	2741.791	60.00	14.65	3.33	2745.13	.00	2.33	3.84	4.000	.000	.00	0 .0
2.151	.1378					.0210	.05	1.45	2.50	.91	.013	.00	.00	PIPE
-6666.332	2740.643	1.497	2742.140	60.00	13.97	3.03	2745.17	.00	2.33	3.87	4.000	.000	.00	0 .0
1.856	.1378					.0184	.03	1.50	2.34	.91	.013	.00	.00	PIPE
-6664.476	2740.898	1.551	2742.449	60.00	13.32	2.76	2745.21	.00	2.33	3.90	4.000	.000	.00	0 .0
1.600	.1378					.0162	.03	1.55	2.18	.91	.013	.00	.00	PIPE
-6662.876	2741.119	1.607	2742.726	60.00	12.70	2.51	2745.23	.00	2.33	3.92	4.000	.000	.00	0 .0
1.366	.1378					.0142	.02	1.61	2.04	.91	.013	.00	.00	PIPE
-6661.510	2741.307	1.666	2742.973	60.00	12.11	2.28	2745.25	.00	2.33	3.94	4.000	.000	.00	0 .0
1.166	.1378					.0124	.01	1.67	1.90	.91	.013	.00	.00	PIPE

THE SEVENTY

GCW INC. PROJECT# 840.050

FILENAME: MAIN1_FAC8B.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-6660.345	2741.468	1.727	2743.195	60.00	11.55	2.07	2745.27	.00	2.33	3.96	4.000	.000	.00	0 .0
.979	.1378					.0109	.01	1.73	1.78	.91	.013	.00	.00	PIPE
-6659.365	2741.603	1.791	2743.394	60.00	11.01	1.88	2745.28	.00	2.33	3.98	4.000	.000	.00	0 .0
.820	.1378					.0096	.01	1.79	1.66	.91	.013	.00	.00	PIPE
-6658.545	2741.716	1.857	2743.573	60.00	10.50	1.71	2745.28	.00	2.33	3.99	4.000	.000	.00	0 .0
.662	.1378					.0085	.01	1.86	1.55	.91	.013	.00	.00	PIPE
-6657.883	2741.807	1.927	2743.734	60.00	10.01	1.56	2745.29	.00	2.33	4.00	4.000	.000	.00	0 .0
.525	.1378					.0074	.00	1.93	1.44	.91	.013	.00	.00	PIPE
-6657.358	2741.879	2.000	2743.879	60.00	9.54	1.41	2745.29	.00	2.33	4.00	4.000	.000	.00	0 .0
.393	.1378					.0066	.00	2.00	1.34	.91	.013	.00	.00	PIPE
-6656.965	2741.933	2.077	2744.010	60.00	9.10	1.29	2745.30	.00	2.33	4.00	4.000	.000	.00	0 .0
.272	.1378					.0058	.00	2.08	1.25	.91	.013	.00	.00	PIPE
-6656.693	2741.971	2.158	2744.129	60.00	8.68	1.17	2745.30	.00	2.33	3.99	4.000	.000	.00	0 .0
.160	.1378					.0051	.00	2.16	1.16	.91	.013	.00	.00	PIPE
-6656.533	2741.993	2.243	2744.236	60.00	8.27	1.06	2745.30	.00	2.33	3.97	4.000	.000	.00	0 .0
.053	.1378					.0045	.00	2.24	1.08	.91	.013	.00	.00	PIPE
-6656.480	2742.000	2.334	2744.333	60.00	7.88	.96	2745.30	.00	2.33	3.94	4.000	.000	.00	0 .0

9

MAIN1_FAC9A.WSW

T1 THE SEVENTY

T2 GCW INC. PROJECT# 840.050

T3 FILENAME: MAIN1_FAC9A.WSW SHT

SO	-7116.3802720.753	24	2725.405			
R	-7078.2202721.390	24		.013	60.000	.000 1
R	-6805.9002728.200	24		.013	-60.000	.000 1
R	-6618.8802747.000	24		.013	0.000	.000 0
SH	-6618.8802747.000	24	.000			
CD	18	4		1.500		
CD	24	4		2.000		
CD	30	4		2.500		
CD	36	4		3.000		
CD	42	4		3.500		
CD	48	4		4.000		
CD	54	4		4.500		
CD	60	4		5.000		
CD	72	4		6.000		
Q			6.000	.0		

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC9A.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-7116.380	2720.753	4.652	2725.405	6.00	1.91	.06	2725.46	.00	.87	.00	2.000	.000	.00	0 .0
38.160	.0167					.0007	.03	.00	.00	.61	.013	.00	.00	PIPE
-7078.220	2721.390	4.054	2725.444	6.00	1.91	.06	2725.50	.00	.87	.00	2.000	.000	.00	0 .0
84.764	.0250					.0007	.06	.00	.00	.55	.013	.00	.00	PIPE
-6993.457	2723.510	2.000	2725.510	6.00	1.91	.06	2725.57	2.00	.87	.00	2.000	.000	.00	0 .0
7.359	.0250					.0007	.00	2.00	.00	.55	.013	.00	.00	PIPE
-6986.097	2723.694	1.814	2725.508	6.00	2.00	.06	2725.57	.00	.87	1.16	2.000	.000	.00	0 .0
4.176	.0250					.0006	.00	1.81	.22	.55	.013	.00	.00	PIPE
-6981.921	2723.798	1.706	2725.504	6.00	2.10	.07	2725.57	.00	.87	1.42	2.000	.000	.00	0 .0
3.337	.0250					.0007	.00	1.71	.26	.55	.013	.00	.00	PIPE
-6978.584	2723.882	1.618	2725.500	6.00	2.20	.08	2725.58	.00	.87	1.57	2.000	.000	.00	0 .0
2.906	.0250					.0008	.00	1.62	.30	.55	.013	.00	.00	PIPE
-6975.679	2723.954	1.540	2725.494	6.00	2.31	.08	2725.58	.00	.87	1.68	2.000	.000	.00	0 .0
2.554	.0250					.0008	.00	1.54	.33	.55	.013	.00	.00	PIPE
-6973.125	2724.018	1.470	2725.489	6.00	2.42	.09	2725.58	.00	.87	1.77	2.000	.000	.00	0 .0
2.280	.0250					.0009	.00	1.47	.36	.55	.013	.00	.00	PIPE
-6970.845	2724.075	1.406	2725.481	6.00	2.54	.10	2725.58	.00	.87	1.83	2.000	.000	.00	0 .0
2.086	.0250					.0011	.00	1.41	.39	.55	.013	.00	.00	PIPE

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC9A.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-6968.759	2724.128	1.346	2725.474	6.00	2.67	.11	2725.58	.00	.87	1.88	2.000	.000	.00	0 .0
1.686	.0250					.0012	.00	1.35	.43	.55	.013	.00	.00	PIPE
-6967.073	2724.170	1.291	2725.461	6.00	2.80	.12	2725.58	.00	.87	1.91	2.000	.000	.00	0 .0
HYDRAULIC JUMP														
-6967.073	2724.170	.554	2724.724	6.00	8.46	1.11	2725.83	.02	.87	1.79	2.000	.000	.00	0 .0
15.837	.0250					.0250	.40	.57	2.37	.55	.013	.00	.00	PIPE
-6951.236	2724.566	.554	2725.120	6.00	8.46	1.11	2726.23	.02	.87	1.79	2.000	.000	.00	0 .0
50.984	.0250					.0256	1.31	.57	2.37	.55	.013	.00	.00	PIPE
-6900.251	2725.841	.547	2726.388	6.00	8.60	1.15	2727.54	.02	.87	1.78	2.000	.000	.00	0 .0
31.144	.0250					.0281	.88	.56	2.42	.55	.013	.00	.00	PIPE
-6869.107	2726.619	.529	2727.148	6.00	9.02	1.26	2728.41	.02	.87	1.76	2.000	.000	.00	0 .0
15.202	.0250					.0321	.49	.55	2.59	.55	.013	.00	.00	PIPE
-6853.905	2727.000	.511	2727.510	6.00	9.46	1.39	2728.90	.02	.87	1.74	2.000	.000	.00	0 .0
10.409	.0250					.0367	.38	.53	2.77	.55	.013	.00	.00	PIPE
-6843.497	2727.260	.494	2727.754	6.00	9.93	1.53	2729.28	.02	.87	1.73	2.000	.000	.00	0 .0
8.010	.0250					.0420	.34	.51	2.96	.55	.013	.00	.00	PIPE
-6835.487	2727.460	.477	2727.937	6.00	10.41	1.68	2729.62	.02	.87	1.70	2.000	.000	.00	0 .0
6.659	.0250					.0480	.32	.50	3.16	.55	.013	.00	.00	PIPE

MAIN1_FAC9A.OUT

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC9A.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-6828.828	2727.626	.462	2728.089	6.00	10.92	1.85	2729.94	.02	.87	1.69	2.000	.000	.00	0 .0
5.652	.0250					.0549	.31	.49	3.37	.55	.013	.00	.00	PIPE
-6823.176	2727.768	.446	2728.214	6.00	11.45	2.04	2730.25	.03	.87	1.67	2.000	.000	.00	0 .0
5.012	.0250					.0628	.31	.47	3.60	.55	.013	.00	.00	PIPE
-6818.164	2727.893	.432	2728.325	6.00	12.01	2.24	2730.57	.03	.87	1.65	2.000	.000	.00	0 .0
4.458	.0250					.0719	.32	.46	3.84	.55	.013	.00	.00	PIPE
-6813.705	2728.005	.417	2728.422	6.00	12.60	2.46	2730.89	.03	.87	1.63	2.000	.000	.00	0 .0
4.077	.0250					.0823	.34	.45	4.10	.55	.013	.00	.00	PIPE
-6809.628	2728.107	.404	2728.511	6.00	13.21	2.71	2731.22	.03	.87	1.61	2.000	.000	.00	0 .0
3.728	.0250					.0942	.35	.44	4.38	.55	.013	.00	.00	PIPE
-6805.899	2728.200	.391	2728.592	6.00	13.86	2.98	2731.57	.00	.87	1.59	2.000	.000	.00	0 .0
67.802	.1005					.1006	6.82	.39	4.67	.39	.013	.00	.00	PIPE
-6738.097	2735.016	.391	2735.407	6.00	13.86	2.98	2738.39	.00	.87	1.59	2.000	.000	.00	0 .0
41.953	.1005					.0999	4.19	.39	4.67	.39	.013	.00	.00	PIPE
-6696.145	2739.233	.392	2739.625	6.00	13.80	2.96	2742.58	.00	.87	1.59	2.000	.000	.00	0 .0
33.984	.1005					.0930	3.16	.39	4.65	.39	.013	.00	.00	PIPE
-6662.160	2742.650	.405	2743.055	6.00	13.15	2.69	2745.74	.00	.87	1.61	2.000	.000	.00	0 .0
11.954	.1005					.0813	.97	.41	4.35	.39	.013	.00	.00	PIPE

* FILE: MAIN1_FAC9A.WSW

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Program Package Serial Number: 7044

WATER SURFACE PROFILE LISTING

Date: 3- 3-2016 Time:10: 9:29

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC9A.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-6650.207	2743.851	.419	2744.271	6.00	12.54	2.44	2746.71	.00	.87	1.63	2.000	.000	.00	0 .0
7.052	.1005					.0710	.50	.42	4.08	.39	.013	.00	.00	PIPE
-6643.155	2744.560	.433	2744.993	6.00	11.96	2.22	2747.21	.00	.87	1.65	2.000	.000	.00	0 .0
4.859	.1005					.0621	.30	.43	3.82	.39	.013	.00	.00	PIPE
-6638.295	2745.049	.448	2745.497	6.00	11.40	2.02	2747.52	.00	.87	1.67	2.000	.000	.00	0 .0
3.643	.1005					.0543	.20	.45	3.58	.39	.013	.00	.00	PIPE
-6634.653	2745.415	.463	2745.878	6.00	10.87	1.84	2747.71	.00	.87	1.69	2.000	.000	.00	0 .0
2.841	.1005					.0474	.13	.46	3.35	.39	.013	.00	.00	PIPE
-6631.812	2745.700	.479	2746.179	6.00	10.36	1.67	2747.85	.00	.87	1.71	2.000	.000	.00	0 .0
2.297	.1005					.0415	.10	.48	3.14	.39	.013	.00	.00	PIPE
-6629.515	2745.931	.495	2746.427	6.00	9.88	1.52	2747.94	.00	.87	1.73	2.000	.000	.00	0 .0
1.880	.1005					.0363	.07	.50	2.94	.39	.013	.00	.00	PIPE
-6627.635	2746.120	.512	2746.633	6.00	9.42	1.38	2748.01	.00	.87	1.75	2.000	.000	.00	0 .0
1.560	.1005					.0317	.05	.51	2.75	.39	.013	.00	.00	PIPE
-6626.075	2746.277	.530	2746.807	6.00	8.98	1.25	2748.06	.00	.87	1.77	2.000	.000	.00	0 .0
1.305	.1005					.0278	.04	.53	2.57	.39	.013	.00	.00	PIPE
-6624.770	2746.408	.549	2746.957	6.00	8.57	1.14	2748.10	.00	.87	1.79	2.000	.000	.00	0 .0
1.110	.1005					.0243	.03	.55	2.41	.39	.013	.00	.00	PIPE

* FILE: MAIN1_FAC9A.WSW

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Program Package Serial Number: 7044

WATER SURFACE PROFILE LISTING

Date: 3- 3-2016 Time:10: 9:29

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC9A.WSW SHT

MAIN1_FAC9A.OUT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-6623.660	2746.520	.568	2747.088	6.00	8.17	1.04	2748.12	.00	.87	1.80	2.000	.000	.00	0 .0
.948	.1005					.0213	.02	.57	2.26	.39	.013	.00	.00	PIPE
-6622.712	2746.615	.587	2747.202	6.00	7.79	.94	2748.14	.00	.87	1.82	2.000	.000	.00	0 .0
.789	.1005					.0186	.01	.59	2.11	.39	.013	.00	.00	PIPE
-6621.923	2746.694	.608	2747.302	6.00	7.42	.86	2748.16	.00	.87	1.84	2.000	.000	.00	0 .0
.675	.1005					.0163	.01	.61	1.97	.39	.013	.00	.00	PIPE
-6621.249	2746.762	.629	2747.391	6.00	7.08	.78	2748.17	.00	.87	1.86	2.000	.000	.00	0 .0
.565	.1005					.0143	.01	.63	1.85	.39	.013	.00	.00	PIPE
-6620.684	2746.819	.651	2747.470	6.00	6.75	.71	2748.18	.00	.87	1.87	2.000	.000	.00	0 .0
.469	.1005					.0125	.01	.65	1.73	.39	.013	.00	.00	PIPE
-6620.214	2746.866	.674	2747.540	6.00	6.44	.64	2748.18	.00	.87	1.89	2.000	.000	.00	0 .0
.385	.1005					.0109	.00	.67	1.62	.39	.013	.00	.00	PIPE
-6619.830	2746.905	.698	2747.603	6.00	6.14	.58	2748.19	.00	.87	1.91	2.000	.000	.00	0 .0
.310	.1005					.0096	.00	.70	1.51	.39	.013	.00	.00	PIPE
-6619.520	2746.936	.723	2747.659	6.00	5.85	.53	2748.19	.00	.87	1.92	2.000	.000	.00	0 .0
.242	.1005					.0084	.00	.72	1.41	.39	.013	.00	.00	PIPE
-6619.278	2746.960	.749	2747.709	6.00	5.58	.48	2748.19	.00	.87	1.94	2.000	.000	.00	0 .0
.182	.1005					.0074	.00	.75	1.32	.39	.013	.00	.00	PIPE

♀ FILE: MAIN1_FAC9A.WSW

W S P G W - CIVILDESIGN Version 14.08

Program Package Serial Number: 7044

WATER SURFACE PROFILE LISTING

Date: 3- 3-2016 Time:10: 9:29

THE SEVENTY

GCW INC. PROJECT# 840.050

FILENAME: MAIN1_FAC9A.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-6619.096	2746.979	.776	2747.755	6.00	5.32	.44	2748.19	.00	.87	1.95	2.000	.000	.00	0 .0
.127	.1005					.0065	.00	.78	1.23	.39	.013	.00	.00	PIPE
-6618.969	2746.991	.804	2747.795	6.00	5.07	.40	2748.19	.00	.87	1.96	2.000	.000	.00	0 .0
.066	.1005					.0057	.00	.80	1.15	.39	.013	.00	.00	PIPE
-6618.903	2746.998	.834	2747.832	6.00	4.84	.36	2748.20	.00	.87	1.97	2.000	.000	.00	0 .0
.023	.1005					.0050	.00	.83	1.07	.39	.013	.00	.00	PIPE
-6618.880	2747.000	.866	2747.866	6.00	4.60	.33	2748.20	.00	.87	1.98	2.000	.000	.00	0 .0

♀

MAIN1_FAC10A.WSW

T1 THE SEVENTY

T2 GCW INC. PROJECT# 840.050

T3 FILENAME: MAIN1_FAC10A.WSW

SO 7790.9102687.180 48

2692.147

R 7806.9102689.220 48 .013

4.000 .000 1

R 7827.3302695.000 48 .013

.000 .000

SH 7827.3302695.000 48

.000

CD 18 4 1.500

CD 24 4 2.000

CD 30 4 2.500

CD 36 4 3.000

CD 42 4 3.500

CD 48 4 4.000

CD 54 4 4.500

CD 60 4 5.000

CD 72 4 6.000

Q 23.000 .0

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC10A.WSW

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
7790.910	2687.180	4.967	2692.147	23.00	1.83	.05	2692.20	.00	1.41	.00	4.000	.000	.00	0 .0
7.622	.1275					.0003	.00	.00	.00	.58	.013	.00	.00	PIPE
7798.532	2688.152	4.000	2692.152	23.00	1.83	.05	2692.20	4.00	1.41	.00	4.000	.000	.00	0 .0
2.866	.1275					.0002	.00	4.00	.00	.58	.013	.00	.00	PIPE
7801.397	2688.517	3.629	2692.146	23.00	1.92	.06	2692.20	.00	1.41	2.32	4.000	.000	.00	0 .0
1.652	.1275					.0002	.00	3.63	.15	.58	.013	.00	.00	PIPE
7803.050	2688.728	3.413	2692.141	23.00	2.01	.06	2692.20	.00	1.41	2.83	4.000	.000	.00	0 .0
1.341	.1275					.0003	.00	3.41	.18	.58	.013	.00	.00	PIPE
7804.391	2688.899	3.236	2692.135	23.00	2.11	.07	2692.20	.00	1.41	3.14	4.000	.000	.00	0 .0
1.172	.1275					.0003	.00	3.24	.20	.58	.013	.00	.00	PIPE
7805.563	2689.048	3.080	2692.128	23.00	2.21	.08	2692.20	.00	1.41	3.37	4.000	.000	.00	0 .0
1.041	.1275					.0003	.00	3.08	.22	.58	.013	.00	.00	PIPE
7806.604	2689.181	2.940	2692.121	23.00	2.32	.08	2692.21	.00	1.41	3.53	4.000	.000	.00	0 .0
.305	.1275					.0003	.00	2.94	.24	.58	.013	.00	.00	PIPE
7806.909	2689.220	2.899	2692.119	23.00	2.36	.09	2692.20	.00	1.41	3.57	4.000	.000	.00	0 .0
HYDRAULIC JUMP														
7806.910	2689.219	.598	2689.817	23.00	19.56	5.94	2695.76	.00	1.41	2.85	4.000	.000	.00	0 .0
1.546	.2831					.1062	.16	.60	5.37	.48	.013	.00	.00	PIPE

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC10A.WSW

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
7808.456	2689.657	.608	2690.265	23.00	19.07	5.65	2695.91	.00	1.41	2.87	4.000	.000	.00	0 .0
2.635	.2831					.0959	.25	.61	5.19	.48	.013	.00	.00	PIPE
7811.091	2690.403	.628	2691.031	23.00	18.18	5.13	2696.16	.00	1.41	2.91	4.000	.000	.00	0 .0
2.235	.2831					.0837	.19	.63	4.86	.48	.013	.00	.00	PIPE
7813.326	2691.036	.649	2691.685	23.00	17.33	4.67	2696.35	.00	1.41	2.95	4.000	.000	.00	0 .0
1.915	.2831					.0731	.14	.65	4.55	.48	.013	.00	.00	PIPE
7815.241	2691.578	.671	2692.249	23.00	16.53	4.24	2696.49	.00	1.41	2.99	4.000	.000	.00	0 .0
1.654	.2831					.0638	.11	.67	4.27	.48	.013	.00	.00	PIPE
7816.895	2692.046	.694	2692.740	23.00	15.76	3.86	2696.60	.00	1.41	3.03	4.000	.000	.00	0 .0
1.441	.2831					.0558	.08	.69	4.00	.48	.013	.00	.00	PIPE
7818.335	2692.454	.717	2693.171	23.00	15.02	3.51	2696.68	.00	1.41	3.07	4.000	.000	.00	0 .0
1.257	.2831					.0487	.06	.72	3.75	.48	.013	.00	.00	PIPE
7819.593	2692.810	.741	2693.551	23.00	14.33	3.19	2696.74	.00	1.41	3.11	4.000	.000	.00	0 .0
1.101	.2831					.0425	.05	.74	3.51	.48	.013	.00	.00	PIPE
7820.693	2693.121	.766	2693.887	23.00	13.66	2.90	2696.78	.00	1.41	3.15	4.000	.000	.00	0 .0
.965	.2831					.0372	.04	.77	3.29	.48	.013	.00	.00	PIPE
7821.659	2693.395	.792	2694.187	23.00	13.02	2.63	2696.82	.00	1.41	3.19	4.000	.000	.00	0 .0
.848	.2831					.0325	.03	.79	3.08	.48	.013	.00	.00	PIPE

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC10A.WSW

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
7822.506	2693.635	.819	2694.454	23.00	12.42	2.39	2696.85	.00	1.41	3.23	4.000	.000	.00	0 .0
.745	.2831					.0284	.02	.82	2.89	.48	.013	.00	.00	PIPE
7823.251	2693.845	.847	2694.692	23.00	11.84	2.18	2696.87	.00	1.41	3.27	4.000	.000	.00	0 .0
.654	.2831					.0248	.02	.85	2.71	.48	.013	.00	.00	PIPE
7823.905	2694.030	.876	2694.906	23.00	11.29	1.98	2696.89	.00	1.41	3.31	4.000	.000	.00	0 .0
.573	.2831					.0217	.01	.88	2.53	.48	.013	.00	.00	PIPE
7824.478	2694.193	.906	2695.099	23.00	10.76	1.80	2696.90	.00	1.41	3.35	4.000	.000	.00	0 .0
.502	.2831					.0190	.01	.91	2.37	.48	.013	.00	.00	PIPE
7824.980	2694.335	.937	2695.272	23.00	10.26	1.64	2696.91	.00	1.41	3.39	4.000	.000	.00	0 .0
.438	.2831					.0166	.01	.94	2.22	.48	.013	.00	.00	PIPE
7825.418	2694.459	.969	2695.428	23.00	9.78	1.49	2696.91	.00	1.41	3.43	4.000	.000	.00	0 .0
.380	.2831					.0145	.01	.97	2.08	.48	.013	.00	.00	PIPE
7825.798	2694.566	1.002	2695.569	23.00	9.33	1.35	2696.92	.00	1.41	3.47	4.000	.000	.00	0 .0
.325	.2831					.0127	.00	1.00	1.95	.48	.013	.00	.00	PIPE
7826.123	2694.658	1.037	2695.696	23.00	8.90	1.23	2696.92	.00	1.41	3.51	4.000	.000	.00	0 .0
.282	.2831					.0111	.00	1.04	1.83	.48	.013	.00	.00	PIPE
7826.405	2694.738	1.072	2695.810	23.00	8.48	1.12	2696.93	.00	1.41	3.54	4.000	.000	.00	0 .0
.236	.2831					.0097	.00	1.07	1.71	.48	.013	.00	.00	PIPE

♀ FILE: MAIN1_FAC10A.WSW

W S P G W - CIVILDESIGN Version 14.08

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Program Package Serial Number: 7044

WATER SURFACE PROFILE LISTING

Date: 3- 3-2016 Time:10:10: 8

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC10A.WSW

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
7826.642	2694.805	1.109	2695.914	23.00	8.09	1.02	2696.93	.00	1.41	3.58	4.000	.000	.00	0 .0
.194	.2831					.0085	.00	1.11	1.60	.48	.013	.00	.00	PIPE
7826.836	2694.860	1.148	2696.008	23.00	7.71	.92	2696.93	.00	1.41	3.62	4.000	.000	.00	0 .0
.159	.2831					.0074	.00	1.15	1.50	.48	.013	.00	.00	PIPE
7826.995	2694.905	1.188	2696.093	23.00	7.35	.84	2696.93	.00	1.41	3.66	4.000	.000	.00	0 .0
.124	.2831					.0065	.00	1.19	1.40	.48	.013	.00	.00	PIPE
7827.119	2694.940	1.230	2696.170	23.00	7.01	.76	2696.93	.00	1.41	3.69	4.000	.000	.00	0 .0
.095	.2831					.0057	.00	1.23	1.31	.48	.013	.00	.00	PIPE
7827.214	2694.967	1.273	2696.240	23.00	6.68	.69	2696.93	.00	1.41	3.73	4.000	.000	.00	0 .0
.065	.2831					.0050	.00	1.27	1.23	.48	.013	.00	.00	PIPE
7827.279	2694.986	1.318	2696.304	23.00	6.37	.63	2696.93	.00	1.41	3.76	4.000	.000	.00	0 .0
.041	.2831					.0044	.00	1.32	1.15	.48	.013	.00	.00	PIPE
7827.320	2694.997	1.364	2696.361	23.00	6.08	.57	2696.93	.00	1.41	3.79	4.000	.000	.00	0 .0
.010	.2831					.0038	.00	1.36	1.07	.48	.013	.00	.00	PIPE
7827.330	2695.000	1.414	2696.414	23.00	5.79	.52	2696.93	.00	1.41	3.82	4.000	.000	.00	0 .0

♀

MAIN1_FAC10B.WSW

T1 THE SEVENTY					
T2	GCW INC. PROJECT# 840.050				
T3	FILENAME: MAIN1_FAC10B.WSW				
SO	-7762.9102686.410 48		2692.147		
R	-7746.9102687.580 48	.013		28.340	.000 1
R	-7707.3402694.000 48	.013		.000	.000
SH	-7707.3402694.000 48		.000		
CD	18 4	1.500			
CD	24 4	2.000			
CD	30 4	2.500			
CD	36 4	3.000			
CD	42 4	3.500			
CD	48 4	4.000			
CD	54 4	4.500			
CD	60 4	5.000			
CD	72 4	6.000			
Q		36.000	.0		

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC10B.WSW

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-7762.910	2686.410	5.737	2692.147	36.00	2.86	.13	2692.27	.00	1.79	.00	4.000	.000	.00	0 .0
16.000	.0731					.0006	.01	.00	.00	.82	.013	.00	.00	PIPE
-7746.910	2687.580	4.598	2692.178	36.00	2.86	.13	2692.31	.00	1.79	.00	4.000	.000	.00	0 .0
3.698	.1622					.0006	.00	4.60	.00	.68	.013	.00	.00	PIPE
-7743.212	2688.180	4.000	2692.180	36.00	2.86	.13	2692.31	.00	1.79	.00	4.000	.000	.00	0 .0
2.209	.1622					.0006	.00	4.00	.00	.68	.013	.00	.00	PIPE
-7741.003	2688.538	3.629	2692.167	36.00	3.00	.14	2692.31	.00	1.79	2.32	4.000	.000	.00	0 .0
1.025	.1622					.0006	.00	3.63	.23	.68	.013	.00	.00	PIPE
-7739.978	2688.705	3.452	2692.157	36.00	3.12	.15	2692.31	.00	1.79	2.75	4.000	.000	.00	0 .0
HYDRAULIC JUMP														
-7739.978	2688.705	.829	2689.533	36.00	19.12	5.68	2695.21	.00	1.79	3.24	4.000	.000	.00	0 .0
.856	.1622					.0699	.06	.83	4.42	.68	.013	.00	.00	PIPE
-7739.121	2688.844	.834	2689.677	36.00	18.93	5.57	2695.24	.00	1.79	3.25	4.000	.000	.00	0 .0
4.885	.1622					.0646	.32	.83	4.36	.68	.013	.00	.00	PIPE
-7734.236	2689.636	.863	2690.499	36.00	18.05	5.06	2695.56	.00	1.79	3.29	4.000	.000	.00	0 .0
4.075	.1622					.0565	.23	.86	4.09	.68	.013	.00	.00	PIPE
-7730.161	2690.297	.892	2691.189	36.00	17.21	4.60	2695.79	.00	1.79	3.33	4.000	.000	.00	0 .0
3.430	.1622					.0494	.17	.89	3.83	.68	.013	.00	.00	PIPE

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC10B.WSW

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-7726.731	2690.854	.923	2691.777	36.00	16.41	4.18	2695.96	.00	1.79	3.37	4.000	.000	.00	0 .0
2.932	.1622					.0432	.13	.92	3.59	.68	.013	.00	.00	PIPE
-7723.799	2691.329	.954	2692.283	36.00	15.65	3.80	2696.09	.00	1.79	3.41	4.000	.000	.00	0 .0
2.511	.1622					.0377	.09	.95	3.36	.68	.013	.00	.00	PIPE
-7721.288	2691.737	.987	2692.724	36.00	14.92	3.46	2696.18	.00	1.79	3.45	4.000	.000	.00	0 .0
2.168	.1622					.0330	.07	.99	3.14	.68	.013	.00	.00	PIPE
-7719.120	2692.089	1.021	2693.110	36.00	14.23	3.14	2696.25	.00	1.79	3.49	4.000	.000	.00	0 .0
1.879	.1622					.0289	.05	1.02	2.94	.68	.013	.00	.00	PIPE
-7717.241	2692.394	1.056	2693.450	36.00	13.56	2.86	2696.31	.00	1.79	3.53	4.000	.000	.00	0 .0
1.625	.1622					.0252	.04	1.06	2.76	.68	.013	.00	.00	PIPE
-7715.615	2692.657	1.093	2693.750	36.00	12.93	2.60	2696.35	.00	1.79	3.57	4.000	.000	.00	0 .0
1.420	.1622					.0221	.03	1.09	2.58	.68	.013	.00	.00	PIPE
-7714.195	2692.888	1.130	2694.018	36.00	12.33	2.36	2696.38	.00	1.79	3.60	4.000	.000	.00	0 .0
1.222	.1622					.0193	.02	1.13	2.41	.68	.013	.00	.00	PIPE
-7712.973	2693.086	1.170	2694.256	36.00	11.76	2.15	2696.40	.00	1.79	3.64	4.000	.000	.00	0 .0
1.061	.1622					.0169	.02	1.17	2.26	.68	.013	.00	.00	PIPE
-7711.913	2693.258	1.211	2694.469	36.00	11.21	1.95	2696.42	.00	1.79	3.68	4.000	.000	.00	0 .0
.918	.1622					.0148	.01	1.21	2.11	.68	.013	.00	.00	PIPE

MAIN1_FAC10B.OUT

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC10B.WSW

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-7710.995	2693.407	1.253	2694.660	36.00	10.69	1.77	2696.43	.00	1.79	3.71	4.000	.000	.00	0 .0
.786	.1622					.0130	.01	1.25	1.98	.68	.013	.00	.00	PIPE
-7710.209	2693.534	1.297	2694.832	36.00	10.19	1.61	2696.44	.00	1.79	3.74	4.000	.000	.00	0 .0
.667	.1622					.0114	.01	1.30	1.85	.68	.013	.00	.00	PIPE
-7709.542	2693.643	1.343	2694.986	36.00	9.72	1.47	2696.45	.00	1.79	3.78	4.000	.000	.00	0 .0
.560	.1622					.0100	.01	1.34	1.73	.68	.013	.00	.00	PIPE
-7708.982	2693.733	1.391	2695.125	36.00	9.26	1.33	2696.46	.00	1.79	3.81	4.000	.000	.00	0 .0
.470	.1622					.0087	.00	1.39	1.62	.68	.013	.00	.00	PIPE
-7708.513	2693.810	1.440	2695.250	36.00	8.83	1.21	2696.46	.00	1.79	3.84	4.000	.000	.00	0 .0
.376	.1622					.0077	.00	1.44	1.51	.68	.013	.00	.00	PIPE
-7708.137	2693.871	1.492	2695.363	36.00	8.42	1.10	2696.46	.00	1.79	3.87	4.000	.000	.00	0 .0
.296	.1622					.0067	.00	1.49	1.41	.68	.013	.00	.00	PIPE
-7707.840	2693.919	1.546	2695.465	36.00	8.03	1.00	2696.47	.00	1.79	3.90	4.000	.000	.00	0 .0
.224	.1622					.0059	.00	1.55	1.32	.68	.013	.00	.00	PIPE
-7707.616	2693.955	1.602	2695.557	36.00	7.66	.91	2696.47	.00	1.79	3.92	4.000	.000	.00	0 .0
.158	.1622					.0052	.00	1.60	1.23	.68	.013	.00	.00	PIPE
-7707.458	2693.981	1.660	2695.641	36.00	7.30	.83	2696.47	.00	1.79	3.94	4.000	.000	.00	0 .0
.090	.1622					.0045	.00	1.66	1.15	.68	.013	.00	.00	PIPE

♀ FILE: MAIN1_FAC10B.WSW

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Program Package Serial Number: 7044

WATER SURFACE PROFILE LISTING

Date: 3- 3-2016 Time:10:31:10

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC10B.WSW

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-7707.368	2693.995	1.721	2695.717	36.00	6.96	.75	2696.47	.00	1.79	3.96	4.000	.000	.00	0 .0
.028	.1622					.0040	.00	1.72	1.07	.68	.013	.00	.00	PIPE
-7707.340	2694.000	1.786	2695.786	36.00	6.63	.68	2696.47	.00	1.79	3.98	4.000	.000	.00	0 .0

♀

MAIN1_FAC12A.WSW

T1 THE SEVENTY

T2 GCW INC. PROJECT# 840.050

T3 FILENAME: MAIN1_FAC12A.WSW SHT

SO 8723.6402677.000 24

2685.475

R 8739.6402678.080 24 .013

0.000 .000 0

SH 8739.6402678.080 24

.000

CD 18 4 1.500

CD 24 4 2.000

CD 30 4 2.500

CD 36 4 3.000

CD 42 4 3.500

CD 48 4 4.000

CD 54 4 4.500

CD 60 4 5.000

CD 72 4 6.000

Q 22.000 .0

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC12A.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
8723.640	2677.000	8.475	2685.475	22.00	7.00	.76	2686.24	.00	1.68	.00	2.000	.000	.00	0 .0
16.000	.0675					.0095	.15	8.48	.00	.85	.013	.00	.00	PIPE
8739.640	2678.080	7.546	2685.626	22.00	7.00	.76	2686.39	.00	1.68	.00	2.000	.000	.00	0 .0

MAIN1_FAC12B.WSW

T1 THE SEVENTY

T2 GCW INC. PROJECT# 840.050

T3 FILENAME: MAIN1_FAC12B.WSW SHT

SO -8695.6402677.000 24

2685.475

R -8679.6402678.080 24 .013

0.000 .000 0

SH -8679.6402678.080 24

.000

CD 18 4 1.500

CD 24 4 2.000

CD 30 4 2.500

CD 36 4 3.000

CD 42 4 3.500

CD 48 4 4.000

CD 54 4 4.500

CD 60 4 5.000

CD 72 4 6.000

Q 22.000 .0

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC12B.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-8695.640	2677.000	8.475	2685.475	22.00	7.00	.76	2686.24	.00	1.68	.00	2.000	.000	.00	0 .0
16.000	.0675					.0095	.15	8.48	.00	.85	.013	.00	.00	PIPE
-8679.640	2678.080	7.546	2685.626	22.00	7.00	.76	2686.39	.00	1.68	.00	2.000	.000	.00	0 .0

MAIN1_FAC13A.WSW

T1 THE SEVENTY

T2 GCW INC. PROJECT# 840.050

T3 FILENAME: MAIN1_FAC13A.WSW

SO	-9166.0602668.400	36		2675.655			
R	-9136.0602672.900	36	.013		14.000	.000	1
R	-9121.9202675.020	36	.013		.000	.000	
SH	-9121.9202675.020	36		.000			
CD	18	4					
						1.500	
CD	24	4				2.000	
CD	30	4				2.500	
CD	36	4				3.000	
CD	42	4				3.500	
CD	48	4				4.000	
CD	54	4				4.500	
CD	60	4				5.000	
CD	72	4				6.000	
Q			22.000	.0			

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC13A.WSW

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-9166.060	2668.400	7.255	2675.655	22.00	3.11	.15	2675.81	.00	1.51	.00	3.000	.000	.00	0 .0
28.701	.1500					.0011	.03	.00	.00	.59	.013	.00	.00	PIPE
-9137.358	2672.705	3.000	2675.705	22.00	3.11	.15	2675.86	3.00	1.51	.00	3.000	.000	.00	0 .0
1.299	.1500					.0010	.00	3.00	.00	.59	.013	.00	.00	PIPE
-9136.060	2672.900	2.796	2675.696	22.00	3.21	.16	2675.86	.00	1.51	1.51	3.000	.000	.00	0 .0
1.103	.1499					.0010	.00	2.80	.27	.59	.013	.00	.00	PIPE
-9134.957	2673.065	2.616	2675.681	22.00	3.36	.18	2675.86	.00	1.51	2.00	3.000	.000	.00	0 .0
.437	.1499					.0010	.00	2.62	.33	.59	.013	.00	.00	PIPE
-9134.521	2673.131	2.542	2675.673	22.00	3.44	.18	2675.86	.00	1.51	2.16	3.000	.000	.00	0 .0
HYDRAULIC JUMP														
-9134.521	2673.131	.837	2673.968	22.00	13.65	2.89	2676.86	.00	1.51	2.69	3.000	.000	.00	0 .0
1.113	.1499					.0362	.04	.84	3.11	.59	.013	.00	.00	PIPE
-9133.407	2673.298	.854	2674.152	22.00	13.26	2.73	2676.88	.00	1.51	2.71	3.000	.000	.00	0 .0
1.858	.1499					.0325	.06	.85	2.99	.59	.013	.00	.00	PIPE
-9131.549	2673.576	.884	2674.460	22.00	12.64	2.48	2676.94	.00	1.51	2.74	3.000	.000	.00	0 .0
1.603	.1499					.0285	.05	.88	2.79	.59	.013	.00	.00	PIPE
-9129.946	2673.817	.915	2674.732	22.00	12.05	2.26	2676.99	.00	1.51	2.76	3.000	.000	.00	0 .0
1.385	.1499					.0249	.03	.92	2.61	.59	.013	.00	.00	PIPE

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC13A.WSW

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-9128.562	2674.024	.947	2674.971	22.00	11.49	2.05	2677.02	.00	1.51	2.79	3.000	.000	.00	0 .0
1.198	.1499					.0218	.03	.95	2.44	.59	.013	.00	.00	PIPE
-9127.363	2674.204	.980	2675.184	22.00	10.96	1.86	2677.05	.00	1.51	2.81	3.000	.000	.00	0 .0
1.028	.1499					.0191	.02	.98	2.29	.59	.013	.00	.00	PIPE
-9126.335	2674.358	1.015	2675.374	22.00	10.45	1.70	2677.07	.00	1.51	2.84	3.000	.000	.00	0 .0
.887	.1499					.0168	.01	1.02	2.14	.59	.013	.00	.00	PIPE
-9125.448	2674.491	1.051	2675.542	22.00	9.96	1.54	2677.08	.00	1.51	2.86	3.000	.000	.00	0 .0
.763	.1499					.0147	.01	1.05	2.00	.59	.013	.00	.00	PIPE
-9124.686	2674.606	1.088	2675.694	22.00	9.50	1.40	2677.09	.00	1.51	2.88	3.000	.000	.00	0 .0
.645	.1499					.0129	.01	1.09	1.87	.59	.013	.00	.00	PIPE
-9124.041	2674.702	1.127	2675.830	22.00	9.06	1.27	2677.10	.00	1.51	2.91	3.000	.000	.00	0 .0
.539	.1499					.0113	.01	1.13	1.75	.59	.013	.00	.00	PIPE
-9123.502	2674.783	1.168	2675.951	22.00	8.64	1.16	2677.11	.00	1.51	2.93	3.000	.000	.00	0 .0
.452	.1499					.0099	.00	1.17	1.63	.59	.013	.00	.00	PIPE
-9123.050	2674.851	1.210	2676.061	22.00	8.23	1.05	2677.11	.00	1.51	2.94	3.000	.000	.00	0 .0
.366	.1499					.0087	.00	1.21	1.52	.59	.013	.00	.00	PIPE
-9122.684	2674.906	1.254	2676.160	22.00	7.85	.96	2677.12	.00	1.51	2.96	3.000	.000	.00	0 .0
.281	.1499					.0076	.00	1.25	1.42	.59	.013	.00	.00	PIPE

MAIN1_FAC13A.OUT

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC13A.WSW

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-9122.402	2674.948	1.301	2676.249	22.00	7.48	.87	2677.12	.00	1.51	2.97	3.000	.000	.00	0 .0
.217	.1499					.0067	.00	1.30	1.33	.59	.013	.00	.00	PIPE
-9122.186	2674.980	1.349	2676.330	22.00	7.14	.79	2677.12	.00	1.51	2.98	3.000	.000	.00	0 .0
.152	.1499					.0059	.00	1.35	1.24	.59	.013	.00	.00	PIPE
-9122.033	2675.003	1.399	2676.402	22.00	6.80	.72	2677.12	.00	1.51	2.99	3.000	.000	.00	0 .0
.085	.1499					.0052	.00	1.40	1.15	.59	.013	.00	.00	PIPE
-9121.948	2675.016	1.452	2676.468	22.00	6.49	.65	2677.12	.00	1.51	3.00	3.000	.000	.00	0 .0
.028	.1499					.0046	.00	1.45	1.08	.59	.013	.00	.00	PIPE
-9121.920	2675.020	1.508	2676.528	22.00	6.18	.59	2677.12	.00	1.51	3.00	3.000	.000	.00	0 .0

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MAIN1_FAC13B.WSW

T1 THE SEVENTY

T2 GCW INC. PROJECT# 840.050

T3 FILENAME: MAIN1_FAC13B.WSW

SO 9187.8102668.400 36

2675.655

R 9208.6502669.840 36 .013

24.240 .000 1

R 9238.3302671.880 36 .013

.000 .000

SH 9238.3302671.880 36

.000

CD 18 4 1.500

CD 24 4 2.000

CD 30 4 2.500

CD 36 4 3.000

CD 42 4 3.500

CD 48 4 4.000

CD 54 4 4.500

CD 60 4 5.000

CD 72 4 6.000

Q 22.000 .0

THE SEVENTY
 GCW INC. PROJECT# 840.050
 FILENAME: MAIN1_FAC13B.WSW

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
9187.810	2668.400	7.255	2675.655	22.00	3.11	.15	2675.81	.00	1.51	.00	3.000	.000	.00	0 .0
20.841	.0691					.0011	.02	.00	.00	.72	.013	.00	.00	PIPE
9208.650	2669.840	5.861	2675.701	22.00	3.11	.15	2675.85	.00	1.51	.00	3.000	.000	.00	0 .0
29.680	.0687					.0011	.03	5.86	.00	.72	.013	.00	.00	PIPE
9238.330	2671.880	3.853	2675.733	22.00	3.11	.15	2675.88	.00	1.51	.00	3.000	.000	.00	0 .0

WSPGW ANALYSIS

MAIN 2

MAIN2.WSW

T1	THE SEVENTY									
T2	GCW INC. PROJECT# 840.050									
T3	FILENAME: MAIN2-RCB2.WSW SHT									
SO	-7519.0102698.462	15							2703.115	
R	-7413.7302706.021	15		.015						89.000
R	-7319.4202712.792	15		.015						.000
R	-7198.3502721.485	15		.015						-62.000
R	-7059.4702724.374	15		.015						.000
R	-6981.7202725.991	15		.015						.000
R	-6923.1002727.210	15		.015						30.000
R	-6798.3502729.805	15		.015						.000
R	-6749.9902730.821	15		.015						.000
R	-6739.8902731.030	15		.015						30.000
R	-6609.8402733.736	15		.015						.000
R	-6526.9502734.565	15		.015						-42.000
JX	-6230.9102740.485	15	48	.015	23.000			2740.485		30.0
R	-6143.4902748.869	15		.015						.000
R	-6094.8102753.537	15		.015						-45.000
TS	-6083.2402754.647	18		.015						.000
R	-6052.2502757.619	18		.015						25.000
R	-6034.0202759.370	18		.015						41.800
SH	-6034.0202759.370	18							.000	
CD	10	3	1	1.000	12.000	25.000	.000	.000	.00	
CD	11	3	0	.000	9.000	17.000	.000	.000	.00	
CD	12	3	0	.000	12.000	25.000	.000	.000	.00	
CD	13	3	0	.000	12.000	15.000	.000	.000	.00	
CD	14	3	0	.000	9.000	12.000	.000	.000	.00	
CD	15	3	0	.000	8.000	10.000	.000	.000	.00	
CD	16	4	0	.000	6.000	.000	.000	.000	.00	
CD	17	4	0	.000	4.000	.000	.000	.000	.00	
CD	18	3	0	.000	9.000	20.000	.000	.000	.00	
CD	19	3	0	.000	9.000	20.000	.000	.000	.00	
CD	48	4	0	.000	4.000	.000	.000	.000	.00	
Q				1910.000	.0					

FILE: MAIN2.WSW

MAIN2.OUT
W S P G W - CIVILDESIGN Version 14.08
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THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN2-RCB2.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-7519.010	2698.462	4.749	2703.210	1933.00	40.71	25.73	2728.94	8.00	8.00	10.00	8.000	10.000	.00	0 .0
21.536	.0718					.0509	1.10	8.00	3.29	4.20	.015	.00	.00	BOX
-7497.474	2700.008	4.795	2704.803	1933.00	40.31	25.24	2730.04	8.00	8.00	10.00	8.000	10.000	.00	0 .0
83.744	.0718					.0472	3.95	8.00	3.24	4.20	.015	.00	.00	BOX
-7413.730	2706.021	5.029	2711.050	1933.00	38.44	22.94	2733.99	.00	8.00	10.00	8.000	10.000	.00	0 .0
43.842	.0718					.0424	1.86	5.03	3.02	4.20	.015	.00	.00	BOX
-7369.888	2709.169	5.196	2714.365	1933.00	37.20	21.49	2735.85	.00	8.00	10.00	8.000	10.000	.00	0 .0
50.468	.0718					.0381	1.92	5.20	2.88	4.20	.015	.00	.00	BOX
-7319.420	2712.792	5.450	2718.242	1933.00	35.47	19.53	2737.78	8.00	8.00	10.00	8.000	10.000	.00	0 .0
6.813	.0718					.0354	.24	8.00	2.68	4.20	.015	.00	.00	BOX
-7312.607	2713.281	5.491	2718.772	1933.00	35.21	19.25	2738.02	8.00	8.00	10.00	8.000	10.000	.00	0 .0
38.146	.0718					.0330	1.26	8.00	2.65	4.20	.015	.00	.00	BOX
-7274.460	2716.020	5.759	2721.779	1933.00	33.57	17.50	2739.28	8.00	8.00	10.00	8.000	10.000	.00	0 .0
30.661	.0718					.0291	.89	8.00	2.47	4.20	.015	.00	.00	BOX
-7243.800	2718.222	6.040	2724.261	1933.00	32.01	15.91	2740.17	8.00	8.00	10.00	8.000	10.000	.00	0 .0
24.969	.0718					.0257	.64	8.00	2.30	4.20	.015	.00	.00	BOX
-7218.831	2720.014	6.334	2726.349	1933.00	30.52	14.46	2740.81	8.00	8.00	10.00	8.000	10.000	.00	0 .0
20.481	.0718					.0227	.47	8.00	2.14	4.20	.015	.00	.00	BOX

FILE: MAIN2.WSW

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THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN2-RCB2.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-7198.350	2721.485	6.644	2728.129	1933.00	29.10	13.15	2741.27	.00	8.00	10.00	8.000	10.000	.00	0 .0
138.880	.0208					.0214	2.98	6.64	1.99	6.71	.015	.00	.00	BOX
-7059.470	2724.374	6.614	2730.988	1933.00	29.23	13.27	2744.25	.00	8.00	10.00	8.000	10.000	.00	0 .0
77.750	.0208					.0217	1.68	6.61	2.00	6.71	.015	.00	.00	BOX
-6981.720	2725.991	6.591	2732.582	1933.00	29.33	13.36	2745.94	8.00	8.00	10.00	8.000	10.000	.00	0 .0
58.620	.0208					.0218	1.28	8.00	2.01	6.71	.015	.00	.00	BOX
-6923.100	2727.210	6.571	2733.781	1933.00	29.42	13.44	2747.22	.00	8.00	10.00	8.000	10.000	.00	0 .0
124.750	.0208					.0222	2.77	6.57	2.02	6.71	.015	.00	.00	BOX
-6798.350	2729.805	6.517	2736.322	1933.00	29.66	13.66	2749.98	.00	8.00	10.00	8.000	10.000	.00	0 .0
48.360	.0210					.0225	1.09	6.52	2.05	6.68	.015	.00	.00	BOX
-6749.990	2730.821	6.494	2737.315	1933.00	29.77	13.76	2751.07	8.00	8.00	10.00	8.000	10.000	.00	0 .0
10.100	.0207					.0226	.23	8.00	2.06	6.72	.015	.00	.00	BOX
-6739.890	2731.030	6.488	2737.518	1933.00	29.79	13.78	2751.30	.00	8.00	10.00	8.000	10.000	.00	0 .0
130.050	.0208					.0231	3.00	6.49	2.06	6.71	.015	.00	.00	BOX
-6609.840	2733.736	6.400	2740.136	1933.00	30.20	14.17	2754.30	1.25	8.00	10.00	8.000	10.000	.00	0 .0
9.033	.0100					.0236	.21	7.65	2.10	8.00	.015	.00	.00	BOX
-6600.807	2733.826	6.364	2740.190	1933.00	30.37	14.33	2754.52	1.27	8.00	10.00	8.000	10.000	.00	0 .0
73.857	.0100					.0254	1.87	7.63	2.12	8.00	.015	.00	.00	BOX

FILE: MAIN2.WSW

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THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN2-RCB2.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
---------	-------------	------------	------------	---------	-----------	----------	----------------	------------	----------------	----------------	----------------	-----------------	----	----------------

L/Elem	Ch Slope	*****	*****	*****	*****	SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-6526.950	2734.565	6.068	2740.633	1933.00	31.86	15.76	2756.39	.00	8.00	10.00	8.000	10.000	.00	0 .0
JUNCT STR	.0200					.0333	9.85	6.07	2.28		.015	.00	.00	BOX
-6230.910	2740.485	5.194	2745.679	1910.00	36.77	21.00	2766.67	.00	8.00	10.00	8.000	10.000	.00	0 .0
.523	.0959					.0396	.02	5.19	2.84	3.75	.015	.00	.00	BOX
-6230.387	2740.535	5.198	2745.734	1910.00	36.74	20.96	2766.70	.00	8.00	10.00	8.000	10.000	.00	0 .0
28.127	.0959					.0372	1.05	5.20	2.84	3.75	.015	.00	.00	BOX
-6202.259	2743.233	5.452	2748.685	1910.00	35.03	19.06	2767.74	.00	8.00	10.00	8.000	10.000	.00	0 .0
23.230	.0959					.0328	.76	5.45	2.64	3.75	.015	.00	.00	BOX
-6179.029	2745.461	5.718	2751.179	1910.00	33.40	17.32	2768.50	.00	8.00	10.00	8.000	10.000	.00	0 .0
19.349	.0959					.0289	.56	5.72	2.46	3.75	.015	.00	.00	BOX
-6159.681	2747.316	5.997	2753.313	1910.00	31.85	15.75	2769.06	.00	8.00	10.00	8.000	10.000	.00	0 .0
16.190	.0959					.0255	.41	6.00	2.29	3.75	.015	.00	.00	BOX
-6143.490	2748.869	6.290	2755.159	1910.00	30.37	14.32	2769.48	8.00	8.00	10.00	8.000	10.000	.00	0 .0
.647	.0959					.0239	.02	8.00	2.13	3.75	.015	.00	.00	BOX
-6142.842	2748.931	6.303	2755.234	1910.00	30.30	14.26	2769.49	8.00	8.00	10.00	8.000	10.000	.00	0 .0
13.462	.0959					.0225	.30	8.00	2.13	3.75	.015	.00	.00	BOX
-6129.380	2750.222	6.611	2756.833	1910.00	28.89	12.96	2769.79	8.00	8.00	10.00	8.000	10.000	.00	0 .0
11.255	.0959					.0199	.22	8.00	1.98	3.75	.015	.00	.00	BOX

* FILE: MAIN2.WSW
 W S P G W - CIVILDESIGN Version 14.08
 Program Package Serial Number: 7044
 WATER SURFACE PROFILE LISTING
 Date: 3- 2-2016 Time: 6:22:33
 PAGE 4

THE SEVENTY
 GCW INC. PROJECT# 840.050
 FILENAME: MAIN2-RCB2.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
-6118.125	2751.301	6.933	2758.235	1910.00	27.55	11.78	2770.02	8.00	8.00	10.00	8.000	10.000	.00	0 .0
9.358	.0959					.0176	.16	8.00	1.84	3.75	.015	.00	.00	BOX
-6108.767	2752.199	7.272	2759.470	1910.00	26.27	10.71	2770.18	8.00	8.00	10.00	8.000	10.000	.00	0 .0
7.706	.0959					.0156	.12	8.00	1.72	3.75	.015	.00	.00	BOX
----- WARNING - Flow depth near top of box conduit -----														
-6101.061	2752.938	7.627	2760.564	1910.00	25.04	9.74	2770.30	8.00	8.00	10.00	8.000	10.000	.00	0 .0
6.250	.0959					.0173	.11	8.00	1.60	3.75	.015	.00	.00	BOX
----- WARNING - Flow depth near top of box conduit -----														
-6094.810	2753.537	8.000	2761.537	1910.00	23.88	8.85	2770.39	.00	8.00	10.00	8.000	10.000	.00	0 .0
TRANS STR	.0959					.0025	.03	8.00	1.49		.015	.00	.00	BOX
-6083.240	2754.647	15.899	2770.546	1910.00	10.61	1.75	2772.29	.00	6.57	20.00	9.000	20.000	.00	0 .0
30.990	.0959					.0025	.08	.00	.62	2.14	.015	.00	.00	BOX
-6052.250	2757.619	13.190	2770.809	1910.00	10.61	1.75	2772.56	.00	6.57	20.00	9.000	20.000	.00	0 .0
18.230	.0961					.0025	.05	.00	.62	2.13	.015	.00	.00	BOX
-6034.020	2759.370	11.723	2771.094	1910.00	10.61	1.75	2772.84	.00	6.57	20.00	9.000	20.000	.00	0 .0

WSPGW ANALYSIS

MAINLINE 2 LATERALS

MAIN2-RCP6.WSW

T1	THE TWO FIFTY			
T2	GCW INC. PROJECT# 840.050			
T3	FILENAME: MAIN-RCP6.WSW SHT			
SO	-6230.9302741.000 48	2748.635		
R	-6157.6002742.480 48		-48.500	.000 1
R	-5802.5302764.240 48		0.000	.000 0
SH	-5802.5302764.240 48	.000		
CD	18 4		1.500	
CD	24 4		2.000	
CD	30 4		2.500	
CD	36 4		3.000	
CD	42 4		3.500	
CD	48 4		4.000	
CD	54 4		4.500	
CD	60 4		5.000	
CD	72 4		6.000	
Q	54.000 .0			

THE TWO FIFTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN-RCP6.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-6230.930	2741.000	7.635	2748.635	54.00	4.30	.29	2748.92	.00	2.21	.00	4.000	.000	.00	0 .0
73.330	.0202					.0014	.10	.00	.00	1.40	.013	.00	.00	PIPE
-6157.600	2742.480	6.315	2748.795	54.00	4.30	.29	2749.08	.00	2.21	.00	4.000	.000	.00	0 .0
34.604	.0613					.0014	.05	6.32	.00	1.05	.013	.00	.00	PIPE
-6122.996	2744.601	4.243	2748.844	54.00	4.30	.29	2749.13	.00	2.21	.00	4.000	.000	.00	0 .0
HYDRAULIC JUMP														
-6122.996	2744.601	1.054	2745.654	54.00	20.43	6.48	2752.13	.00	2.21	3.52	4.000	.000	.00	0 .0
5.583	.0613					.0613	.34	1.05	4.16	1.05	.013	.00	.00	PIPE
-6117.414	2744.943	1.054	2745.996	54.00	20.43	6.48	2752.47	.00	2.21	3.52	4.000	.000	.00	0 .0
143.660	.0613					.0583	8.38	1.05	4.16	1.05	.013	.00	.00	PIPE
-5973.753	2753.747	1.081	2754.828	54.00	19.69	6.02	2760.85	.00	2.21	3.55	4.000	.000	.00	0 .0
54.188	.0613					.0519	2.81	1.08	3.95	1.05	.013	.00	.00	PIPE
-5919.565	2757.068	1.118	2758.186	54.00	18.78	5.48	2763.66	.00	2.21	3.59	4.000	.000	.00	0 .0
28.844	.0613					.0454	1.31	1.12	3.70	1.05	.013	.00	.00	PIPE
-5890.721	2758.835	1.157	2759.992	54.00	17.90	4.98	2764.97	.00	2.21	3.63	4.000	.000	.00	0 .0
19.126	.0613					.0397	.76	1.16	3.46	1.05	.013	.00	.00	PIPE
-5871.595	2760.007	1.197	2761.204	54.00	17.07	4.53	2765.73	.00	2.21	3.66	4.000	.000	.00	0 .0
13.930	.0613					.0348	.48	1.20	3.24	1.05	.013	.00	.00	PIPE

THE TWO FIFTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN-RCP6.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-5857.665	2760.861	1.239	2762.100	54.00	16.28	4.11	2766.21	.00	2.21	3.70	4.000	.000	.00	0 .0
10.701	.0613					.0304	.33	1.24	3.03	1.05	.013	.00	.00	PIPE
-5846.964	2761.517	1.283	2762.800	54.00	15.52	3.74	2766.54	.00	2.21	3.73	4.000	.000	.00	0 .0
8.522	.0613					.0267	.23	1.28	2.83	1.05	.013	.00	.00	PIPE
-5838.441	2762.039	1.328	2763.367	54.00	14.80	3.40	2766.77	.00	2.21	3.77	4.000	.000	.00	0 .0
6.911	.0613					.0234	.16	1.33	2.65	1.05	.013	.00	.00	PIPE
-5831.530	2762.463	1.375	2763.838	54.00	14.11	3.09	2766.93	.00	2.21	3.80	4.000	.000	.00	0 .0
5.685	.0613					.0205	.12	1.38	2.48	1.05	.013	.00	.00	PIPE
-5825.846	2762.811	1.424	2764.235	54.00	13.45	2.81	2767.04	.00	2.21	3.83	4.000	.000	.00	0 .0
4.718	.0613					.0180	.08	1.42	2.32	1.05	.013	.00	.00	PIPE
-5821.128	2763.100	1.475	2764.575	54.00	12.83	2.55	2767.13	.00	2.21	3.86	4.000	.000	.00	0 .0
3.935	.0613					.0157	.06	1.48	2.16	1.05	.013	.00	.00	PIPE
-5817.193	2763.341	1.528	2764.869	54.00	12.23	2.32	2767.19	.00	2.21	3.89	4.000	.000	.00	0 .0
3.267	.0613					.0138	.05	1.53	2.02	1.05	.013	.00	.00	PIPE
-5813.926	2763.542	1.584	2765.125	54.00	11.66	2.11	2767.24	.00	2.21	3.91	4.000	.000	.00	0 .0
2.744	.0613					.0121	.03	1.58	1.89	1.05	.013	.00	.00	PIPE
-5811.182	2763.710	1.641	2765.351	54.00	11.12	1.92	2767.27	.00	2.21	3.94	4.000	.000	.00	0 .0
2.260	.0613					.0106	.02	1.64	1.76	1.05	.013	.00	.00	PIPE

MAIN2_FAC16C.WSW

T1	THE SEVENTY				
T2	GCW INC. PROJECT# 840.050				
T3	FILENAME: MAIN2_FAC16C.WSW SHT				
SO	-6220.9102741.560	48	2745.679		
R	-6157.5802745.110	48		-48.500	.000 1
R	-5802.5102764.240	48		0.000	.000 0
SH	-5802.5102764.240	48	.000		
CD	18	4		1.500	
CD	24	4		2.000	
CD	30	4		2.500	
CD	36	4		3.000	
CD	42	4		3.500	
CD	48	4		4.000	
CD	54	4		4.500	
CD	60	4		5.000	
CD	72	4		6.000	
Q	54.000	.0			

Date: 3- 3-2016 Time:10: 1:21

THE SEVENTY
 GCW INC. PROJECT# 840.050
 FILENAME: MAIN2_FAC16C.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-Ft	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-6220.910	2741.560	1.082	2742.642	54.00	19.67	6.01	2748.65	.57	2.21	3.55	4.000	.000	.00	0 .0
63.330	.0561					.0545	3.45	1.65	3.95	1.08	.013	.00	.00	PIPE
-6157.581	2745.110	1.089	2746.198	54.00	19.51	5.91	2752.11	.00	2.21	3.56	4.000	.000	.00	0 .0
37.031	.0539					.0539	2.00	1.09	3.90	1.09	.013	.00	.00	PIPE
-6120.550	2747.105	1.089	2748.194	54.00	19.51	5.91	2754.10	.00	2.21	3.56	4.000	.000	.00	0 .0
147.574	.0539					.0511	7.55	1.09	3.90	1.09	.013	.00	.00	PIPE
-5972.976	2755.056	1.118	2756.174	54.00	18.78	5.48	2761.65	.00	2.21	3.59	4.000	.000	.00	0 .0
53.987	.0539					.0454	2.45	1.12	3.70	1.09	.013	.00	.00	PIPE
-5918.988	2757.964	1.157	2759.121	54.00	17.90	4.98	2764.10	.00	2.21	3.63	4.000	.000	.00	0 .0
29.132	.0539					.0397	1.16	1.16	3.46	1.09	.013	.00	.00	PIPE
-5889.856	2759.534	1.197	2760.731	54.00	17.07	4.53	2765.26	.00	2.21	3.66	4.000	.000	.00	0 .0
19.329	.0539					.0348	.67	1.20	3.24	1.09	.013	.00	.00	PIPE
-5870.527	2760.575	1.239	2761.814	54.00	16.28	4.11	2765.93	.00	2.21	3.70	4.000	.000	.00	0 .0
14.085	.0539					.0304	.43	1.24	3.03	1.09	.013	.00	.00	PIPE
-5856.442	2761.334	1.283	2762.617	54.00	15.52	3.74	2766.36	.00	2.21	3.73	4.000	.000	.00	0 .0
10.843	.0539					.0267	.29	1.28	2.83	1.09	.013	.00	.00	PIPE
-5845.599	2761.918	1.328	2763.247	54.00	14.80	3.40	2766.65	.00	2.21	3.77	4.000	.000	.00	0 .0
8.589	.0539					.0234	.20	1.33	2.65	1.09	.013	.00	.00	PIPE

Date: 3- 3-2016 Time:10: 1:21

THE SEVENTY
 GCW INC. PROJECT# 840.050
 FILENAME: MAIN2_FAC16C.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-Ft	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-5837.010	2762.381	1.375	2763.756	54.00	14.11	3.09	2766.85	.00	2.21	3.80	4.000	.000	.00	0 .0
6.945	.0539					.0205	.14	1.38	2.48	1.09	.013	.00	.00	PIPE
-5830.064	2762.755	1.424	2764.179	54.00	13.45	2.81	2766.99	.00	2.21	3.83	4.000	.000	.00	0 .0
5.690	.0539					.0180	.10	1.42	2.32	1.09	.013	.00	.00	PIPE
-5824.374	2763.062	1.475	2764.537	54.00	12.83	2.55	2767.09	.00	2.21	3.86	4.000	.000	.00	0 .0
4.699	.0539					.0157	.07	1.48	2.16	1.09	.013	.00	.00	PIPE
-5819.675	2763.315	1.528	2764.843	54.00	12.23	2.32	2767.17	.00	2.21	3.89	4.000	.000	.00	0 .0
3.871	.0539					.0138	.05	1.53	2.02	1.09	.013	.00	.00	PIPE
-5815.804	2763.524	1.584	2765.108	54.00	11.66	2.11	2767.22	.00	2.21	3.91	4.000	.000	.00	0 .0
3.231	.0539					.0121	.04	1.58	1.89	1.09	.013	.00	.00	PIPE
-5812.573	2763.698	1.641	2765.339	54.00	11.12	1.92	2767.26	.00	2.21	3.94	4.000	.000	.00	0 .0
2.647	.0539					.0106	.03	1.64	1.76	1.09	.013	.00	.00	PIPE
-5809.925	2763.840	1.701	2765.542	54.00	10.60	1.74	2767.29	.00	2.21	3.96	4.000	.000	.00	0 .0
2.147	.0539					.0093	.02	1.70	1.65	1.09	.013	.00	.00	PIPE
-5807.778	2763.956	1.764	2765.720	54.00	10.11	1.59	2767.31	.00	2.21	3.97	4.000	.000	.00	0 .0
1.734	.0539					.0082	.01	1.76	1.54	1.09	.013	.00	.00	PIPE
-5806.044	2764.050	1.829	2765.879	54.00	9.64	1.44	2767.32	.00	2.21	3.99	4.000	.000	.00	0 .0
1.331	.0539					.0072	.01	1.83	1.43	1.09	.013	.00	.00	PIPE

Date: 3- 3-2016 Time:10: 1:21

THE SEVENTY
 GCW INC. PROJECT# 840.050
 FILENAME: MAIN2_FAC16C.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-Ft	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-5804.714	2764.121	1.898	2766.020	54.00	9.19	1.31	2767.33	.00	2.21	3.99	4.000	.000	.00	0 .0
.992	.0539					.0064	.01	1.90	1.33	1.09	.013	.00	.00	PIPE

MAIN2_FAC16C.OUT

-5803.722	2764.175	1.970	2766.145	54.00	8.76	1.19	2767.34	.00	2.21	4.00	4.000	.000	.00	0	.0
.690	.0539	-	-	-	-	.0056	.00	1.97	1.24	1.09	.013	.00	.00	PIPE	
-5803.031	2764.212	2.045	2766.257	54.00	8.35	1.08	2767.34	.00	2.21	4.00	4.000	.000	.00	0	.0
.398	.0539	-	-	-	-	.0049	.00	2.05	1.16	1.09	.013	.00	.00	PIPE	
-5802.633	2764.233	2.124	2766.357	54.00	7.96	.98	2767.34	.00	2.21	3.99	4.000	.000	.00	0	.0
.124	.0539	-	-	-	-	.0043	.00	2.12	1.08	1.09	.013	.00	.00	PIPE	
-5802.510	2764.240	2.209	2766.448	54.00	7.59	.89	2767.34	.00	2.21	3.98	4.000	.000	.00	0	.0
-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	

8

MAIN2_FAC17.WSW

T1	THE SEVENTY			
T2	GCW INC. PROJECT# 840.050			
T3	FILENAME: MAIN1_FAC17.WSW			
SO	-6739.9902733.420	42	2737.518	
R	-6682.9002744.240	42		.013
SH	-6682.9002744.240	42	.000	.000
CD	18	4	1.500	
CD	24	4	2.000	
CD	30	4	2.500	
CD	36	4	3.000	
CD	42	4	3.500	
CD	48	4	4.000	
CD	54	4	4.500	
CD	60	4	5.000	
CD	72	4	6.000	
Q	51.000	.0		

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC17.WSW

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
-6739.990	2733.420	.930	2734.350	51.00	24.89	9.62	2743.97	.00	2.23	3.09	3.500	.000	.00	0 .0
1.454	.1895	-	-	-	-	.1067	.16	.93	5.39	.81	.013	.00	.00	PIPE
-6738.536	2733.696	.934	2734.630	51.00	24.72	9.49	2744.12	.00	2.23	3.10	3.500	.000	.00	0 .0
9.182	.1895	-	-	-	-	.0990	.91	.93	5.34	.81	.013	.00	.00	PIPE
-6729.354	2735.436	.966	2736.402	51.00	23.57	8.63	2745.03	.00	2.23	3.13	3.500	.000	.00	0 .0
7.295	.1895	-	-	-	-	.0867	.63	.97	5.00	.81	.013	.00	.00	PIPE
-6722.059	2736.818	1.000	2737.818	51.00	22.48	7.84	2745.66	.00	2.23	3.16	3.500	.000	.00	0 .0
5.966	.1895	-	-	-	-	.0759	.45	1.00	4.68	.81	.013	.00	.00	PIPE
-6716.093	2737.949	1.035	2738.984	51.00	21.43	7.13	2746.12	.00	2.23	3.19	3.500	.000	.00	0 .0
4.973	.1895	-	-	-	-	.0664	.33	1.04	4.38	.81	.013	.00	.00	PIPE
-6711.120	2738.892	1.071	2739.963	51.00	20.43	6.48	2746.45	.00	2.23	3.23	3.500	.000	.00	0 .0
4.204	.1895	-	-	-	-	.0581	.24	1.07	4.09	.81	.013	.00	.00	PIPE
-6706.917	2739.688	1.108	2740.796	51.00	19.48	5.89	2746.69	.00	2.23	3.26	3.500	.000	.00	0 .0
3.583	.1895	-	-	-	-	.0509	.18	1.11	3.83	.81	.013	.00	.00	PIPE
-6703.333	2740.367	1.147	2741.515	51.00	18.58	5.36	2746.87	.00	2.23	3.29	3.500	.000	.00	0 .0
3.078	.1895	-	-	-	-	.0446	.14	1.15	3.58	.81	.013	.00	.00	PIPE
-6700.255	2740.951	1.188	2742.139	51.00	17.71	4.87	2747.01	.00	2.23	3.31	3.500	.000	.00	0 .0
2.664	.1895	-	-	-	-	.0391	.10	1.19	3.35	.81	.013	.00	.00	PIPE

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC17.WSW

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
-6697.591	2741.456	1.230	2742.686	51.00	16.89	4.43	2747.11	.00	2.23	3.34	3.500	.000	.00	0 .0
2.309	.1895	-	-	-	-	.0343	.08	1.23	3.13	.81	.013	.00	.00	PIPE
-6695.282	2741.893	1.274	2743.167	51.00	16.10	4.03	2747.19	.00	2.23	3.37	3.500	.000	.00	0 .0
2.006	.1895	-	-	-	-	.0300	.06	1.27	2.93	.81	.013	.00	.00	PIPE
-6693.276	2742.273	1.320	2743.594	51.00	15.35	3.66	2747.25	.00	2.23	3.39	3.500	.000	.00	0 .0
1.745	.1895	-	-	-	-	.0264	.05	1.32	2.73	.81	.013	.00	.00	PIPE
-6691.532	2742.604	1.368	2743.972	51.00	14.64	3.33	2747.30	.00	2.23	3.42	3.500	.000	.00	0 .0
1.523	.1895	-	-	-	-	.0231	.04	1.37	2.55	.81	.013	.00	.00	PIPE
-6690.009	2742.893	1.417	2744.310	51.00	13.96	3.02	2747.33	.00	2.23	3.44	3.500	.000	.00	0 .0
1.317	.1895	-	-	-	-	.0203	.03	1.42	2.38	.81	.013	.00	.00	PIPE
-6688.691	2743.142	1.469	2744.611	51.00	13.31	2.75	2747.36	.00	2.23	3.45	3.500	.000	.00	0 .0
1.141	.1895	-	-	-	-	.0178	.02	1.47	2.23	.81	.013	.00	.00	PIPE
-6687.550	2743.359	1.523	2744.882	51.00	12.69	2.50	2747.38	.00	2.23	3.47	3.500	.000	.00	0 .0
.985	.1895	-	-	-	-	.0157	.02	1.52	2.08	.81	.013	.00	.00	PIPE
-6686.565	2743.545	1.579	2745.124	51.00	12.10	2.27	2747.40	.00	2.23	3.48	3.500	.000	.00	0 .0
.839	.1895	-	-	-	-	.0138	.01	1.58	1.94	.81	.013	.00	.00	PIPE
-6685.726	2743.704	1.638	2745.343	51.00	11.53	2.07	2747.41	.00	2.23	3.49	3.500	.000	.00	0 .0
.709	.1895	-	-	-	-	.0121	.01	1.64	1.81	.81	.013	.00	.00	PIPE

THE SEVENTY
GCW INC. PROJECT# 840.050
FILENAME: MAIN1_FAC17.WSW

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
-6685.017	2743.839	1.700	2745.539	51.00	11.00	1.88	2747.42	.00	2.23	3.50	3.500	.000	.00	0 .0
.591	.1895	-	-	-	-	.0107	.01	1.70	1.68	.81	.013	.00	.00	PIPE

MAIN2_FAC17.OUT															
-6684.426	2743.951	1.765	2745.716	51.00	10.49	1.71	2747.42	.00	2.23	3.50	3.500	.000	.00	0	.0
.484	.1895	-	-	-	-	.0094	.00	1.77	1.57	.81	.013	.00	.00	PIPE	
-6683.942	2744.042	1.833	2745.875	51.00	10.00	1.55	2747.43	.00	2.23	3.50	3.500	.000	.00	0	.0
.387	.1895	-	-	-	-	.0083	.00	1.83	1.46	.81	.013	.00	.00	PIPE	
-6683.556	2744.116	1.904	2746.020	51.00	9.53	1.41	2747.43	.00	2.23	3.49	3.500	.000	.00	0	.0
.292	.1895	-	-	-	-	.0073	.00	1.90	1.36	.81	.013	.00	.00	PIPE	
-6683.263	2744.171	1.979	2746.150	51.00	9.09	1.28	2747.43	.00	2.23	3.47	3.500	.000	.00	0	.0
.206	.1895	-	-	-	-	.0064	.00	1.98	1.26	.81	.013	.00	.00	PIPE	
-6683.058	2744.210	2.058	2746.268	51.00	8.67	1.17	2747.43	.00	2.23	3.45	3.500	.000	.00	0	.0
.120	.1895	-	-	-	-	.0057	.00	2.06	1.17	.81	.013	.00	.00	PIPE	
-6682.938	2744.233	2.142	2746.375	51.00	8.26	1.06	2747.43	.00	2.23	3.41	3.500	.000	.00	0	.0
.038	.1895	-	-	-	-	.0050	.00	2.14	1.08	.81	.013	.00	.00	PIPE	
-6682.900	2744.240	2.232	2746.472	51.00	7.87	.96	2747.44	.00	2.23	3.36	3.500	.000	.00	0	.0
-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	

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MAIN2_FAC19.WSW

T1	THE SEVENTY				
T2	GCW INC. PROJECT# 840.050				
T3	FILENAME: MAIN2_FAC19.WSW SHT				
SO	-7049.3802726.520	18	2731.195		
R	-7032.6802728.880	18		60.000	.000 1
R	-7003.6802736.320	18		30.000	.000 0
SH	-7003.6802736.320	18	.000		
CD	18	4		1.500	
CD	24	4		2.000	
CD	30	4		2.500	
CD	36	4		3.000	
CD	42	4		3.500	
CD	48	4		4.000	
CD	54	4		4.500	
CD	60	4		5.000	
CD	72	4		6.000	
Q			2.000	.0	

THE SEVENTY
 GCW INC. PROJECT# 840.050
 FILENAME: MAIN2_FAC19.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-7049.380	2726.520	4.675	2731.195	2.00	1.13	.02	2731.21	.00	.53	.00	1.500	.000	.00	0 .0
16.700	.1413					.0004	.01	.00	.00	.23	.013	.00	.00	PIPE
-7032.680	2728.880	2.325	2731.205	2.00	1.13	.02	2731.23	.00	.53	.00	1.500	.000	.00	0 .0
3.225	.2566					.0004	.00	.00	.00	.20	.013	.00	.00	PIPE
-7029.455	2729.707	1.500	2731.207	2.00	1.13	.02	2731.23	1.50	.53	.00	1.500	.000	.00	0 .0
.534	.2566					.0003	.00	1.50	.00	.20	.013	.00	.00	PIPE
-7028.921	2729.844	1.360	2731.205	2.00	1.19	.02	2731.23	.00	.53	.87	1.500	.000	.00	0 .0
.304	.2566					.0003	.00	1.36	.15	.20	.013	.00	.00	PIPE
-7028.617	2729.922	1.280	2731.202	2.00	1.24	.02	2731.23	.00	.53	1.06	1.500	.000	.00	0 .0
.252	.2566					.0004	.00	1.28	.18	.20	.013	.00	.00	PIPE
-7028.365	2729.987	1.213	2731.200	2.00	1.31	.03	2731.23	.00	.53	1.18	1.500	.000	.00	0 .0
.121	.2566					.0004	.00	1.21	.20	.20	.013	.00	.00	PIPE
-7028.245	2730.018	1.155	2731.173	2.00	1.37	.03	2731.20	.00	.53	1.26	1.500	.000	.00	0 .0
HYDRAULIC JUMP														
-7028.245	2730.018	.200	2730.218	2.00	14.27	3.16	2733.38	.12	.53	1.02	1.500	.000	.00	0 .0
6.129	.2566					.2316	1.42	.32	6.78	.20	.013	.00	.00	PIPE
-7022.115	2731.591	.207	2731.798	2.00	13.53	2.84	2734.64	.11	.53	1.03	1.500	.000	.00	0 .0
4.458	.2566					.2002	.89	.31	6.31	.20	.013	.00	.00	PIPE

THE SEVENTY
 GCW INC. PROJECT# 840.050
 FILENAME: MAIN2_FAC19.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-7017.657	2732.734	.214	2732.948	2.00	12.90	2.58	2735.53	.10	.53	1.05	1.500	.000	.00	0 .0
2.785	.2566					.1748	.49	.31	5.91	.20	.013	.00	.00	PIPE
-7014.872	2733.449	.221	2733.670	2.00	12.30	2.35	2736.02	.09	.53	1.06	1.500	.000	.00	0 .0
1.978	.2566					.1527	.30	.31	5.54	.20	.013	.00	.00	PIPE
-7012.895	2733.956	.229	2734.185	2.00	11.72	2.13	2736.32	.08	.53	1.08	1.500	.000	.00	0 .0
1.518	.2566					.1333	.20	.31	5.20	.20	.013	.00	.00	PIPE
-7011.377	2734.346	.236	2734.582	2.00	11.18	1.94	2736.52	.08	.53	1.09	1.500	.000	.00	0 .0
1.201	.2566					.1163	.14	.31	4.87	.20	.013	.00	.00	PIPE
-7010.176	2734.654	.244	2734.898	2.00	10.66	1.76	2736.66	.07	.53	1.11	1.500	.000	.00	0 .0
.983	.2566					.1016	.10	.31	4.56	.20	.013	.00	.00	PIPE
-7009.193	2734.906	.252	2735.158	2.00	10.16	1.60	2736.76	.06	.53	1.12	1.500	.000	.00	0 .0
.815	.2566					.0887	.07	.32	4.28	.20	.013	.00	.00	PIPE
-7008.378	2735.115	.261	2735.376	2.00	9.69	1.46	2736.83	.06	.53	1.14	1.500	.000	.00	0 .0
.690	.2566					.0776	.05	.32	4.01	.20	.013	.00	.00	PIPE
-7007.688	2735.292	.270	2735.562	2.00	9.24	1.33	2736.89	.06	.53	1.15	1.500	.000	.00	0 .0
.590	.2566					.0678	.04	.33	3.76	.20	.013	.00	.00	PIPE
-7007.098	2735.444	.279	2735.723	2.00	8.81	1.20	2736.93	.05	.53	1.17	1.500	.000	.00	0 .0
.509	.2566					.0592	.03	.33	3.52	.20	.013	.00	.00	PIPE

THE SEVENTY
 GCW INC. PROJECT# 840.050
 FILENAME: MAIN2_FAC19.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-7006.589	2735.574	.288	2735.862	2.00	8.40	1.10	2736.96	.05	.53	1.18	1.500	.000	.00	0 .0
.437	.2566					.0517	.02	.33	3.30	.20	.013	.00	.00	PIPE

MAIN2_FAC19.OUT

-7006.152	2735.686	.298	2735.984	2.00	8.01	1.00	2736.98	.04	.53	1.20	1.500	.000	.00	0	.0
.381	.2566	-	-	-	-	.0452	.02	.34	3.09	.20	.013	.00	.00	PIPE	
-7005.771	2735.784	.308	2736.092	2.00	7.63	.91	2737.00	.04	.53	1.21	1.500	.000	.00	0	.0
.329	.2566	-	-	-	-	.0395	.01	.35	2.89	.20	.013	.00	.00	PIPE	
-7005.442	2735.868	.319	2736.187	2.00	7.28	.82	2737.01	.04	.53	1.23	1.500	.000	.00	0	.0
.292	.2566	-	-	-	-	.0345	.01	.36	2.71	.20	.013	.00	.00	PIPE	
-7005.150	2735.943	.329	2736.272	2.00	6.94	.75	2737.02	.03	.53	1.24	1.500	.000	.00	0	.0
.248	.2566	-	-	-	-	.0302	.01	.36	2.54	.20	.013	.00	.00	PIPE	
-7004.903	2736.007	.341	2736.348	2.00	6.62	.68	2737.03	.03	.53	1.26	1.500	.000	.00	0	.0
.221	.2566	-	-	-	-	.0264	.01	.37	2.38	.20	.013	.00	.00	PIPE	
-7004.682	2736.063	.352	2736.415	2.00	6.31	.62	2737.03	.03	.53	1.27	1.500	.000	.00	0	.0
.189	.2566	-	-	-	-	.0230	.00	.38	2.23	.20	.013	.00	.00	PIPE	
-7004.493	2736.112	.364	2736.476	2.00	6.02	.56	2737.04	.03	.53	1.29	1.500	.000	.00	0	.0
.161	.2566	-	-	-	-	.0202	.00	.39	2.09	.20	.013	.00	.00	PIPE	
-7004.332	2736.153	.377	2736.530	2.00	5.74	.51	2737.04	.02	.53	1.30	1.500	.000	.00	0	.0
.140	.2566	-	-	-	-	.0176	.00	.40	1.95	.20	.013	.00	.00	PIPE	

FILE: MAIN2_FAC19.WSW
 W S P G W - CIVILDESIGN Version 14.08
 Program Package Serial Number: 7044
 WATER SURFACE PROFILE LISTING
 Date: 3- 3-2016 Time:10: 2:58
 THE SEVENTY
 GCW INC. PROJECT# 840.050
 FILENAME: MAIN2_FAC19.WSW SHT
 PAGE 4

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top width	Height/Dia.-FT	Base wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope				SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch	
-7004.191	2736.189	.390	2736.579	2.00	5.47	.46	2737.04	.02	.53	1.32	1.500	.000	.00	0
.121	.2566	-	-	-	.0154	.00	.41	1.83	.20	.013	.00	.00	PIPE	
-7004.070	2736.220	.403	2736.623	2.00	5.21	.42	2737.05	.02	.53	1.33	1.500	.000	.00	0
.100	.2566	-	-	-	.0135	.00	.42	1.71	.20	.013	.00	.00	PIPE	
-7003.970	2736.246	.417	2736.663	2.00	4.97	.38	2737.05	.02	.53	1.34	1.500	.000	.00	0
.081	.2566	-	-	-	.0118	.00	.44	1.60	.20	.013	.00	.00	PIPE	
-7003.889	2736.266	.432	2736.698	2.00	4.74	.35	2737.05	.02	.53	1.36	1.500	.000	.00	0
.068	.2566	-	-	-	.0103	.00	.45	1.50	.20	.013	.00	.00	PIPE	
-7003.821	2736.284	.447	2736.731	2.00	4.52	.32	2737.05	.02	.53	1.37	1.500	.000	.00	0
.052	.2566	-	-	-	.0091	.00	.46	1.40	.20	.013	.00	.00	PIPE	
-7003.770	2736.297	.463	2736.760	2.00	4.31	.29	2737.05	.01	.53	1.39	1.500	.000	.00	0
.041	.2566	-	-	-	.0079	.00	.48	1.31	.20	.013	.00	.00	PIPE	
-7003.729	2736.308	.479	2736.787	2.00	4.11	.26	2737.05	.01	.53	1.40	1.500	.000	.00	0
.027	.2566	-	-	-	.0069	.00	.49	1.23	.20	.013	.00	.00	PIPE	
-7003.701	2736.315	.496	2736.811	2.00	3.92	.24	2737.05	.01	.53	1.41	1.500	.000	.00	0
.019	.2566	-	-	-	.0061	.00	.51	1.15	.20	.013	.00	.00	PIPE	
-7003.683	2736.320	.513	2736.833	2.00	3.74	.22	2737.05	.01	.53	1.42	1.500	.000	.00	0
.002	.2566	-	-	-	.0053	.00	.52	1.07	.20	.013	.00	.00	PIPE	

FILE: MAIN2_FAC19.WSW
 W S P G W - CIVILDESIGN Version 14.08
 Program Package Serial Number: 7044
 WATER SURFACE PROFILE LISTING
 Date: 3- 3-2016 Time:10: 2:58
 THE SEVENTY
 GCW INC. PROJECT# 840.050
 FILENAME: MAIN2_FAC19.WSW SHT
 PAGE 5

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top width	Height/Dia.-FT	Base wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope				SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch	
-7003.680	2736.320	.533	2736.853	2.00	3.55	.20	2737.05	.01	.53	1.44	1.500	.000	.00	0

FILE: MAIN2_FAC19.WSW
 W S P G W - CIVILDESIGN Version 14.08
 Program Package Serial Number: 7044
 WATER SURFACE PROFILE LISTING
 Date: 3- 3-2016 Time:10: 2:58
 THE SEVENTY
 GCW INC. PROJECT# 840.050
 FILENAME: MAIN2_FAC19.WSW SHT
 PAGE 5

MAIN2_FAC21.WSW

T1	THE SEVENTY			
T2	GCW INC. PROJECT# 840.050			
T3	FILENAME: MAIN2_FAC21.WSW SHT			
SO	-7308.6402713.300	18		2718.250
R	-7289.4202713.684	18	.013	0.000 .000 0
SH	-7289.4202713.684	18		.000
CD	18	4	1.500	
CD	24	4	2.000	
CD	30	4	2.500	
CD	36	4	3.000	
CD	42	4	3.500	
CD	48	4	4.000	
CD	54	4	4.500	
CD	60	4	5.000	
CD	72	4	6.000	
Q			2.000 .0	

THE SEVENTY
GCW INC. PROJECT# 840.050

FILENAME: MAIN2_FAC21.WSW SHT

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	vel (FPS)	vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top width	Height/Dia.-FT	Base wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch slope				SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch	
-7308.640	2713.300	4.950	2718.250	2.00	1.13	.02	2718.27	.00	.53	.00	1.500	.000	.00	0 .0
19.220	.0200					.0004	.01	4.95	.00	.37	.013	.00	.00	PIPE
-7289.420	2713.684	4.573	2718.257	2.00	1.13	.02	2718.28	.00	.53	.00	1.500	.000	.00	0 .0

HEC-RAS ANALYSIS

EXISTING CONDITIONS MAIN 1

HEC-RAS Version 4.1.0 Jan 2010
U.S. Army Corps of Engineers
Hydrologic Engineering Center
609 Second Street
Davis, California

```

X      X  XXXXXX   XXXX      XXXX      XX      XXXX
X      X  X        X      X      X  X      X  X      X
X      X  X        X      X      X  X      X  X      X
XXXXXXXX XXXX      X      XXX XXXX      XXXXXX      XXXX
X      X  X        X      X      X  X      X  X      X
X      X  X        X      X      X  X      X  X      X
X      X  XXXXXX   XXXX      X      X      X  X      XXXXX

```

PROJECT DATA

Project Title: Main 1 - Existing Condition
Project File : EXIST3.prj
Run Date and Time: 2/29/2016 11:05:34 AM

Project in English units

PLAN DATA

Plan Title: Main1
Plan File : f:\Projects\800\840-050\Division\Fctl\Calcs\HEC-RAS\01-Main1\EXIST3.p02

Geometry Title: Main1
Geometry File : f:\Projects\800\840-050\Division\Fctl\Calcs\HEC-RAS\01-Main1\EXIST3.G01

Flow Title : Main1
Flow File : f:\Projects\800\840-050\Division\Fctl\Calcs\HEC-RAS\01-Main1\EXIST3.F01

Plan Summary Information:

Number of: Cross Sections =	26	Multiple Openings =	0
Culverts =	0	Inline Structures =	0
Bridges =	0	Lateral Structures =	0

Computational Information

Water surface calculation tolerance =	0.01
Critical depth calculation tolerance =	0.01
Maximum number of iterations =	20
Maximum difference tolerance =	0.3
Flow tolerance factor =	0.001

Computation Options

Critical depth computed at all cross sections
Conveyance Calculation Method: At breaks in n values only
Friction Slope Method: Average Conveyance
Computational Flow Regime: Subcritical Flow

FLOW DATA

Flow Title: Main1
Flow File : f:\Projects\800\840-050\Division\Fctl\Calcs\HEC-RAS\01-Main1\EXIST3.F01

Flow Data (cfs)

River	Reach	RS	PF 1
Unnamed Wash	Main1	2700	2128

Unnamed Wash	Main1	1700	2227
Unnamed Wash	Main1	1500	2472
Unnamed Wash	Main1	800	2493
Unnamed Wash	Main1	500	4209

Boundary Conditions

River	Reach	Profile	Upstream	
Downstream				
Unnamed Wash	Main1	PF 1	Critical	Known WS = 2684.83

GEOMETRY DATA

Geometry Title: Main1

Geometry File : f:\Projects\800\840-050\Division\Fctl\Calcs\HEC-RAS\01-Main1\EXIST3.G01

CROSS SECTION

RIVER: Unnamed Wash

REACH: Main1 RS: 2700

INPUT

Description:

Station Elevation Data				num=	32						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2769	4.32	2768	8.89	2767	14.12	2766	19.18	2765		
24.32	2764	29.44	2763	34.62	2762	39.85	2761	45	2760		
48.3	2759	51.08	2758	54.15	2757	58.29	2756	74.22	2755		
77.45	2757	80.08	2756	90.95	2755	94.1	2754	95.07	2753		
97.37	2758	99.58	2759	100.37	2760	101.18	2761	101.97	2762		
103.09	2763	105.64	2764	108.63	2765	112.52	2766	116.09	2767		
119.56	2768	127.49	2769								

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	127.49	.035

Bank Sta:	Left	Right	Lengths:	Left	Channel	Right	Coeff	Contr.	Expan.
0	127.49		95.75	98.69	107.97		.1	.3	

CROSS SECTION

RIVER: Unnamed Wash

REACH: Main1 RS: 2600

INPUT

Description:

Station Elevation Data				num=	34						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2765	3.19	2764	6.31	2763	9.41	2762	12.03	2761		
12.88	2760	13.83	2759	14.76	2758	15.74	2757	16.76	2756		
17.69	2755	18.58	2754	22.83	2752	32.12	2752	37.82	2754		
43.67	2755	52.8	2756	66.54	2757	66.62	2758	66.71	2759		
68.82	2761	68.85	2761	70.78	2759	71.78	2758	72.75	2757		
86.93	2757	90.38	2758	91.7	2759	92.96	2760	94.15	2761		
99.48	2762	104.49	2763	110.14	2764	115.64	2765				

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	115.64	.035

Bank Sta:	Left	Right	Lengths:	Left	Channel	Right	Coeff	Contr.	Expan.
0	115.64		101.86	103.65	108.71		.1	.3	

CROSS SECTION

RIVER: Unnamed Wash

REACH: Main1

RS: 2500

INPUT

Description:

Station Elevation Data			num= 20						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2761	.38	2760	.75	2759	1.17	2758	1.89	2756
2.3	2755	2.68	2754	3.06	2753	3.44	2752	9.58	2748
17.77	2748	34.89	2752	60.1	2753	67.24	2754	71.71	2755
76.74	2756	84.67	2758	93.68	2759	99.64	2760	104.45	2761

Manning's n Values

num= 3		
Sta	n Val	Sta
0	.035	0
		104.45
		.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	0	104.45		108.74	100.43	96.31	.1 .3

CROSS SECTION

RIVER: Unnamed Wash

REACH: Main1

RS: 2400

INPUT

Description:

Station Elevation Data			num= 23						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2758	15.42	2758	18.34	2757	21.01	2756	23.33	2755
24.99	2754	26.51	2753	29.64	2751	31.2	2750	33.06	2749
35.06	2748	37.36	2747	68.67	2749	90.83	2749	95.4	2751
98.61	2752	104.46	2754	109.02	2755	118.84	2756	121.79	2757
123.77	2758	126.1	2759	128.13	2759				

Manning's n Values

num= 3		
Sta	n Val	Sta
0	.035	0
		128.13
		.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	0	128.13		109.52	114.22	121.17	.1 .3

CROSS SECTION

RIVER: Unnamed Wash

REACH: Main1

RS: 2300

INPUT

Description:

Station Elevation Data			num= 33						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2757	13.08	2756	20.71	2755	24.77	2754	28.47	2753
32.13	2752	33.53	2751	34.62	2750	35.7	2749	36.76	2748
37.76	2747	39.95	2746	42.62	2745	49.66	2744	64.78	2744
70.38	2745	73.02	2746	74.87	2747	76.67	2748	78.26	2749
79.83	2750	83.9	2751	88.3	2752	92.1	2753	95.71	2754
99.67	2755	104.09	2756	108.38	2757	112.21	2758	115.85	2759
119.41	2760	122.82	2761	126.24	2762				

Manning's n Values

num= 3		
Sta	n Val	Sta
0	.035	0
		126.24
		.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	0	126.24		191.53	193.81	198.19	.1 .3

RIVER: Unnamed Wash
REACH: Main1 RS: 2200

Description:

Manning's	n Values		num=	3	
Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	127.18	.035

CROSS SECTION

RIVER: Unnamed Wash
REACH: Main1 RS: 2100

Description:

Manning's	n Values		num=	3	
Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	132.68	.035

CROSS SECTION

RIVER: Unnamed Wash
REACH: Main1 RS: 2000

Description:

Manning's n Values		num=		2
Sta	n Val	Sta	n Val	
0	.035	116.39	.03	

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
-----------	------	-------	----------	--------------	-------	--------------	--------

0 137.36 231.62 197.66 162.89 .1 .3

CROSS SECTION

RIVER: Unnamed Wash

REACH: Main1

RS: 1900

INPUT

Description:

Station Elevation Data

num=

54

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2760	7.86	2759	8.62	2758	9.33	2757	10.1	2756
12.21	2754	14.17	2753	16.04	2752	17.72	2751	19.29	2750
22.45	2748	24.24	2747	26.07	2746	27.89	2745	29.73	2744
31.59	2743	33.35	2742	35.09	2741	37.27	2740	39.81	2739
42.41	2738	43.87	2737	44.98	2736	46.08	2735	46.55	2734
47.14	2733	47.96	2732	49.45	2730	50.64	2729	51.77	2728
52.93	2727	54.04	2726	55.19	2725	56.32	2724	69.55	2724
69.74	2725	69.88	2726	70.03	2727	70.55	2728	72.22	2729
75.51	2729	80.71	2729	83.34	2730	86.02	2731	88.45	2732
90.22	2733	91.95	2734	94.33	2735	96.69	2736	99.84	2737
102.86	2738	105.74	2739	124.05	2740	124.05	2741		

Manning's n Values

num=

2

Sta	n Val	Sta	n Val
0	.035	105.74	.03

Bank Sta: Left Right

0 124.05

Lengths: Left Channel

122.47 101.94

Right

85.19

Coeff Contr.

.1

Expan.

.3

CROSS SECTION

RIVER: Unnamed Wash

REACH: Main1

RS: 1800

INPUT

Description:

Station Elevation Data

num=

53

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2740	3.91	2746	13.58	2747	27.29	2747	40.79	2744
44.66	2743	46.27	2742	47.87	2741	49.53	2740	51.08	2739
54.43	2737	56.3	2736	58.22	2735	60.13	2734	63.04	2732
64.1	2731	64.52	2730	64.99	2729	65.44	2728	66.35	2726
66.79	2725	67.28	2724	67.73	2723	68.2	2722	69.12	2720
75.66	2719	79.29	2721	79.87	2722	80.21	2723	80.48	2724
80.76	2725	81.02	2726	81.44	2727	82.21	2728	83.08	2729
83.9	2730	84.67	2731	86.85	2732	92.81	2732	94.63	2732
100.04	2732	102.44	2731	104.77	2730	115.2	2730	116.94	2731
118.67	2732	120.41	2733	122.2	2734	125.27	2735	129.23	2736
133.96	2737	139.92	2738	148.25	2737				

Manning's n Values

num=

3

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	148.25	.035

Bank Sta: Left Right

0 148.25

Lengths: Left Channel

140.2 137.49

Right

140.54

Coeff Contr.

.1

Expan.

.3

CROSS SECTION

RIVER: Unnamed Wash

REACH: Main1

RS: 1700

INPUT

Description:

Station Elevation Data

num=

37

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2737	1.25	2737	11.94	2735	15.37	2734	18.84	2733

22.36	2732	26.44	2731	32.09	2730	36.2	2729	39.93	2726
40.4	2725	40.83	2724	41.29	2723	42.62	2720	43.08	2719
43.53	2718	43.95	2717	44.26	2716	52.91	2717	52.98	2718
53.05	2719	53.18	2720	53.54	2722	54.25	2723	54.56	2724
54.58	2725	54.7	2726	55.93	2727	57.21	2728	61.3	2729
62.1	2730	62.82	2731	64.63	2731	65.76	2730	72.27	2730
75.99	2731	92.39	2732						

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	92.39	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	0	92.39		145.9	141.68		.1	.3

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1 RS: 1600

INPUT

Description:

Station Elevation Data num= 41

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2730	.84	2730	3.34	2729	5.76	2728	8.34	2727
10.96	2726	13.73	2725	16.56	2724	18.7	2723	19.54	2722
20.05	2721	20.5	2720	20.95	2719	21.4	2718	21.81	2717
22.7	2715	23.18	2714	23.61	2713	24.1	2712	25.18	2711
32.35	2711	32.43	2712	32.46	2713	32.51	2714	32.51	2715
32.55	2716	32.61	2717	32.63	2718	32.73	2719	32.76	2720
32.87	2721	33	2722	33.08	2723	33.17	2724	41.32	2725
47.05	2724	57.68	2725	64.05	2727	72.68	2728	75.19	2729
79.21	2730								

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	79.21	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	0	79.21		132.22	129.11		.1	.3

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1 RS: 1500

INPUT

Description:

Station Elevation Data num= 54

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2739	5.25	2739	10.38	2738	11.16	2737	11.88	2736
12.54	2735	13.99	2733	15.85	2732	19.53	2730	20.91	2729
22.3	2728	25.12	2726	26.47	2725	27.51	2723	27.95	2722
28.38	2721	28.86	2720	29.24	2719	29.73	2718	30.09	2717
30.55	2716	30.96	2715	31.37	2714	31.75	2713	32.14	2712
32.55	2711	32.96	2710	36.88	2707	40.43	2707	40.71	2708
41.04	2709	41.4	2710	41.76	2711	42.06	2712	42.35	2713
42.61	2714	42.89	2715	43.12	2716	44.34	2717	46.18	2718
48.75	2719	51.54	2720	53.99	2721	56.32	2722	58.52	2723
60.88	2724	63.2	2725	65.05	2726	66.91	2727	68.83	2728
70.84	2729	73.94	2730	79.58	2732	81.97	2733		

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	81.97	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	0	81.97		270.26	260.99		.1	.3

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
0 .035 0 .035 100 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
0 100 199.59 208.99 220.51 .1 .3

CROSS SECTION

RIVER: Unnamed Wash
REACH: Main1 RS: 1100

INPUT

Description:

Station Elevation Data			num= 29								
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2707	5.35	2707	8.38	2706	9.68	2705	12.44	2703		
13.93	2702	15.38	2701	17.01	2700	18.58	2699	21.52	2697		
22.94	2696	26.14	2694	29.68	2693	34.53	2692	38.4	2691		
56.38	2691	57.13	2692	57.9	2693	59.43	2695	60.24	2696		
61.29	2697	62.43	2698	63.9	2699	65.12	2700	66.01	2701		
66.45	2702	66.68	2703	66.92	2704	74.91	2705				

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
0 .035 0 .035 74.91 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
0 74.91 173.12 189.13 202.7 .1 .3

CROSS SECTION

RIVER: Unnamed Wash
REACH: Main1 RS: 1000

INPUT

Description:

Station Elevation Data			num= 30								
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2700	1.85	2697	4.99	2695	7.03	2694	9.01	2693		
15.23	2690	17.81	2689	23.14	2688	37.9	2687.36	46.38	2687		
53.45	2687	55.47	2688	56.45	2689	56.76	2690	57.1	2691		
57.5	2692	59.29	2694	60.1	2695	60.84	2696	61.57	2697		
62.25	2698	62.94	2699	67.06	2701	69.55	2702	72.11	2703		
72.82	2704	73.47	2705	75.18	2707	77.09	2708	82.18	2709		

Manning's n Values num= 3
Sta n Val Sta n Val Sta n Val
0 .035 0 .035 82.18 .035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
0 82.18 200.05 199.88 200.05 .1 .3

CROSS SECTION

RIVER: Unnamed Wash
REACH: Main1 RS: 900

INPUT

Description:

Station Elevation Data			num= 29								
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2697	2.01	2696	6.96	2693	8.56	2692	9.68	2691		
10.78	2690	11.92	2689	13	2688	14.12	2687	15.2	2686		
16.3	2685	17.24	2684	26.67	2683	30.04	2683	41.4	2683		
45.22	2684	46.68	2685	47.87	2686	48.94	2687	50.02	2688		
51.05	2689	52.27	2690	53.58	2691	54.05	2692	54.3	2693		

54.53	2694	61.14	2696	68.17	2697	76.52	2697
-------	------	-------	------	-------	------	-------	------

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	76.52	.035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.

	0	76.52		200.06	199.87	200.06		.1	.3
--	---	-------	--	--------	--------	--------	--	----	----

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1 RS: 800

INPUT

Description:

Station Elevation Data				num=	32					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	2695	5.28	2694	9.97	2693	16.15	2691	17.35	2690	
18.64	2689	19.91	2688	21.18	2687	22.6	2686	24.45	2685	
26.51	2684	28.59	2683	29.67	2682	30.77	2681	31.87	2680	
41.31	2679	45.06	2679	53.43	2679	55.64	2680	57.69	2681	
59.22	2682	60.74	2683	62.39	2684	64.07	2685	65.7	2686	
67.32	2687	69.12	2688	70.94	2689	72.73	2690	76.3	2692	
78.37	2693	88.81	2695							

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	88.81	.035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.

	0	88.81		200	199.91	200		.1	.3
--	---	-------	--	-----	--------	-----	--	----	----

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1 RS: 700

INPUT

Description:

Station Elevation Data				num=	32					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	2692	13.46	2690	20.83	2689	24.82	2688	26.72	2687	
27.64	2686	28.5	2685	29.4	2684	30.34	2683	31.24	2682	
32.5	2681	33.91	2680	35.36	2679	36.22	2678	37	2677	
40.67	2676	49.89	2676	60.98	2676	63.89	2677	65.31	2678	
66.7	2679	68.22	2680	70.18	2681	72.05	2682	73.98	2683	
75.51	2684	76.92	2685	78.38	2686	79.79	2687	82.47	2688	
85.76	2689	93.54	2689							

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	93.54	.035

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.

	0	93.54		105.58	90.05	91.05		.1	.3
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CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1 RS: 600

INPUT

Description:

Station Elevation Data				num=	53					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	2691	2.03	2691	4.75	2690	14.29	2689	26.04	2688	
33.69	2687	34.32	2686	34.69	2685	35.04	2684	35.4	2683	

35.71	2682	36.05	2681	36.46	2680	37.14	2679	39.75	2678
42.44	2677	44.85	2676	46.95	2675	49.06	2674	61.8	2674
76.28	2675	80.1	2676	83.77	2677	89.32	2679	91.29	2680
93.62	2681	96.54	2682	98.84	2683	106.09	2683	110.53	2682
112.97	2682	122.92	2682	123.43	2681	124.01	2680	124.46	2679
124.94	2678	125.31	2677	125.68	2676	126.77	2675	128.15	2674
139.97	2675	142.29	2676	144.19	2677	146.82	2678	149.09	2679
151.09	2680	153.17	2681	156.53	2682	159.47	2683	165.89	2685
167.92	2686	170.23	2687	172.74	2688				

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	172.74	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	0	172.74		165.96	163.56		.1	.3

Ineffective Flow num= 1

Sta L	Sta R	Elev	Permanent
106.09	172.74	2690	F

CROSS SECTION

RIVER: Unnamed Wash
REACH: Main1 RS: 500

INPUT

Description:

Station	Elevation	Data	num=	29						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	2687	16.29	2686	33.47	2685	48.37	2684	54.57	2683	
62.81	2681	65.1	2680	67.73	2679	70.01	2678	72.24	2677	
73.94	2676	77.08	2673	90.18	2672.27	94.92	2672	106.5	2672	
113.63	2673	126.37	2676	128.11	2677	129.52	2678	131.24	2679	
134.08	2680	139.43	2681	153.77	2683	159.91	2684	162.55	2685	
164.37	2686	166.37	2687	168.53	2688	187.05	2690			

Manning's n Values num= 2

Sta	n Val	Sta	n Val
0	.03	48.37	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	0	187.05		58.23	51.31		.1	.3

CROSS SECTION

RIVER: Unnamed Wash
REACH: Main1 RS: 400

INPUT

Description:

Station	Elevation	Data	num=	41						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	2688.01	6.8	2685	9.24	2684	16.28	2683	28.94	2683	
32.59	2684	36.71	2685	41.98	2685	55.92	2684	78.44	2684	
97.61	2684	98.46	2683	100.13	2681	100.9	2680	101.76	2679	
102.54	2678	103.66	2677	105.88	2676	108.08	2675	110.35	2674	
112.62	2673	114.93	2672	118.66	2671	154.09	2671	157.32	2672	
159.33	2673	161.13	2674	161.97	2675	162.88	2676	163.89	2677	
164.96	2678	166.09	2679	167.41	2680	171.11	2683	177.76	2683	
204.74	2683	212.73	2684	215.85	2685	218.94	2686	222.3	2687	
235.52	2689									

Manning's n Values num= 2

Sta	n Val	Sta	n Val
0	.03	97.61	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	0	235.52		116.72	99.89		.1	.3

CROSS SECTION

RIVER: Unnamed Wash

REACH: Main1

RS: 300

INPUT

Description:

Station Elevation Data		num= 35		Sta		Elev		Sta		Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2686.85	10.18	2687	26.16	2686	56.92	2685	67.77	2683		
72.93	2682	74.69	2681	75.93	2680	77.09	2679	78.28	2678		
80.13	2677	81.83	2676	83.53	2675	85.1	2674	89.88	2672		
92.95	2671	96.11	2670	99.27	2669	125.7	2669	131	2670		
133.85	2671	140.06	2673	144.25	2674	149.79	2676	153.27	2677		
159.33	2679	162.93	2680	173.51	2681	187.26	2682	195.52	2683		
202	2684	207.73	2685	212.52	2686	216.49	2687	220.29	2688		

Manning's n Values

num= 2

Sta	n Val	Sta	n Val
0	.035	56.92	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	0	220.29		145.1	100.88	52	.1	.3

CROSS SECTION

RIVER: Unnamed Wash

REACH: Main1

RS: 200

INPUT

Description:

Station Elevation Data		num= 49		Sta		Elev		Sta		Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2693	1.64	2692	3.32	2691	5.46	2690	7.61	2689		
9.35	2688	11.06	2687	12.77	2686	14.47	2685	16.25	2684		
18.24	2683	23	2682	25.51	2681	28.74	2680	31.03	2679		
31.44	2678	32.35	2676	33	2675	33.89	2674	34.55	2673		
35.14	2672	35.58	2671	36.12	2670	36.63	2669	37.08	2668		
38.91	2668	40.82	2668	41.23	2669	41.7	2670	42.11	2671		
42.85	2672	43.48	2673	44.25	2674	46.26	2675	49.04	2676		
59.12	2678	63.36	2679	66.9	2680	70.72	2681	82.01	2682		
117.78	2683	123.57	2684	125.81	2685	127.96	2686	130.18	2687		
132.3	2688	134.11	2689	135.75	2690	137.7	2691				

Manning's n Values

num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	137.7	.035

Bank Sta:	Left	Right	Coeff	Contr.	Expan.
	0	137.7		.3	.5

SUMMARY OF MANNING'S N VALUES

River: Unnamed Wash

Reach	River Sta.	n1	n2	n3
Main1	2700	.035	.035	.035
Main1	2600	.035	.035	.035
Main1	2500	.035	.035	.035
Main1	2400	.035	.035	.035
Main1	2300	.035	.035	.035
Main1	2200	.035	.035	.035
Main1	2100	.035	.035	.035
Main1	2000	.035	.03	
Main1	1900	.035	.03	
Main1	1800	.035	.035	.035

Main1	1700	.035	.035	.035
Main1	1600	.035	.035	.035
Main1	1500	.035	.035	.035
Main1	1400	.035	.035	.035
Main1	1300	.035	.035	.035
Main1	1200	.035	.035	.035
Main1	1100	.035	.035	.035
Main1	1000	.035	.035	.035
Main1	900	.035	.035	.035
Main1	800	.035	.035	.035
Main1	700	.035	.035	.035
Main1	600	.035	.035	.035
Main1	500	.03	.035	
Main1	400	.03	.035	
Main1	300	.03	.035	
Main1	200	.035	.035	.035

SUMMARY OF REACH LENGTHS

River: Unnamed Wash

Reach	River Sta.	Left	Channel	Right
Main1	2700	95.75	98.69	107.97
Main1	2600	101.86	103.65	108.71
Main1	2500	108.74	100.43	96.31
Main1	2400	109.52	114.22	121.17
Main1	2300	191.53	193.81	198.19
Main1	2200	113.96	200.13	254.43
Main1	2100	231.94	197.1	162.04
Main1	2000	231.62	197.66	162.89
Main1	1900	122.47	101.94	85.19
Main1	1800	140.2	137.49	140.54
Main1	1700	145.9	141.68	135.05
Main1	1600	132.22	129.11	128.4
Main1	1500	270.26	260.99	251.15
Main1	1400	197.2	199.44	199.87
Main1	1300	170	195.8	223.9
Main1	1200	199.59	208.99	220.51
Main1	1100	173.12	189.13	202.7
Main1	1000	200.05	199.88	200.05
Main1	900	200.06	199.87	200.06
Main1	800	200	199.91	200
Main1	700	105.58	90.05	91.05
Main1	600	165.96	163.56	169.79
Main1	500	58.23	51.31	62.51
Main1	400	116.72	99.89	88.03
Main1	300	145.1	100.88	52
Main1	200			

SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS

River: Unnamed Wash

Reach	River Sta.	Contr.	Expan.
Main1	2700	.1	.3
Main1	2600	.1	.3
Main1	2500	.1	.3
Main1	2400	.1	.3
Main1	2300	.1	.3
Main1	2200	.1	.3
Main1	2100	.1	.3
Main1	2000	.1	.3
Main1	1900	.1	.3

Main1	1800	.1	.3
Main1	1700	.1	.3
Main1	1600	.1	.3
Main1	1500	.1	.3
Main1	1400	.1	.3
Main1	1300	.1	.3
Main1	1200	.1	.3
Main1	1100	.1	.3
Main1	1000	.1	.3
Main1	900	.1	.3
Main1	800	.1	.3
Main1	700	.1	.3
Main1	600	.1	.3
Main1	500	.1	.3
Main1	400	.1	.3
Main1	300	.1	.3
Main1	200	.3	.5

ERRORS WARNINGS AND NOTES

Errors Warnings and Notes for Plan : Main1

River: Unnamed Wash Reach: Main1 RS: 2700 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 2600 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:Divided flow computed for this cross-section.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 2500 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 2400 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 2300 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 2200 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 2100 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 2000 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning:The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 1800 Profile: PF 1

Warning:The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning:The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

River: Unnamed Wash Reach: Main1 RS: 1700 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated

water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The

program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 1600 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.

Warning:The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate

the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated

water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The

program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 1500 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate

the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated

water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The

program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 1400 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.

Warning:The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate

the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated

water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The

program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 1300 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate

the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated

water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The

program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 1200 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate

the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated

water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 1100 Profile: PF 1

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m) between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 1000 Profile: PF 1

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m) between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 900 Profile: PF 1

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m) between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 800 Profile: PF 1

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m) between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1 RS: 700 Profile: PF 1

Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

River: Unnamed Wash Reach: Main1 RS: 600 Profile: PF 1

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

River: Unnamed Wash Reach: Main1 RS: 300 Profile: PF 1

Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

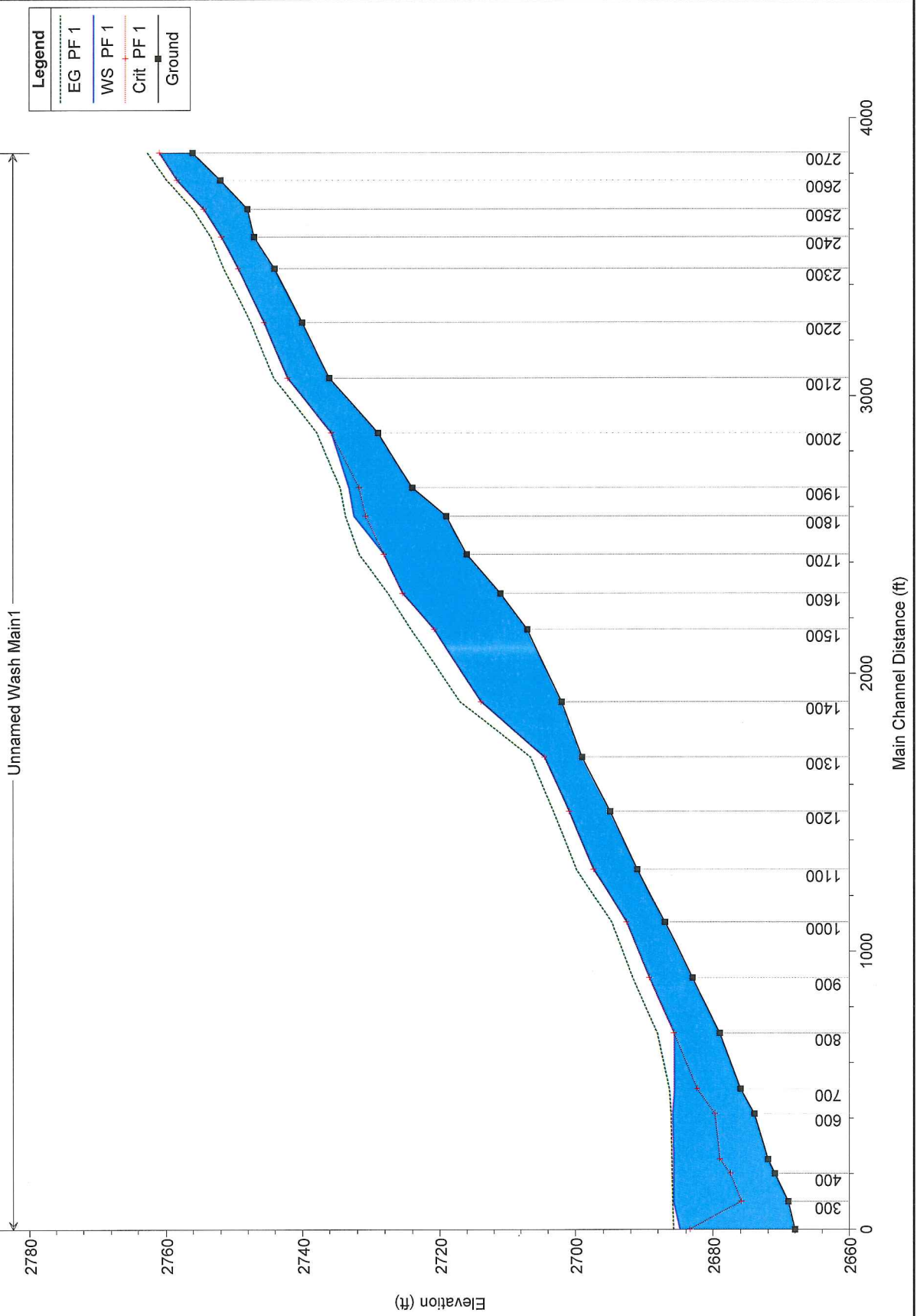
Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

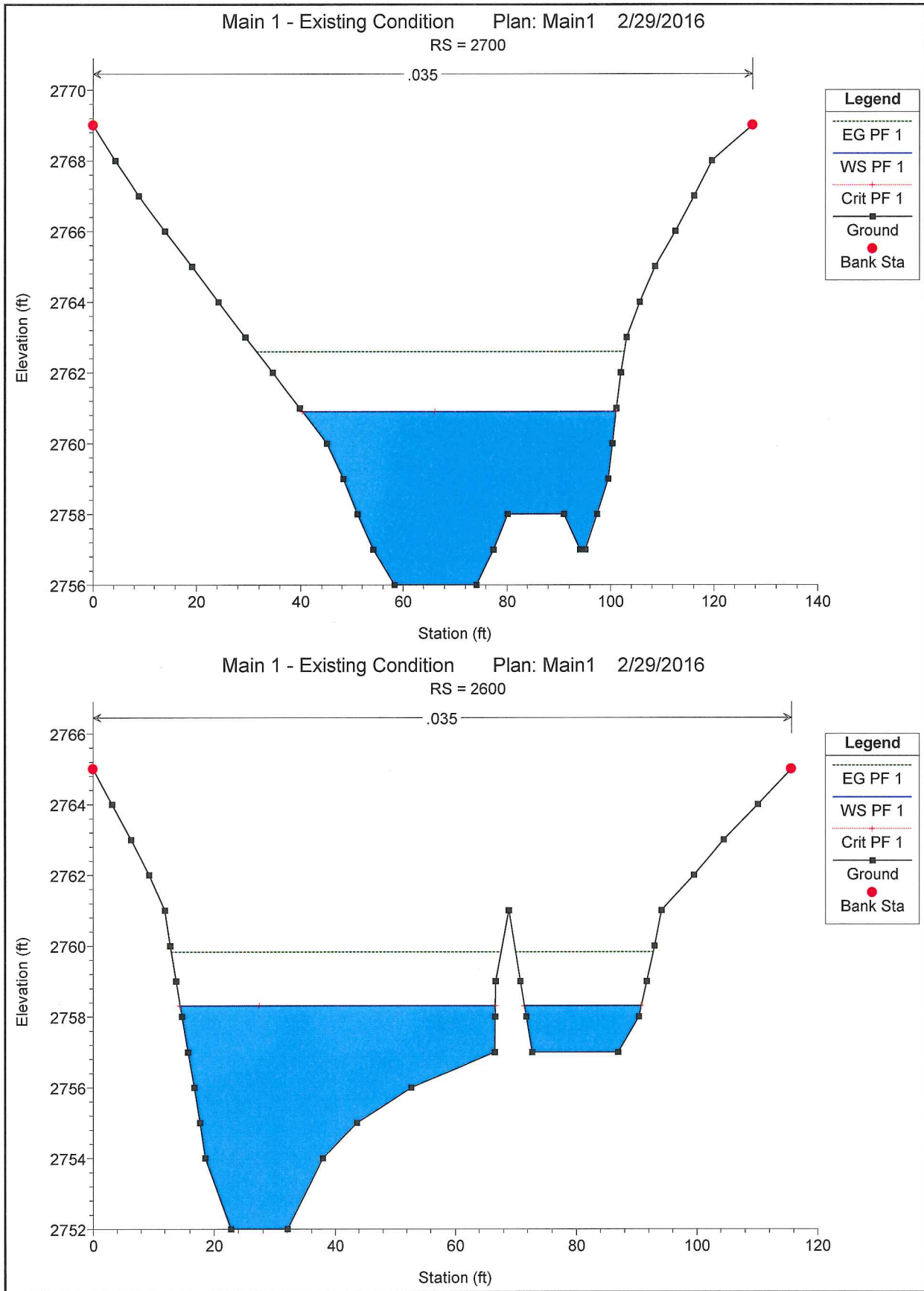
This may indicate the need for additional cross sections.

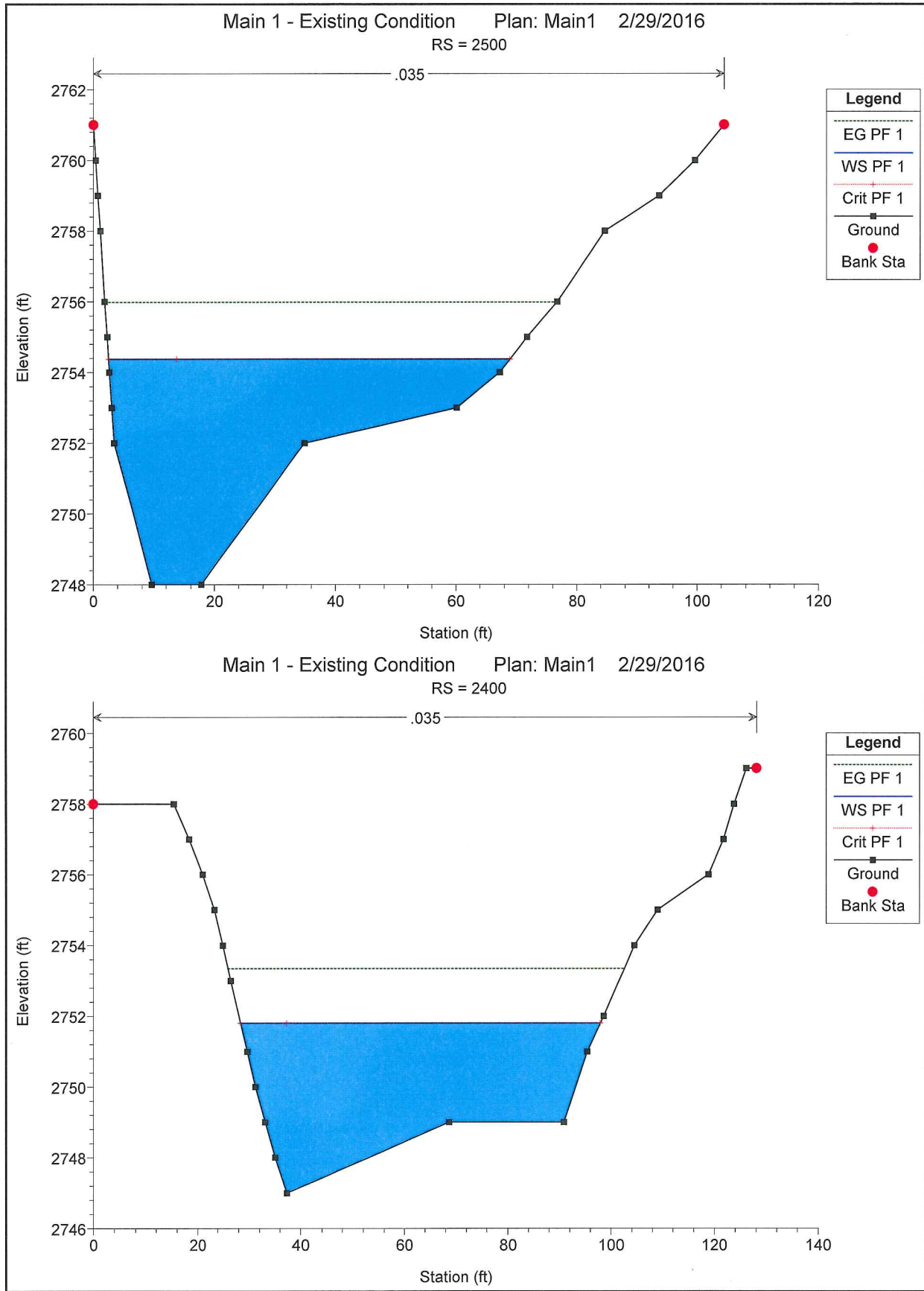
HEC-RAS Plan: Main1 River: Unnamed Wash Reach: Main1 Profile: PF 1

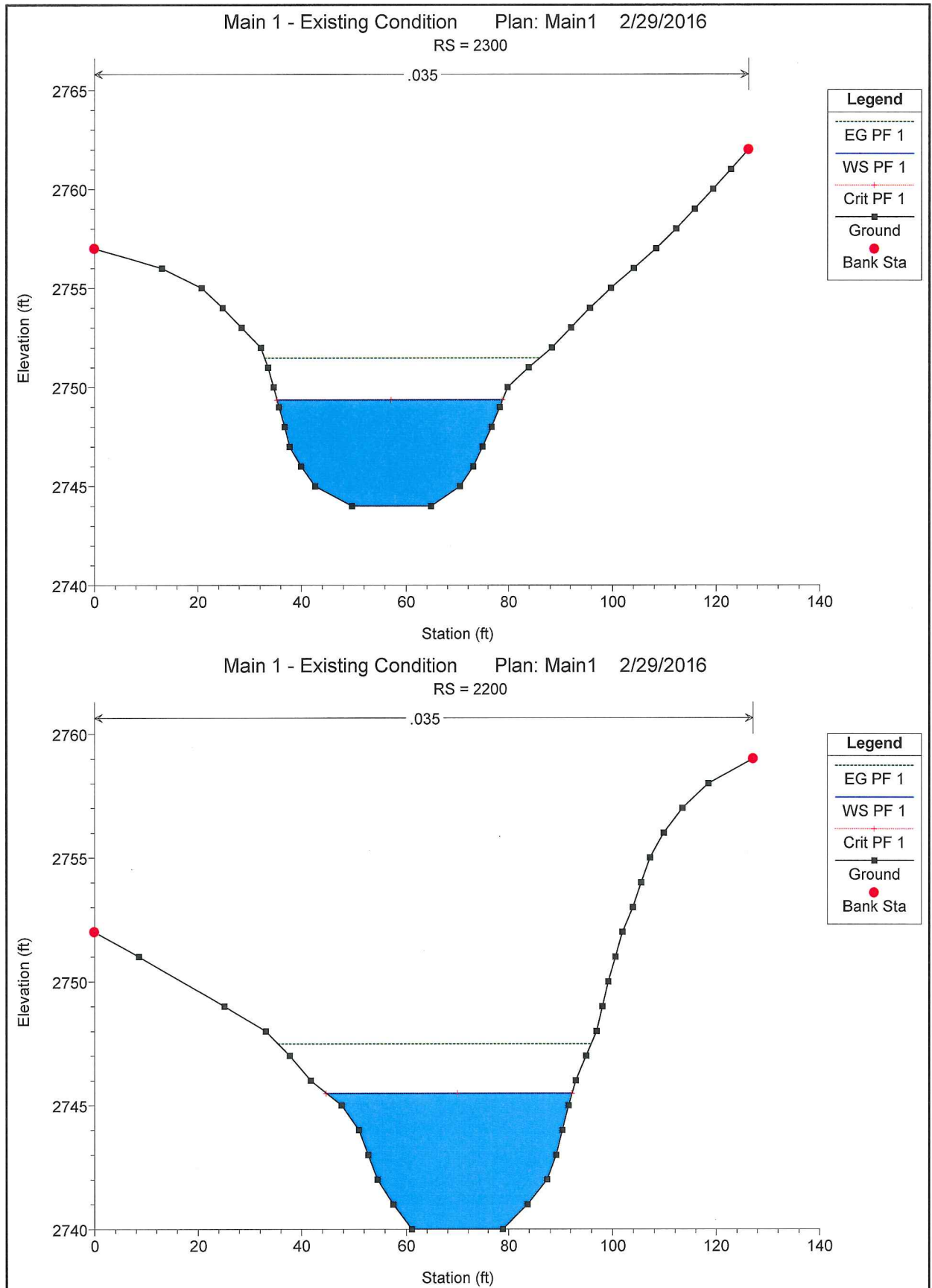
Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Main1	2700	PF 1	2128.00	2756.00	2760.89	2760.89	2762.59	0.012774	10.46	203.44	60.70	1.01
Main1	2600	PF 1	2128.00	2752.00	2758.31	2758.31	2759.83	0.013663	9.90	214.95	71.48	1.01
Main1	2500	PF 1	2128.00	2748.00	2754.37	2754.37	2755.99	0.013412	10.20	208.57	66.36	1.01
Main1	2400	PF 1	2128.00	2747.00	2751.80	2751.80	2753.34	0.012747	9.95	213.77	69.59	1.00
Main1	2300	PF 1	2128.00	2744.00	2749.36	2749.36	2751.48	0.012119	11.68	182.19	43.51	1.01
Main1	2200	PF 1	2128.00	2740.00	2745.49	2745.49	2747.48	0.012174	11.33	187.75	47.51	1.00
Main1	2100	PF 1	2128.00	2736.00	2742.08	2742.08	2744.08	0.012150	11.35	187.55	46.89	1.00
Main1	2000	PF 1	2128.00	2729.00	2735.65	2735.65	2737.77	0.012614	11.69	181.96	43.15	1.00
Main1	1900	PF 1	2128.00	2724.00	2733.14	2731.64	2734.38	0.005770	8.94	237.92	43.40	0.67
Main1	1800	PF 1	2128.00	2719.00	2732.45	2730.71	2733.66	0.008664	8.80	241.76	57.08	0.75
Main1	1700	PF 1	2227.00	2716.00	2728.08	2728.08	2731.68	0.019678	15.22	146.31	20.20	1.00
Main1	1600	PF 1	2227.00	2711.00	2725.34	2725.34	2727.46	0.018419	11.67	190.81	45.98	1.01
Main1	1500	PF 1	2472.00	2707.00	2720.77	2720.77	2724.15	0.018525	14.77	167.39	24.93	1.00
Main1	1400	PF 1	2472.00	2702.00	2713.84	2713.84	2716.92	0.016275	14.09	175.47	28.74	1.00
Main1	1300	PF 1	2472.00	2699.00	2704.43	2704.43	2706.46	0.012057	11.42	216.42	53.98	1.01
Main1	1200	PF 1	2472.00	2695.00	2700.84	2700.84	2703.15	0.012205	12.19	202.78	44.49	1.01
Main1	1100	PF 1	2472.00	2691.00	2697.30	2697.30	2699.76	0.012233	12.57	196.64	40.56	1.01
Main1	1000	PF 1	2472.00	2687.00	2692.52	2692.52	2694.72	0.012304	11.89	207.98	47.97	1.01
Main1	900	PF 1	2472.00	2683.00	2689.15	2689.15	2691.63	0.011974	12.63	195.65	39.48	1.00
Main1	800	PF 1	2493.00	2679.00	2685.65	2685.65	2688.05	0.011853	12.43	200.60	41.88	1.00
Main1	700	PF 1	2493.00	2676.00	2685.62	2682.23	2686.39	0.002350	7.03	354.61	49.85	0.46
Main1	600	PF 1	2493.00	2674.00	2685.89	2679.63	2686.14	0.000568	4.01	621.90	133.33	0.24
Main1	500	PF 1	4209.00	2672.00	2685.74	2678.92	2686.03	0.000687	4.33	971.83	143.10	0.29
Main1	400	PF 1	4209.00	2671.00	2685.77	2677.39	2685.97	0.000532	3.56	1181.20	213.18	0.27
Main1	300	PF 1	4209.00	2669.00	2685.77	2675.79	2685.92	0.000296	3.04	1382.45	178.22	0.19
Main1	200	PF 1	4209.00	2668.00	2684.83	2683.29	2685.76	0.004590	7.74	543.77	110.66	0.62

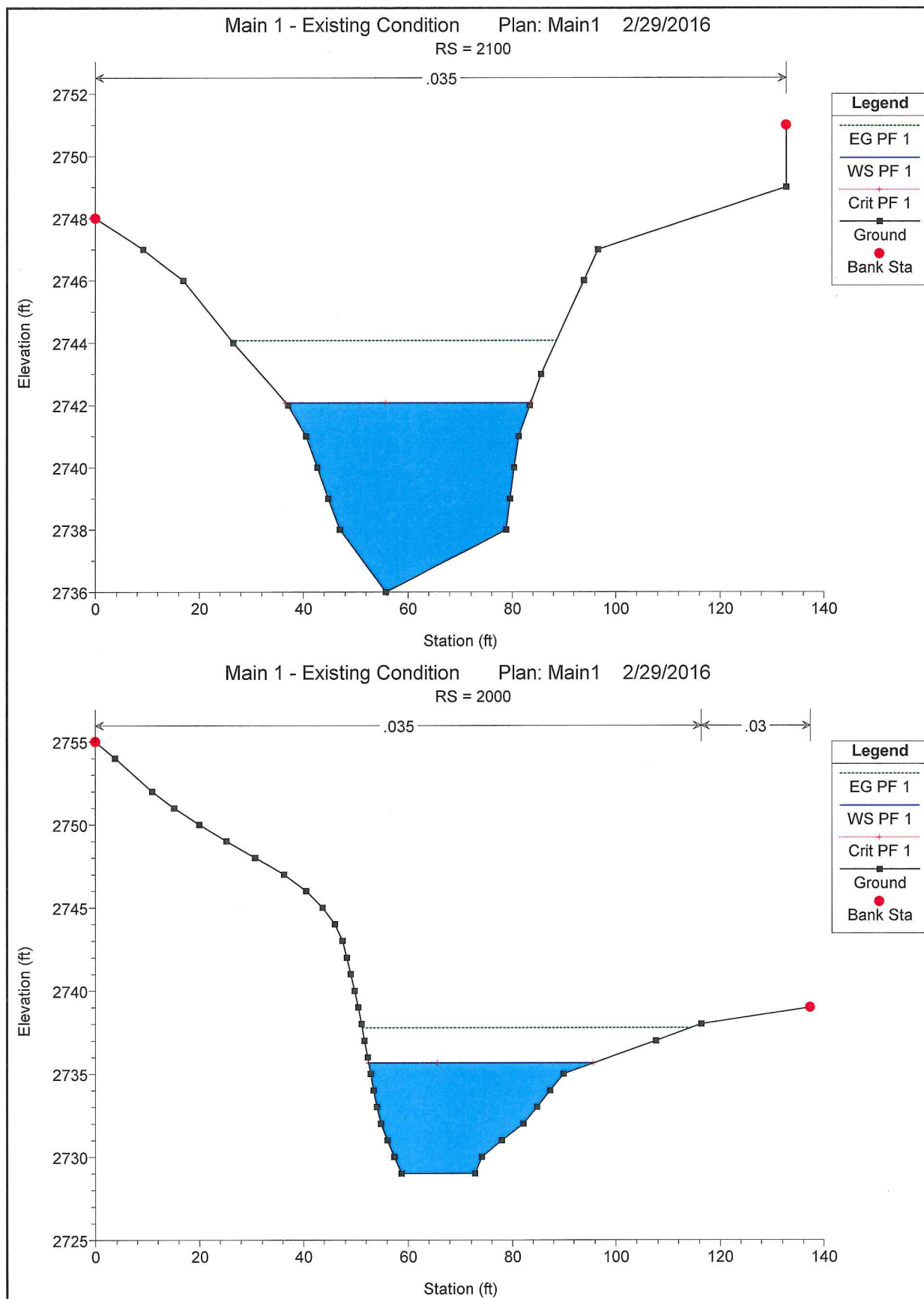
Main 1 - Existing Condition Plan: Main1 2/29/2016

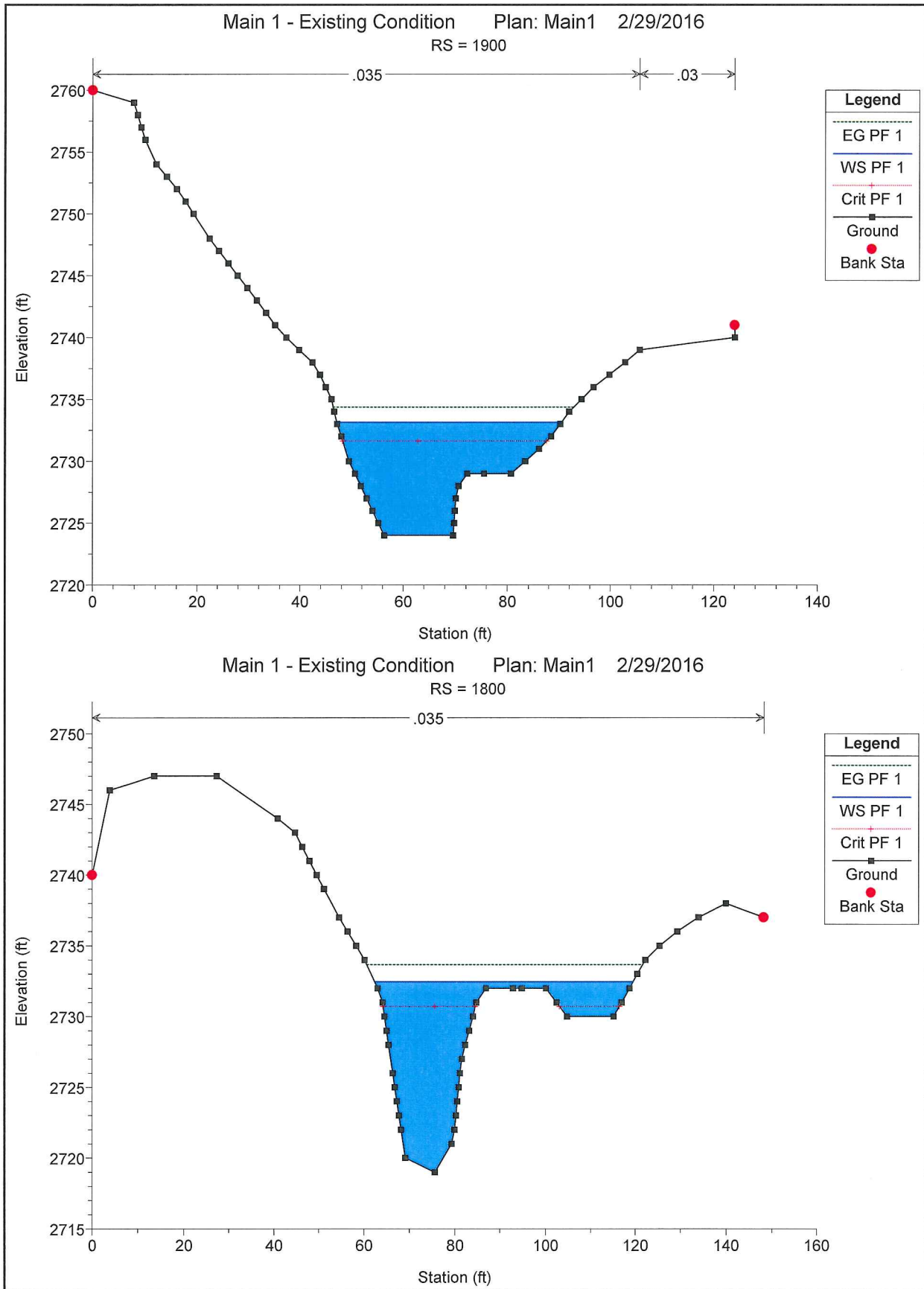


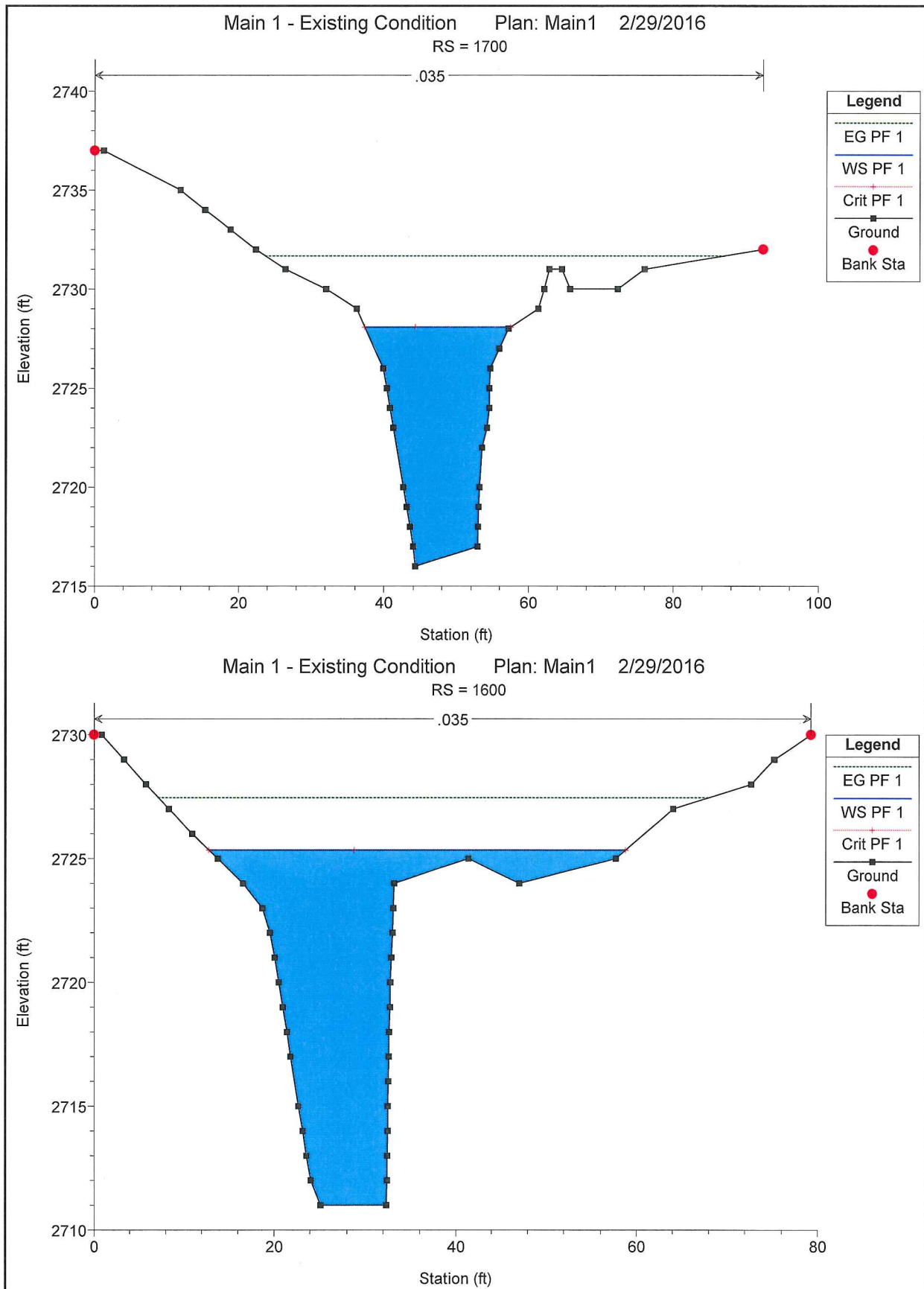


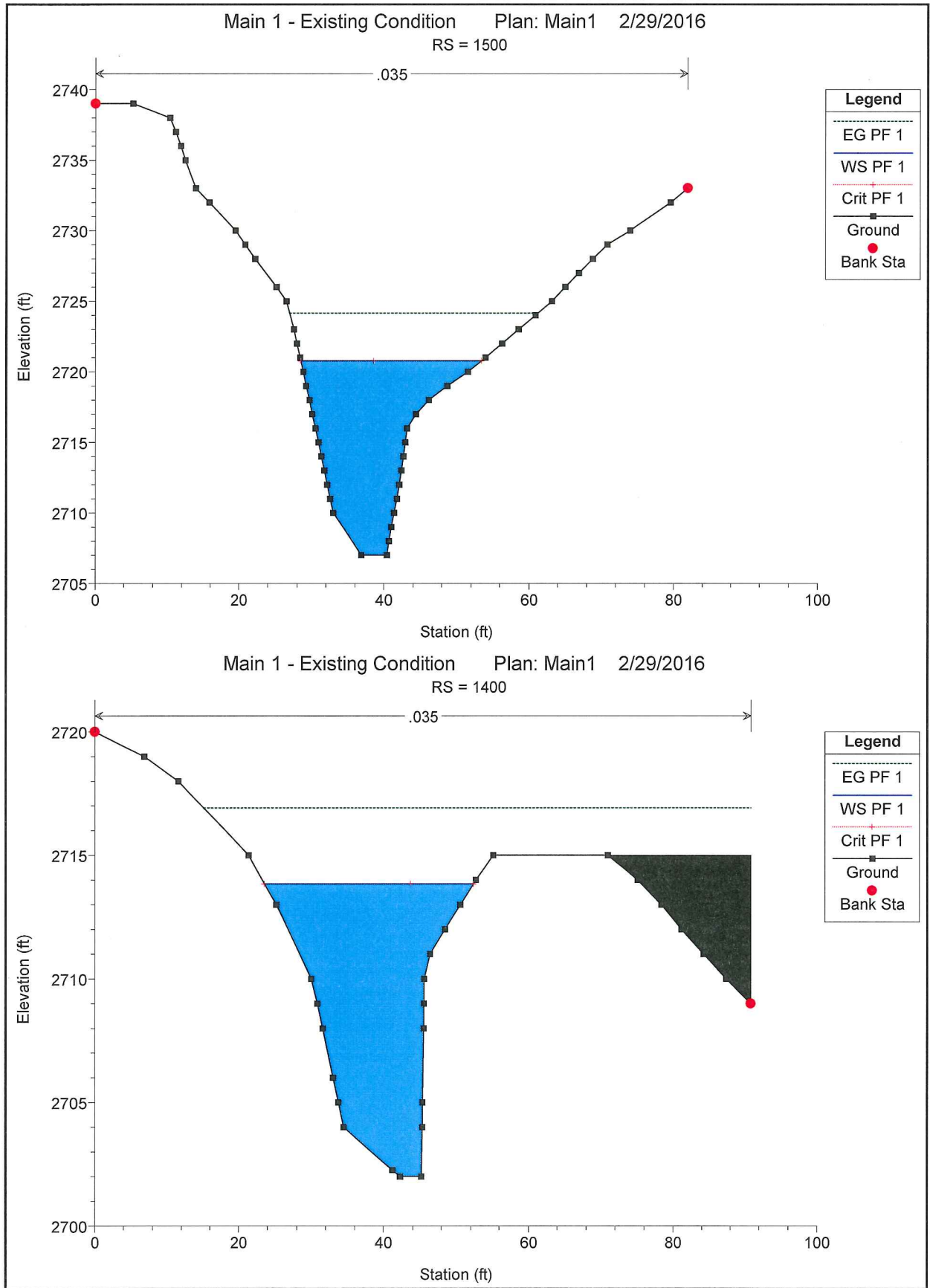


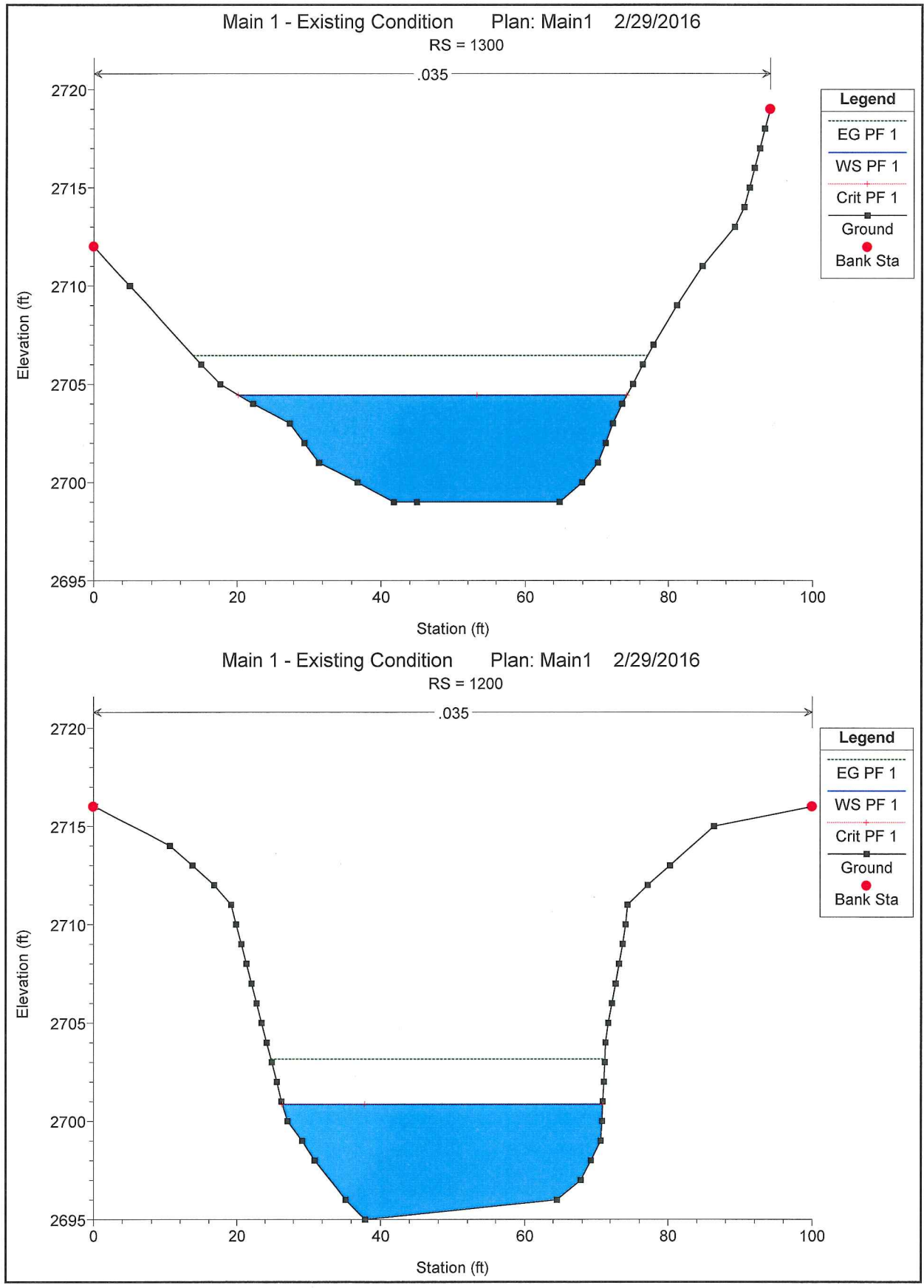


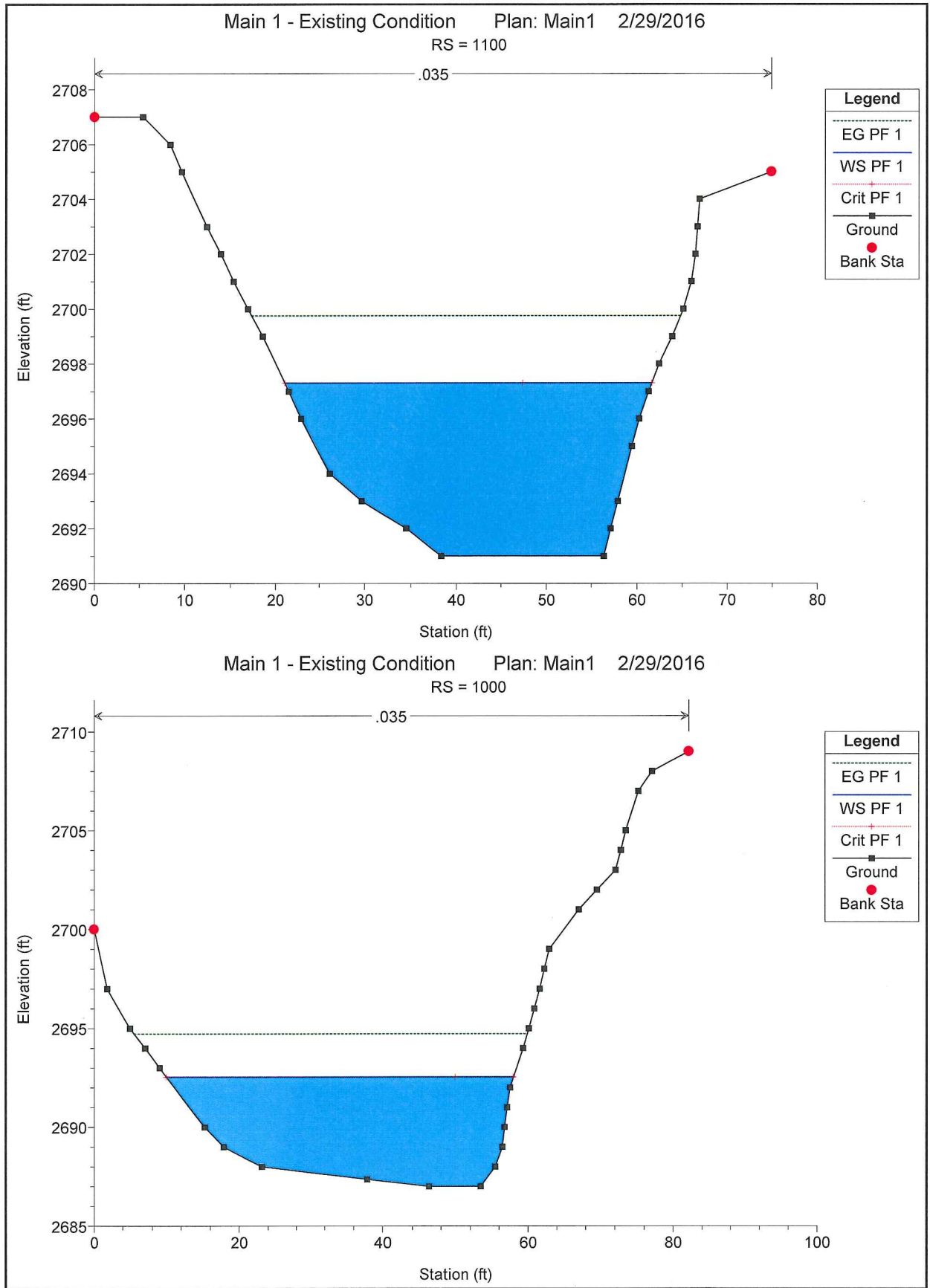


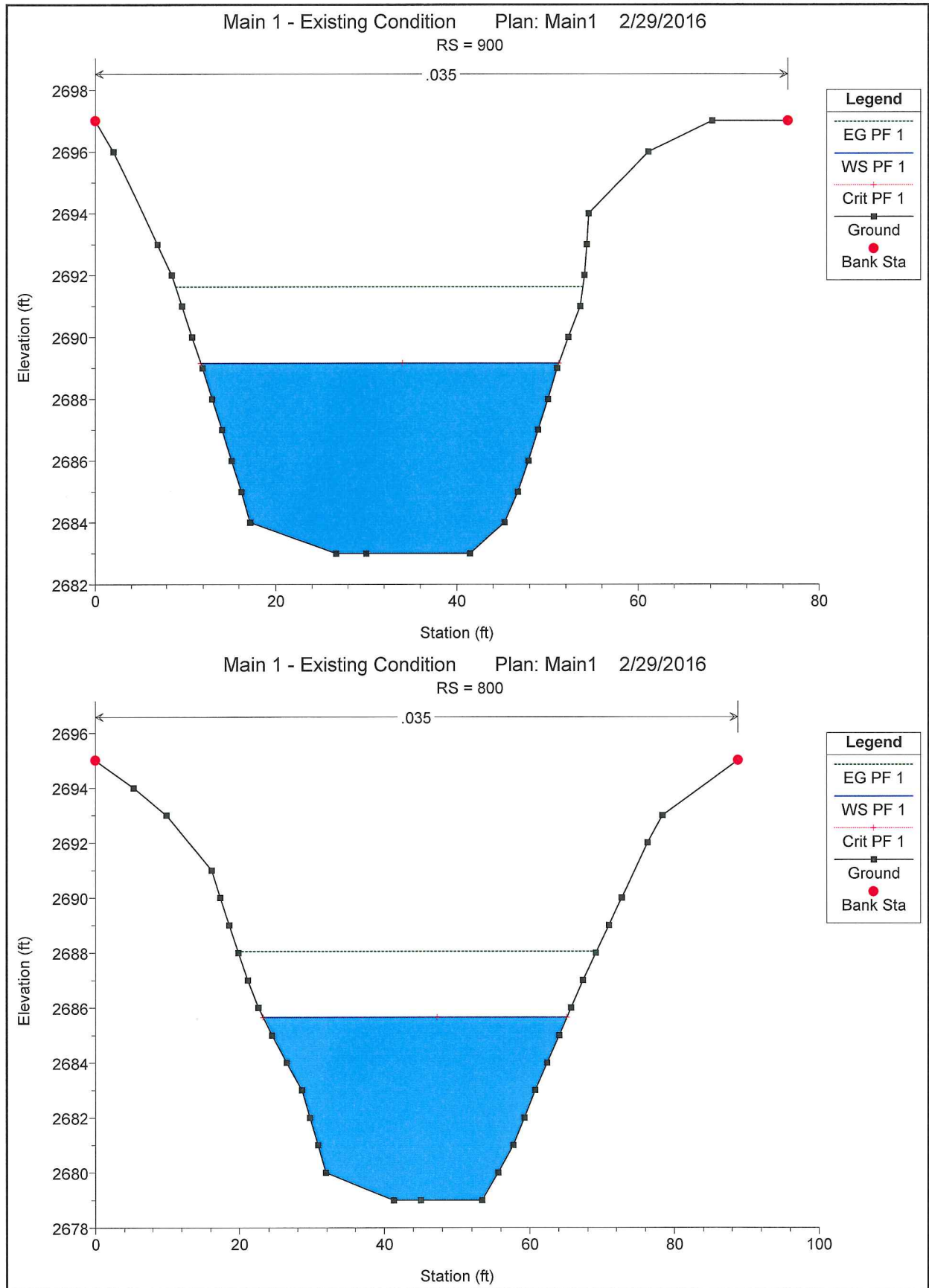


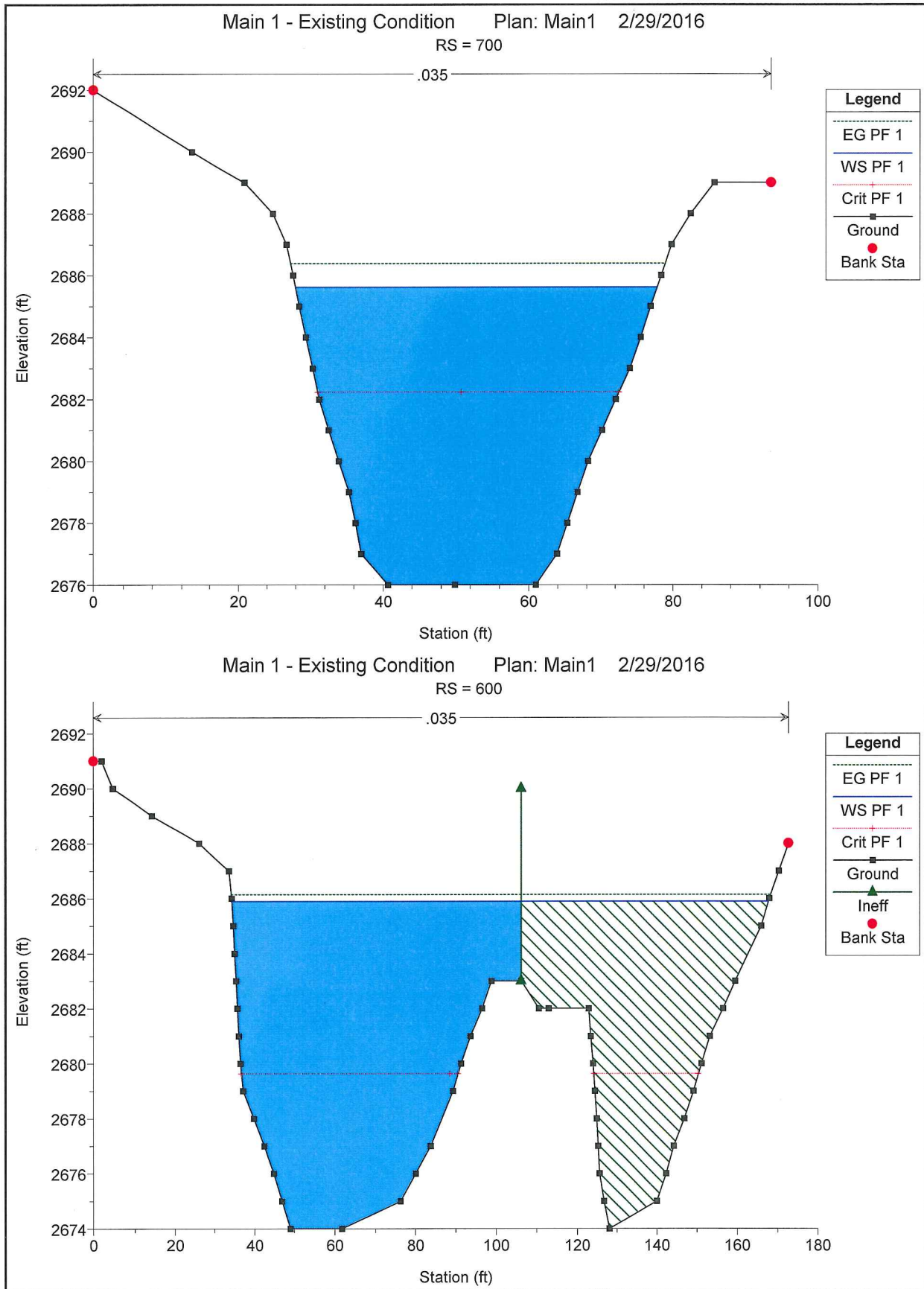


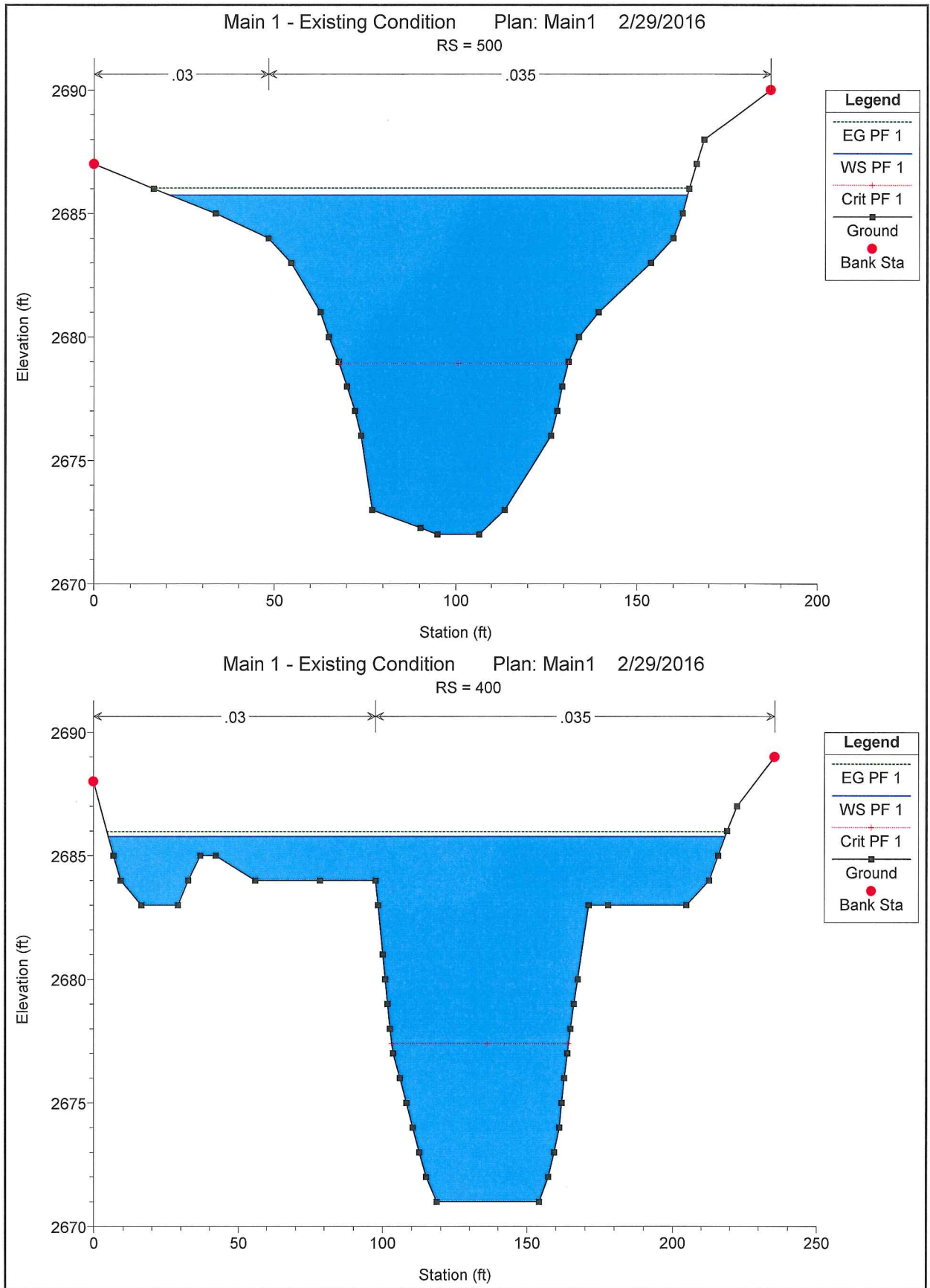












HEC-RAS ANALYSIS

EXISTING CONDITIONS MAIN 2

HEC-RAS Version 4.1.0 Jan 2010
U.S. Army Corps of Engineers
Hydrologic Engineering Center
609 Second Street
Davis, California

```

X      X XXXXXX   XXXX      XXXX      XX      XXXX
X      X X       X   X      X   X      X   X      X
X      X X       X       X      X   X      X   X      X
XXXXXXX XXXX   X       XXX XXXX   XXXXXX   XXXX
X      X X       X       X   X      X   X      X       X
X      X X       X   X      X   X      X   X      X
X      X XXXXXX   XXXX      X   X      X   X      XXXXX

```

PROJECT DATA

Project Title: Main 2 - Existing Condition
Project File : EXISTINGSOUTHWASH.prj
Run Date and Time: 2/29/2016 11:00:05 AM

Project in English units

PLAN DATA

Plan Title: Main2 Existing
Plan File : f:\Projects\800\840-050\Division\Fctl\Calcs\HEC-RAS\02-Main2\EXISTINGSOUTHWASH.P01

Geometry Title: Main2 Existing
Geometry File : f:\Projects\800\840-050\Division\Fctl\Calcs\HEC-RAS\02-Main2\EXISTINGSOUTHWASH.G01

Flow Title : Main2 Existing
Flow File : f:\Projects\800\840-050\Division\Fctl\Calcs\HEC-RAS\02-Main2\EXISTINGSOUTHWASH.F01

Plan Summary Information:

Number of:	Cross Sections =	6	Multiple Openings =	0
	Culverts =	0	Inline Structures =	0
	Bridges =	0	Lateral Structures =	0

Computational Information

Water surface calculation tolerance	=	0.01
Critical depth calculation tolerance	=	0.01
Maximum number of iterations	=	20
Maximum difference tolerance	=	0.3
Flow tolerance factor	=	0.001

Computation Options

Critical depth computed at all cross sections
Conveyance Calculation Method: At breaks in n values only
Friction Slope Method: Average Conveyance
Computational Flow Regime: Mixed Flow

FLOW DATA

Flow Title: Main2 Existing
Flow File : f:\Projects\800\840-050\Division\Fctl\Calcs\HEC-RAS\02-Main2\EXISTINGSOUTHWASH.F01

Flow Data (cfs)

River	Reach	RS	PF 1
Unnamed Lateral	Lateral 1	5400	1912

Boundary Conditions

River	Reach	Profile	Upstream	
Downstream				
Unnamed Lateral	Lateral 1	PF 1	Critical	Normal S = 0.011

GEOMETRY DATA

Geometry Title: Main2 Existing
 Geometry File : f:\Projects\800\840-050\Division\Fctl\Calcs\HEC-RAS\02-Main2\EXISTINGSOUTHWASH.G01

CROSS SECTION

RIVER: Unnamed Lateral
 REACH: Lateral 1 RS: 5400

INPUT

Description:

Station	Elevation	Data	num=	31					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2787	2.95	2786	6.53	2785	38.23	2784	42.43	2784
54.94	2785	58.99	2786	63.69	2787	68.44	2788	75.94	2788
80.04	2787	83.41	2786	87.97	2785	100.26	2785	104.72	2786
134.14	2786	154.63	2786	158.25	2786	164.28	2785	169.88	2784
175.32	2783	181.95	2783	193.11	2783	197.84	2784	204.19	2784
237.35	2781	254.68	2780	258.39	2780	275	2780.8	293.68	2780.8
293.68	2787								

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.035	54.94	.03	237.35	.035	293.68	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	0	293.68		211	96		.1	.3

Blocked Obstructions	num=	2
Sta L	Sta R	Elev
169.88	197.84	2784
169.88	197.84	2782

CROSS SECTION

RIVER: Unnamed Lateral
 REACH: Lateral 1 RS: 5300

INPUT

Description:

Station	Elevation	Data	num=	32					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2783	5.22	2782	10.85	2781	52.66	2781	56.83	2782
60.59	2783	64.22	2784	67.89	2785	71.65	2786	75.71	2787
79.72	2788	83.93	2789	89.08	2790	94.88	2791	108.85	2790
117.91	2789	120.88	2789	131.44	2789	136.09	2788	140.07	2787
143.78	2786	147.88	2785	154.19	2784	198.1	2782	205.69	2781
212	2780	213.74	2779	230.55	2778	231.24	2778	246.2	2779
267.09	2779	267.09	2785						

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.035	56.83	.03	212	.035	267.09	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	0	267.09		181.6	103		.1	.3

Blocked Obstructions num= 2
Sta L Sta R Elev Sta L Sta R Elev
0 60.59 2783 0 60.59 2780

CROSS SECTION

RIVER: Unnamed Lateral
REACH: Lateral 1 RS: 5200

INPUT

Description:

Station Elevation Data num= 36

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2778	6.35	2777	64.02	2777	65.52	2778	78.35	2779
102.26	2779	110.95	2777	112.68	2776	118.85	2775	119.4	2774
119.81	2773	120.22	2772	120.68	2771	121.1	2770	121.53	2769
121.99	2768	123.78	2767	127.96	2766	152.34	2765	160.08	2764
171.08	2764	171.58	2765	172.09	2766	172.47	2767	172.89	2768
173.22	2769	173.57	2770	174.17	2772	174.49	2773	174.77	2774
175.81	2775	186.5	2776	209.86	2777	217.39	2777	238.13	2777
246.61	2777								

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	78.35	.03	102.26	.035

Bank Sta:	Left	Right	Lengths:	Left	Channel	Right	Coeff	Contr.	Expan.
	0	246.61		101.72	101.18	99.54		.1	.3

CROSS SECTION

RIVER: Unnamed Lateral
REACH: Lateral 1 RS: 5100

INPUT

Description:

Station Elevation Data num= 47

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2778.55	6.02	2776	7.94	2775	9.49	2774	23.17	2774
71.71	2775	74.37	2775	93.06	2774	109.68	2773	110.14	2772
110.57	2771	110.99	2770	111.35	2769	114.85	2768	119.16	2767
123.19	2766	126.75	2765	130.16	2764	134.46	2762	136.12	2761
140.9	2760	144.37	2760	148.44	2761	150.35	2761	154.69	2760
161.59	2759	164.24	2759	169.63	2760	173.1	2761	175.15	2762
176.7	2763	199.05	2764	199.21	2765	199.37	2766	199.53	2767
199.62	2768	199.79	2769	199.92	2770	200.06	2771	200.4	2772
205.81	2773	212.2	2774	215.84	2775	241.01	2775	245.76	2774
263.63	2774	263.63	2780						

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	215.84	.03	241.01	.035

Bank Sta:	Left	Right	Lengths:	Left	Channel	Right	Coeff	Contr.	Expan.
	0	263.63		49.87	50.66	49.68		.1	.3

CROSS SECTION

RIVER: Unnamed Lateral
REACH: Lateral 1 RS: 5000

INPUT

Description:

Station Elevation Data num= 38

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2776	.2	2776	2.69	2775	4.37	2774	10.52	2773
12.97	2773	63.61	2773	107.83	2773	128.27	2772	131.15	2771
131.75	2770	132.33	2769	132.94	2768	133.52	2767	134.1	2766

134.69	2765	135.28	2764	135.86	2763	136.47	2762	137.01	2761
137.58	2760	139.32	2759	141.34	2758	156.37	2758	161.79	2759
169.28	2760	173.97	2761	194.87	2762	206.23	2762	208.36	2765
208.68	2766	209.01	2767	209.33	2768	209.62	2769	210.13	2771
217.27	2772	267.37	2773	267.37	2776				

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	267.37	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	0	267.37		99.31 100.71	99.87		.1	.3

CROSS SECTION

RIVER: Unnamed Lateral
 REACH: Lateral 1 RS: 4900

INPUT

Description:

Station Elevation Data num= 37

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2771	22.9	2771	44.41	2770	56.5	2770	80.02	2770
110.42	2769	112.53	2768	112.7	2767	112.95	2766	113.16	2765
113.62	2764	117.02	2763	118.49	2762	119.53	2761	120.36	2760
121.19	2759	122.01	2758	122.82	2757	124.21	2756	141.49	2756
146.47	2757	149.64	2758	159.38	2759	174.05	2759	183.11	2759
183.46	2760	183.75	2761	184.03	2762	184.31	2763	184.65	2764
184.94	2765	185.27	2766	185.58	2767	185.84	2768	190.13	2769
226.92	2770	236.19	2771						

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	236.19	.035

Bank Sta:	Left	Right	Coeff	Contr.	Expan.
	0	236.19		.1	.3

SUMMARY OF MANNING'S N VALUES

River: Unnamed Lateral

Reach	River Sta.	n1	n2	n3	n4
Lateral 1	5400	.035	.03	.035	.035
Lateral 1	5300	.035	.03	.035	.035
Lateral 1	5200	.035	.03	.035	
Lateral 1	5100	.035	.03	.035	
Lateral 1	5000	.035	.035	.035	
Lateral 1	4900	.035	.035	.035	

SUMMARY OF REACH LENGTHS

River: Unnamed Lateral

Reach	River Sta.	Left	Channel	Right
Lateral 1	5400	211	96	93.25
Lateral 1	5300	181.6	103	49.77
Lateral 1	5200	101.72	101.18	99.54
Lateral 1	5100	49.87	50.66	49.68
Lateral 1	5000	99.31	100.71	99.87
Lateral 1	4900			

SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS

River: Unnamed Lateral

Reach	River Sta.	Contr.	Expan.
Lateral 1	5400	.1	.3
Lateral 1	5300	.1	.3
Lateral 1	5200	.1	.3
Lateral 1	5100	.1	.3
Lateral 1	5000	.1	.3
Lateral 1	4900	.1	.3

ERRORS WARNINGS AND NOTES

Errors Warnings and Notes for Plan : 2

River: Unnamed Lateral Reach: Lateral 1 RS: 5400 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Lateral Reach: Lateral 1 RS: 5300 Profile: PF 1

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

River: Unnamed Lateral Reach: Lateral 1 RS: 5200 Profile: PF 1

Warning:The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning:The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

River: Unnamed Lateral Reach: Lateral 1 RS: 5100 Profile: PF 1

Warning:The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning:The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

River: Unnamed Lateral Reach: Lateral 1 RS: 5000 Profile: PF 1

Warning:The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

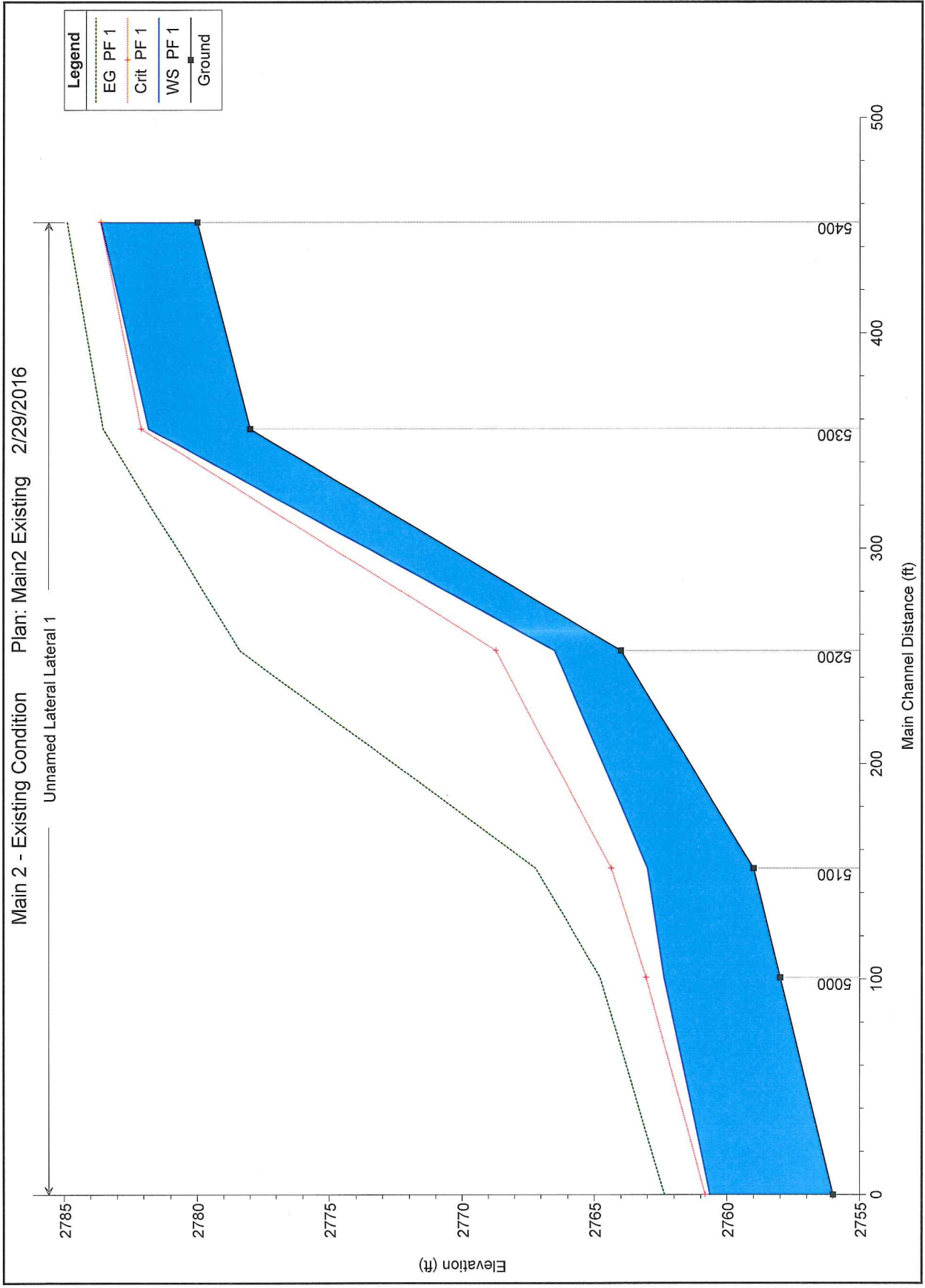
River: Unnamed Lateral Reach: Lateral 1 RS: 4900 Profile: PF 1

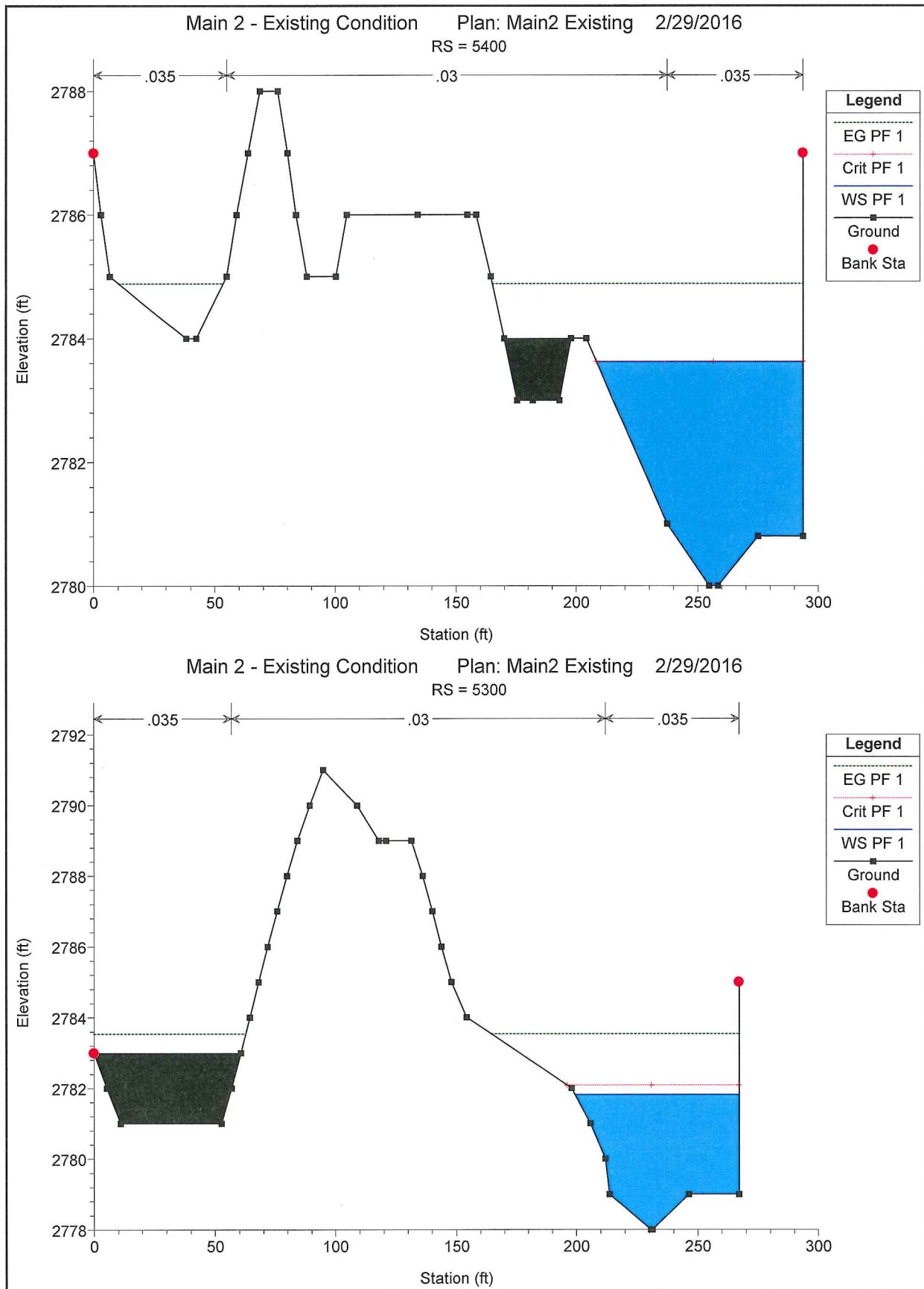
Warning:The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

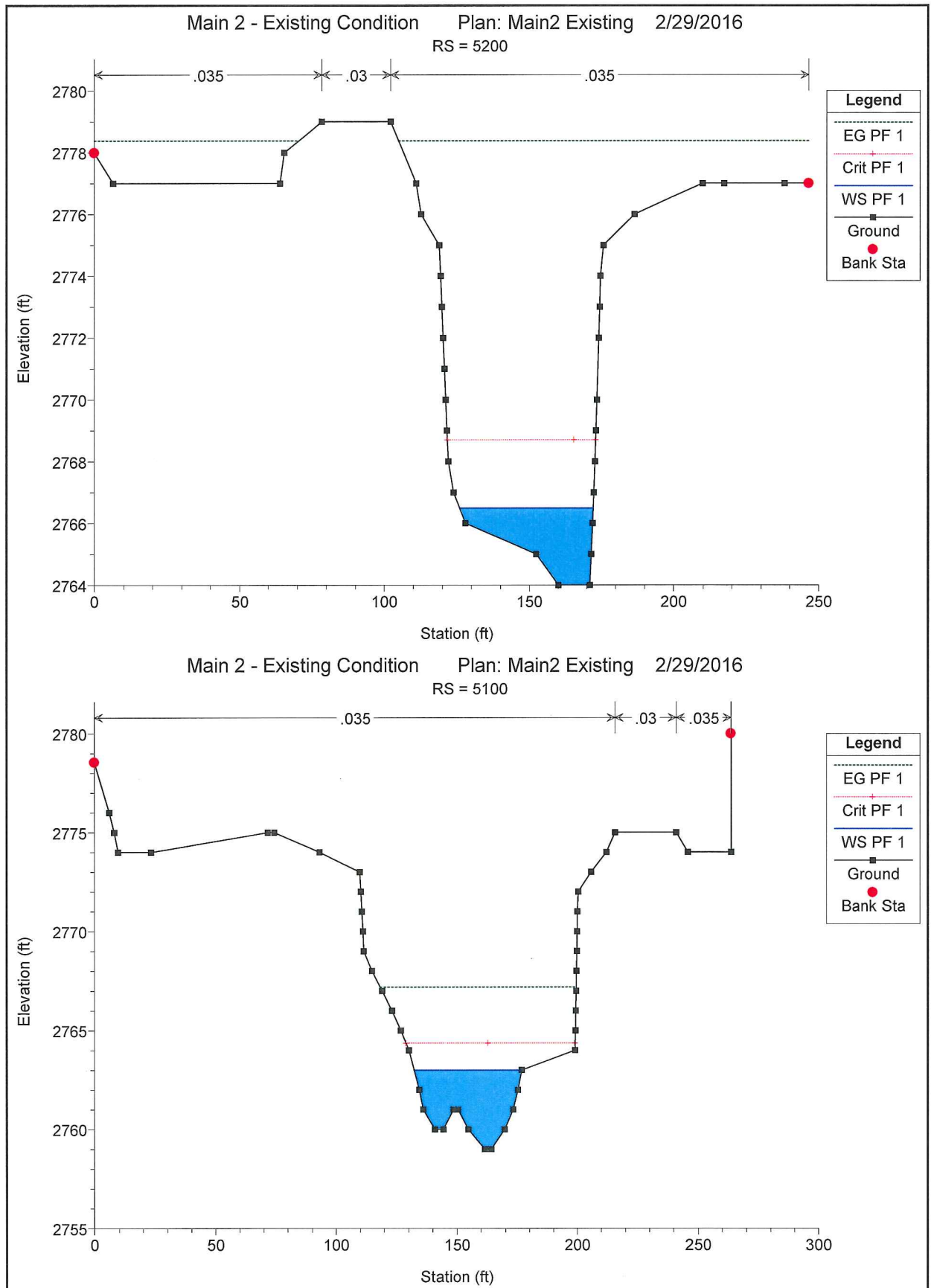
Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

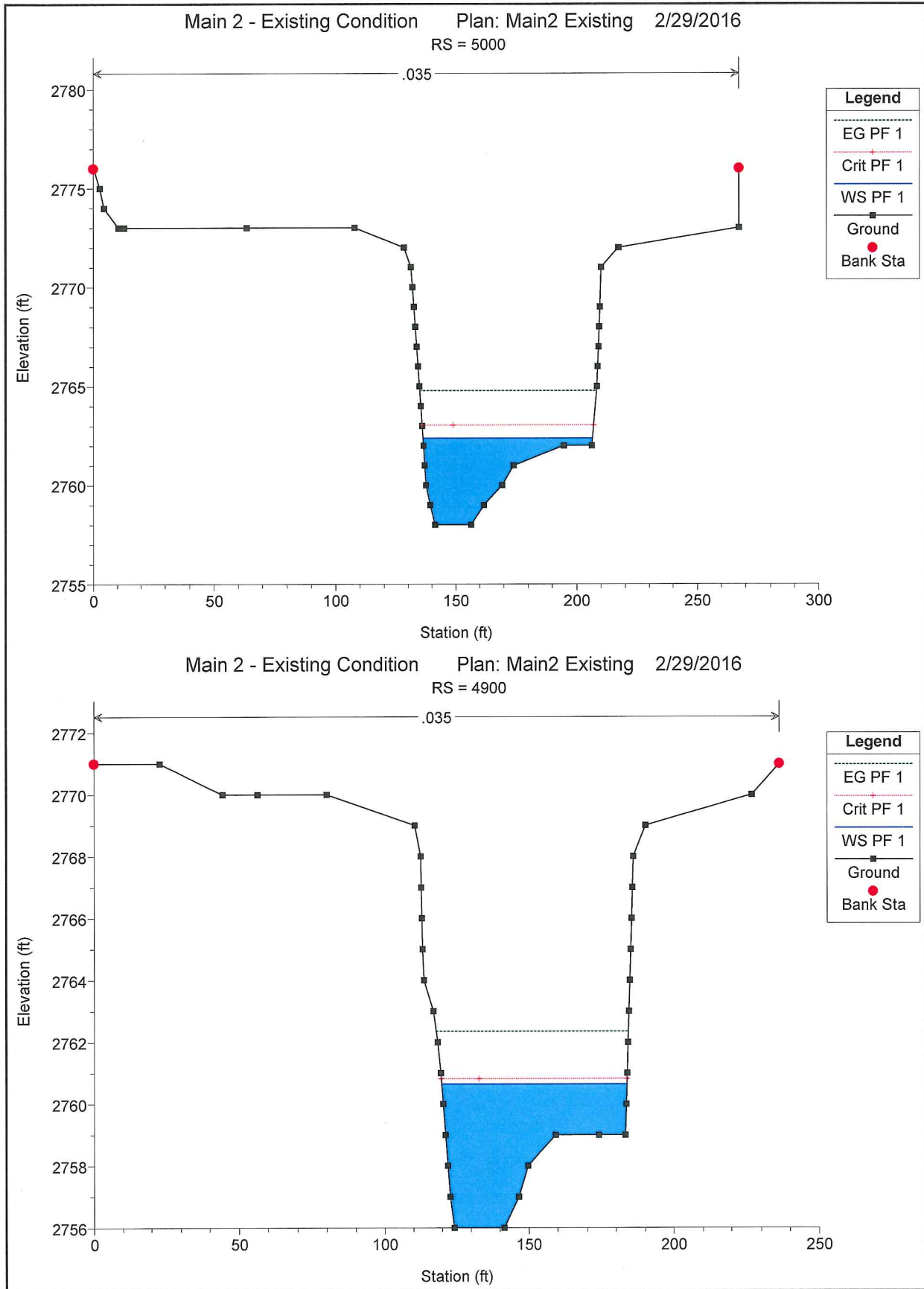
HEC-RAS Plan: 2 River: Unnamed Lateral Reach: Lateral 1 Profile: PF 1

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Lateral 1	5400	PF 1	1912.00	2780.00	2783.62	2783.63	2784.89	0.012091	9.02	211.90	85.33	1.01
Lateral 1	5300	PF 1	1912.00	2778.00	2781.81	2782.08	2783.54	0.015582	10.54	181.43	67.57	1.13
Lateral 1	5200	PF 1	1912.00	2764.00	2766.49	2768.70	2778.38	0.0261843	27.67	69.11	46.38	3.99
Lateral 1	5100	PF 1	1912.00	2759.00	2762.99	2764.36	2767.18	0.0435559	16.44	116.28	44.34	1.79
Lateral 1	5000	PF 1	1912.00	2758.00	2762.37	2763.03	2764.77	0.031622	12.44	153.65	70.25	1.48
Lateral 1	4900	PF 1	1912.00	2756.00	2760.64	2760.82	2762.35	0.016226	10.50	182.15	63.82	1.09









HEC-RAS ANALYSIS

PROPOSED CONDITIONS MAIN 1

HEC-RAS Version 4.1.0 Jan 2010
U.S. Army Corps of Engineers
Hydrologic Engineering Center
609 Second Street
Davis, California

```

X      X  XXXXXX   XXXX      XXXX      XX      XXXX
X      X  X      X      X      X  X      X  X      X
X      X  X      X      X      X  X      X  X      X
XXXXXXXX XXXX      X      XXX XXXX   XXXXXX   XXXX
X      X  X      X      X  X      X  X      X      X
X      X  X      X      X  X      X  X      X      X
X      X  XXXXXX   XXXX      X  X      X  X      XXXXX

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PROJECT DATA

Project Title: Main 1 - Proposed Condition

Project File : PROP3.prj

Run Date and Time: 3/2/2016 4:20:31 PM

Project in English units

PLAN DATA

Plan Title: Current model

Plan File : f:\Projects\800\840-050\Division\Fctl\Calcs\HEC-RAS\01-Main1\PROP3.P01

Geometry Title: Main 1 Proposed

Geometry File : f:\Projects\800\840-050\Division\Fctl\Calcs\HEC-RAS\01-Main1\PROP3.G01

Flow Title : 0 Flow Profiles

Flow File : f:\Projects\800\840-050\Division\Fctl\Calcs\HEC-RAS\01-Main1\PROP3.F01

Plan Summary Information:

Number of:	Cross Sections =	4	Multiple Openings =	0
	Culverts =	0	Inline Structures =	0
	Bridges =	0	Lateral Structures =	0

Computational Information

Water surface calculation tolerance	=	0.01
Critical depth calculation tolerance	=	0.01
Maximum number of iterations	=	20
Maximum difference tolerance	=	0.3
Flow tolerance factor	=	0.001

Computation Options

Critical depth computed at all cross sections
Conveyance Calculation Method: At breaks in n values only
Friction Slope Method: Average Conveyance
Computational Flow Regime: Subcritical Flow

FLOW DATA

Flow Title: 0 Flow Profiles

Flow File : f:\Projects\800\840-050\Division\Fctl\Calcs\HEC-RAS\01-Main1\PROP3.F01

Flow Data (cfs)

River	Reach	RS	PF 1
Unnamed Wash	Main1-Prop	2700	2128

Boundary Conditions

River	Reach	Profile	Upstream	
Downstream				
Unnamed Wash	Main1-Prop	PF 1	Critical	Known WS =
2752.49				

GEOMETRY DATA

Geometry Title: Main 1 Proposed

Geometry File : f:\Projects\800\840-050\Division\Fct1\Calcs\HEC-RAS\01-Main1\PROP3.G01

CROSS SECTION

RIVER: Unnamed Wash

REACH: Main1-Prop RS: 2700

INPUT

Description:

Station Elevation Data				num=	32				
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2769	4.32	2768	8.89	2767	14.12	2766	19.18	2765
24.32	2764	29.44	2763	34.62	2762	39.85	2761	45	2760
48.3	2759	51.08	2758	54.15	2757	58.29	2756	74.22	2756
77.45	2757	80.08	2758	90.95	2758	94.1	2757	95.07	2757
97.37	2758	99.58	2759	100.37	2760	101.18	2761	101.97	2762
103.09	2763	105.64	2764	108.63	2765	112.52	2766	116.09	2767
119.56	2768	127.49	2769						

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	127.49	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	0	127.49		95.75	98.69	107.97	.1	.3

CROSS SECTION

RIVER: Unnamed Wash

REACH: Main1-Prop RS: 2600

INPUT

Description:

Station Elevation Data				num=	34				
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2765	3.19	2764	6.31	2763	9.41	2762	12.03	2761
12.88	2760	13.83	2759	14.76	2758	15.74	2757	16.76	2756
17.69	2755	18.58	2754	22.83	2752	32.12	2752	37.82	2754
43.67	2755	52.8	2756	66.54	2757	66.62	2758	66.71	2759
68.82	2761	68.85	2761	70.78	2759	71.78	2758	72.75	2757
86.93	2757	90.38	2758	91.7	2759	92.96	2760	94.15	2761
99.48	2762	104.49	2763	110.14	2764	115.64	2765		

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	115.64	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	0	115.64		101.86	103.65	108.71	.1	.3

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1-Prop RS: 2500

INPUT

Description:

Station Elevation Data		num=		20					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2761	.38	2760	.75	2759	1.17	2758	1.89	2756
2.3	2755	2.68	2754	3.06	2753	3.44	2752	9.58	2748
17.77	2748	34.89	2752	60.1	2753	67.24	2754	71.71	2755
76.74	2756	84.67	2758	93.68	2759	99.64	2760	104.45	2761

Manning's n Values		num=		3	
Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	104.45	.035

Bank Sta:	Left	Right	Lengths:	Left	Channel	Right	Coeff	Contr.	Expan.
	0	104.45		108.74	100.43	96.31		.1	.3

CROSS SECTION

RIVER: Unnamed Wash
 REACH: Main1-Prop RS: 2400

INPUT

Description:

Station Elevation Data		num=		14					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2758	33	2739.36	55	2739.36	74	2749	90.83	2749
95.4	2751	98.61	2752	104.46	2754	109.02	2755	118.84	2756
121.79	2757	123.77	2758	126.1	2759	128.13	2759		

Manning's n Values		num=		3	
Sta	n Val	Sta	n Val	Sta	n Val
0	.035	0	.035	128.13	.035

Bank Sta:	Left	Right	Coeff	Contr.	Expan.
	0	128.13		.3	.5

SUMMARY OF MANNING'S N VALUES

River: Unnamed Wash

Reach	River Sta.	n1	n2	n3
Main1-Prop	2700	.035	.035	.035
Main1-Prop	2600	.035	.035	.035
Main1-Prop	2500	.035	.035	.035
Main1-Prop	2400	.035	.035	.035

SUMMARY OF REACH LENGTHS

River: Unnamed Wash

Reach	River Sta.	Left	Channel	Right
Main1-Prop	2700	95.75	98.69	107.97
Main1-Prop	2600	101.86	103.65	108.71
Main1-Prop	2500	108.74	100.43	96.31
Main1-Prop	2400			

SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS

River: Unnamed Wash

Reach	River Sta.	Contr.	Expan.
Main1-Prop	2700	.1	.3
Main1-Prop	2600	.1	.3
Main1-Prop	2500	.1	.3
Main1-Prop	2400	.3	.5

ERRORS WARNINGS AND NOTES

Errors Warnings and Notes for Plan : Current mode

River: Unnamed Wash Reach: Main1-Prop RS: 2700 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1-Prop RS: 2600 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:Divided flow computed for this cross-section.

Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

River: Unnamed Wash Reach: Main1-Prop RS: 2500 Profile: PF 1

Warning:The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning:The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning:The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

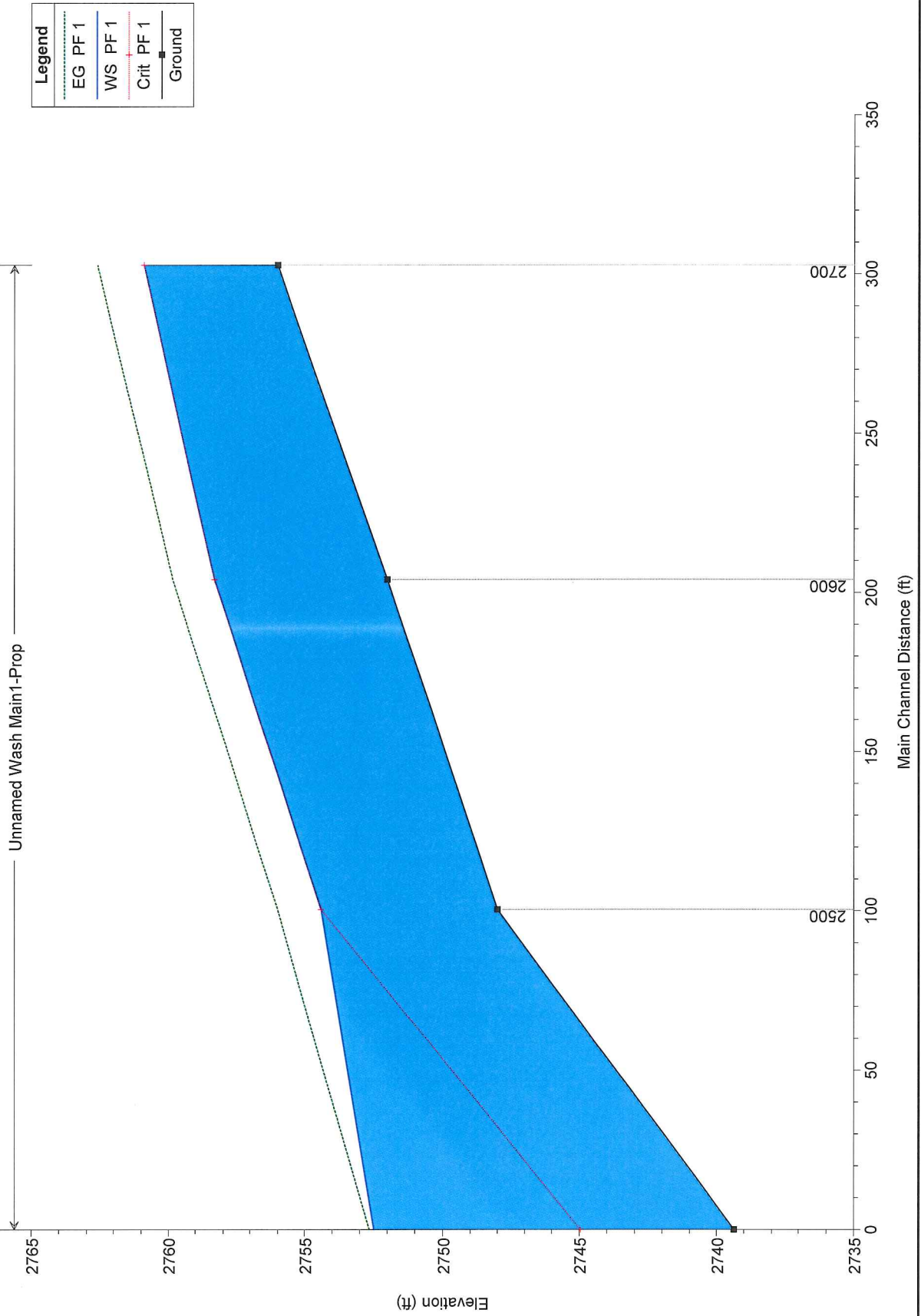
Warning:The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

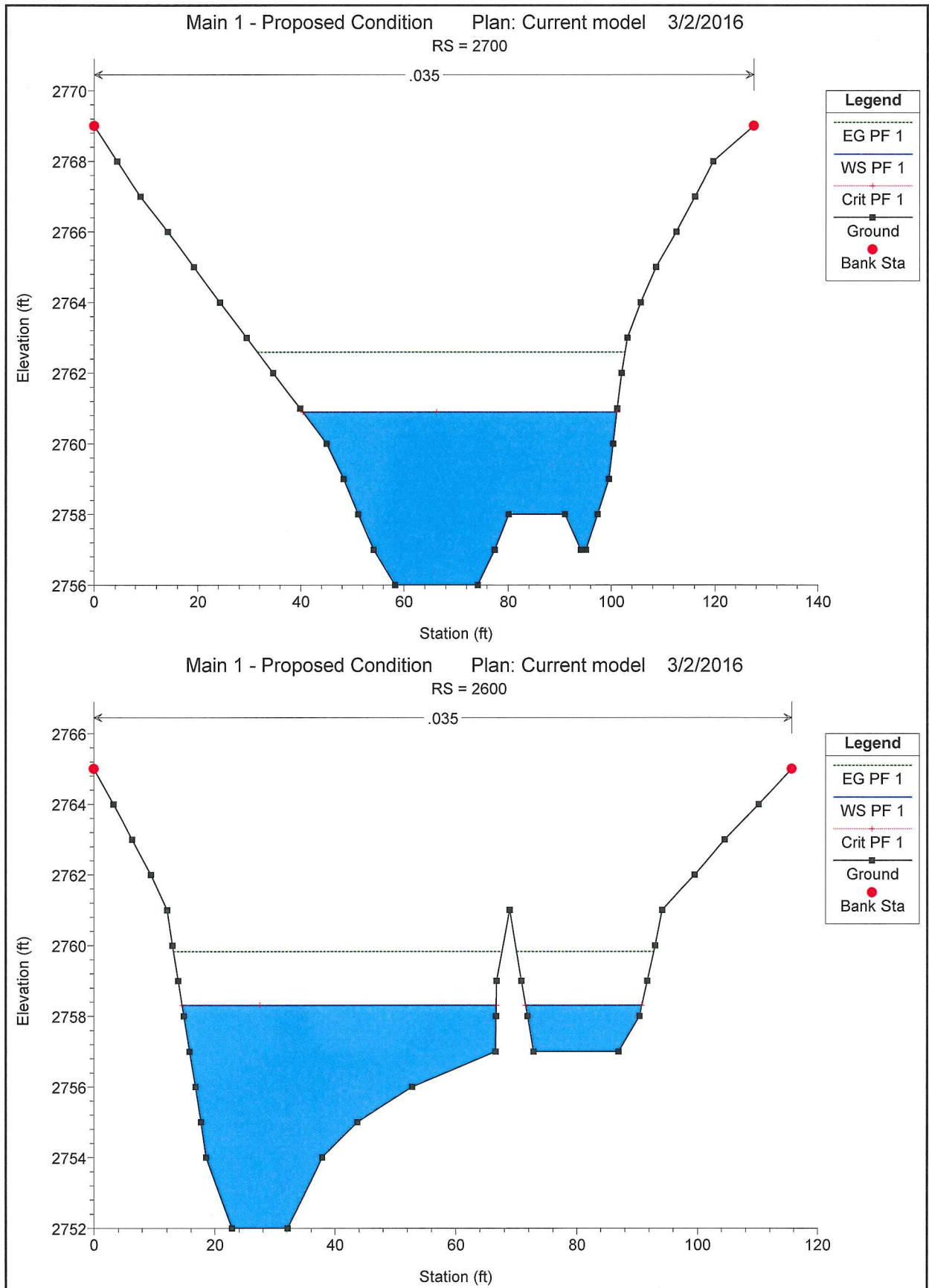
Warning:During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

HEC-RAS Plan: Current mode River: Unnamed Wash Reach: Main1-Prop Profile: PF 1

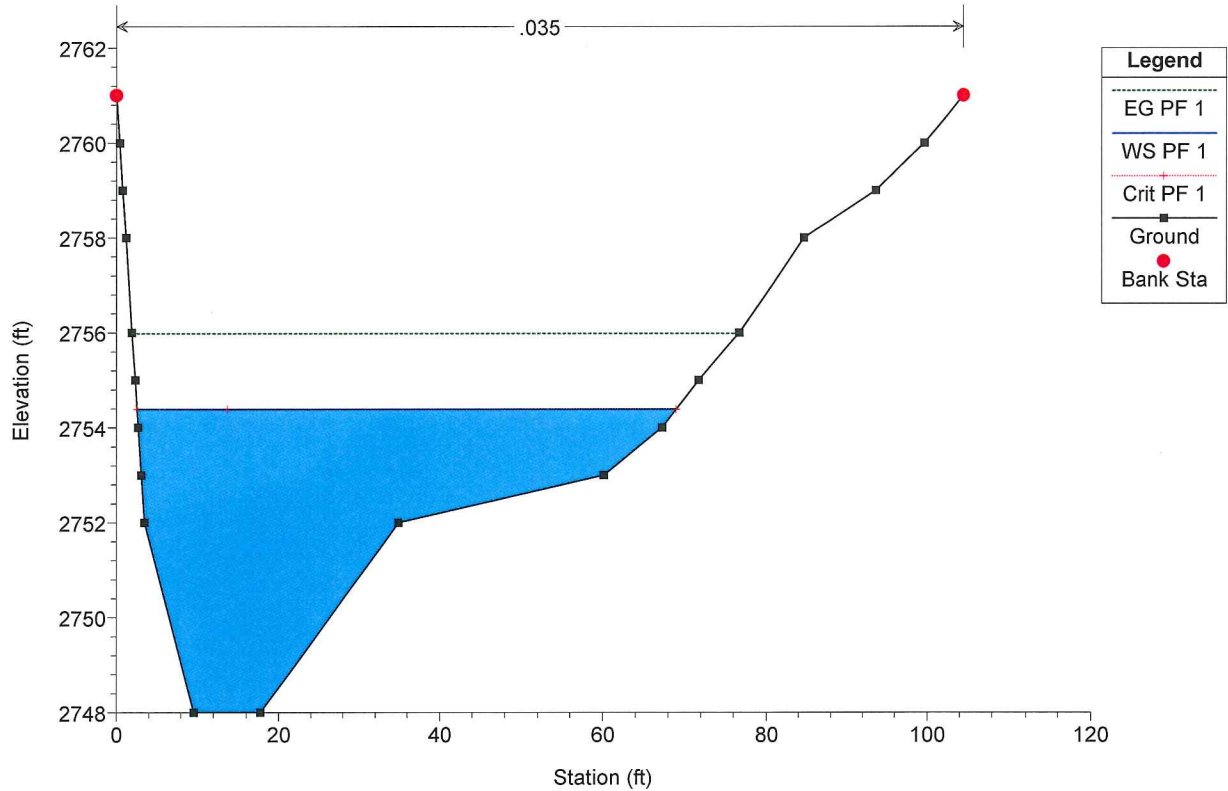
Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Main1-Prop	2700	PF 1	2128.00	2756.00	2760.90	2760.90	2762.59	0.012742	10.45	203.62	60.71	1.01
Main1-Prop	2800	PF 1	2128.00	2752.00	2758.31	2758.31	2759.83	0.013626	9.89	215.14	71.49	1.00
Main1-Prop	2500	PF 1	2128.00	2748.00	2754.39	2754.39	2755.99	0.013172	10.14	209.83	66.45	1.01
Main1-Prop	2400	PF 1	2128.00	2739.36	2752.49	2744.95	2752.65	0.000417	3.16	672.99	90.29	0.20

Main 1 - Proposed Condition Plan: Current model 3/2/2016

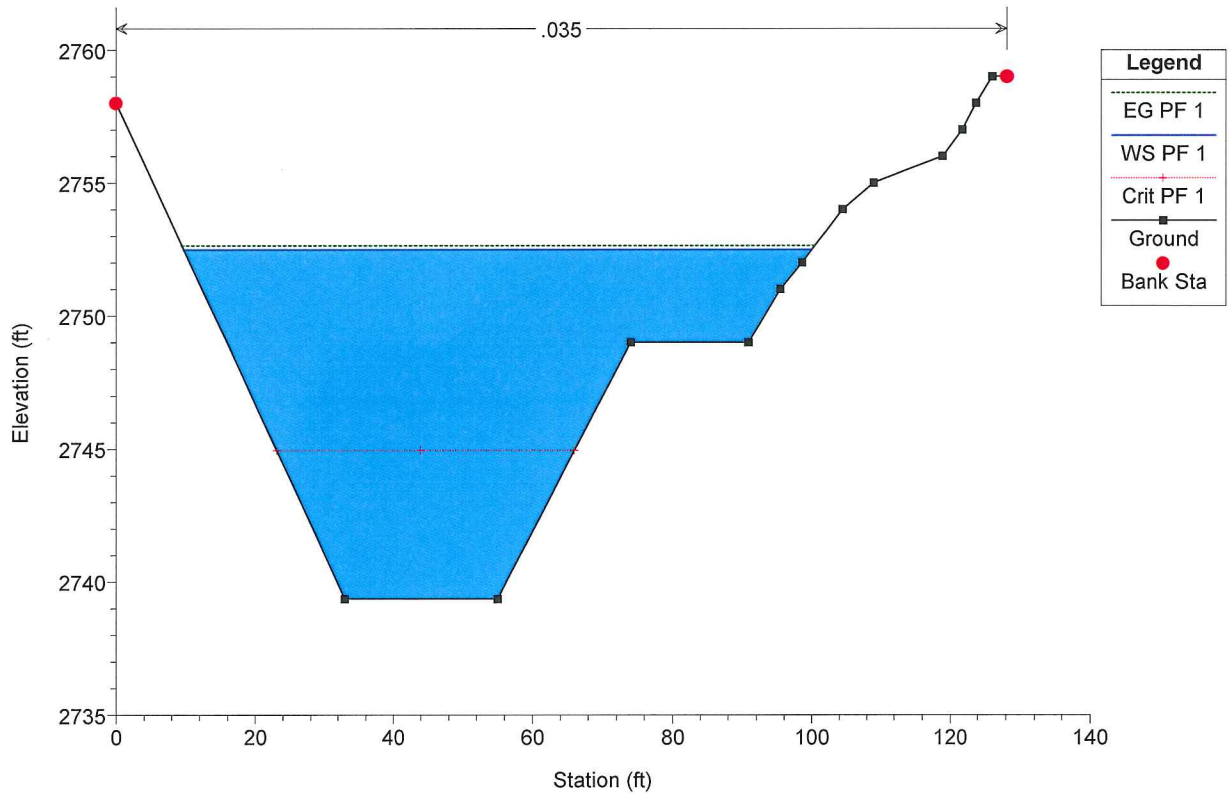




Main 1 - Proposed Condition Plan: Current model 3/2/2016
RS = 2500



Main 1 - Proposed Condition Plan: Current model 3/2/2016
RS = 2400



HEC-RAS ANALYSIS

PROPOSED CONDITIONS MAIN 2

HEC-RAS Version 4.1.0 Jan 2010
 U.S. Army Corps of Engineers
 Hydrologic Engineering Center
 609 Second Street
 Davis, California

```

X      X  XXXXXX   XXXX      XXXX      XX      XXXX
X      X  X      X      X      X  X      X  X      X
X      X  X      X      X      X  X      X  X      X
XXXXXXXX XXXX      X      XXX XXXX      XXXXXX      XXXX
X      X  X      X      X      X  X      X  X      X
X      X  X      X      X      X  X      X  X      X
X      X  XXXXXX   XXXX      X      X      X  X      XXXXX
  
```

PROJECT DATA

Project Title: Main 2 - Proposed Condition
 Project File : PROPOSEDSOUTHWASH.prj
 Run Date and Time: 3/3/2016 9:32:32 AM

Project in English units

PLAN DATA

Plan Title: Main 2
 Plan File : f:\Projects\800\840-050\Division\Fctl\Calcs\HEC-RAS\02-Main2\PROPOSEDSOUTHWASH.P01

Geometry Title: Main 2
 Geometry File : f:\Projects\800\840-050\Division\Fctl\Calcs\HEC-RAS\02-Main2\PROPOSEDSOUTHWASH.G01

Flow Title : Main 2
 Flow File : f:\Projects\800\840-050\Division\Fctl\Calcs\HEC-RAS\02-Main2\PROPOSEDSOUTHWASH.F01

Plan Summary Information:

Number of: Cross Sections =	5	Multiple Openings =	0
Culverts =	0	Inline Structures =	0
Bridges =	0	Lateral Structures =	0

Computational Information

Water surface calculation tolerance =	0.01
Critical depth calculation tolerance =	0.01
Maximum number of iterations =	20
Maximum difference tolerance =	0.3
Flow tolerance factor =	0.001

Computation Options

Critical depth computed at all cross sections
Conveyance Calculation Method: At breaks in n values only
Friction Slope Method: Average Conveyance
Computational Flow Regime: Mixed Flow

FLOW DATA

Flow Title: Main 2
 Flow File : f:\Projects\800\840-050\Division\Fctl\Calcs\HEC-RAS\02-Main2\PROPOSEDSOUTHWASH.F01

Flow Data (cfs)

River	Reach	RS	PF 1
Unnamed Lateral	Lateral 1	5400	1910

Boundary Conditions

River	Reach	Profile	Upstream	
Downstream				
Unnamed Lateral	Lateral 1	PF 1	Critical	Known WS =
2771.09				

GEOMETRY DATA

Geometry Title: Main 2
 Geometry File : f:\Projects\800\840-050\Division\Fct1\Calcs\HEC-RAS\02-Main2\PROPOSEDSOUTHWASH.G01

CROSS SECTION

RIVER: Unnamed Lateral
 REACH: Lateral 1 RS: 5400

INPUT

Description:

Station Elevation Data			num=	31					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2787	2.95	2786	6.53	2785	38.23	2784	42.43	2784
54.94	2785	58.99	2786	63.69	2787	68.44	2788	75.94	2788
80.04	2787	83.41	2786	87.97	2785	100.26	2785	104.72	2786
134.14	2786	154.63	2786	158.25	2786	164.28	2785	169.88	2784
175.32	2783	181.95	2783	193.11	2783	197.84	2784	204.19	2784
237.35	2781	254.68	2780	258.39	2780	275	2780.8	293.68	2780.8
293.68	2787								

Manning's n Values			num=	3
Sta	n Val	Sta	n Val	Sta
0	.035	54.94	.03	237.35
				.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	0	293.68		211	96		.1	.3

Blocked Obstructions			num=	2
Sta L	Sta R	Elev	Sta L	Sta R
169.88	197.84	2784	169.88	197.84
				2782

CROSS SECTION

RIVER: Unnamed Lateral
 REACH: Lateral 1 RS: 5300

INPUT

Description:

Station Elevation Data			num=	32					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2783	5.22	2782	10.85	2781	52.66	2781	56.83	2782
60.59	2783	64.22	2784	67.89	2785	71.65	2786	75.71	2787
79.72	2788	83.93	2789	89.08	2790	94.88	2791	108.85	2790
117.91	2789	120.88	2789	131.44	2789	136.09	2788	140.07	2787
143.78	2786	147.88	2785	154.19	2784	198.1	2782	205.69	2781
212	2780	213.74	2779	230.55	2778	231.24	2778	246.2	2779
267.09	2779	267.09	2785						

Manning's n Values			num=	3
Sta	n Val	Sta	n Val	Sta
0	.035	56.83	.03	212
				.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	0	267.09		181.6	103		.1	.3

Blocked Obstructions num= 2
 Sta L Sta R Elev Sta L Sta R Elev
 0 60.71 2783 0 60.71 2780

CROSS SECTION

RIVER: Unnamed Lateral
 REACH: Lateral 1 RS: 5200

INPUT

Description:

Station Elevation Data num= 25

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2778	.01	2778	6.64	2777	64.28	2777	65.78	2778
78.35	2779	102.26	2779	109.54	2778	111.21	2777	112.94	2776
121.87	2774	126.21	2773	140.34	2772	167.67	2772	170.61	2773
173.68	2774	176.47	2775	179.06	2776	189.98	2777	210.1	2777
217.68	2777	237.76	2777	243.02	2777	246.61	2777	246.61	2780

Manning's n Values num= 6

Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.035	65.78	.03	109.54	.035	112.94	.04	179.06	.035
246.61	.035								

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	0	246.61		101.72	101.18		.1	.3
					99.54			

CROSS SECTION

RIVER: Unnamed Lateral
 REACH: Lateral 1 RS: 5100

INPUT

Description:

Station Elevation Data num= 31

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2778.55	5.55	2776	7.72	2775	28.24	2774	43.78	2773
56.32	2772	71.95	2771	86.42	2770	96.57	2769	104.89	2768
117.08	2767	128.49	2766	139.73	2765	153.97	2764	179.84	2764
183.7	2765	186.61	2766	189.33	2767	191.36	2768	194.16	2769
197.58	2770	200.46	2771	203	2772	206.01	2773	211.83	2774
215.87	2775	241.04	2775	245.71	2774	257.55	2774	263.63	2774
263.63	2780								

Manning's n Values num= 4

Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.035	56.32	.04	203	.035	263.63	.035

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	0	263.63		49.87	50.66		.1	.3
					49.68			

CROSS SECTION

RIVER: Unnamed Lateral
 REACH: Lateral 1 RS: 5000

INPUT

Description:

Station Elevation Data num= 33

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2776	1.02	2776	3.79	2775	32.75	2774	53.22	2773
70.53	2772	92.22	2771	110.68	2770	116.83	2769	121.85	2768
127.31	2767	130.63	2766	133.74	2765	136.6	2764	143.25	2763
149.02	2762	153.27	2761	157.12	2759.39	177.14	2759.39	181.95	2761
185.81	2762	191.56	2763	195.69	2764	199.22	2765	202.35	2766
205.46	2767	208.48	2768	211.28	2769	214.18	2770	217.33	2771
223.48	2772	267.37	2772	267.37	2776				

Manning's n Values		num= 3	
Sta	n Val	Sta	n Val
0	.035	70.53	.04
		223.48	.035

Bank Sta:	Left	Right	Coeff	Contr.	Expan.
	0	267.37		.3	.5

SUMMARY OF MANNING'S N VALUES

River: Unnamed Lateral

Reach	River Sta.	n1	n2	n3	n4	n5	n6
Lateral 1	5400	.035	.03	.035			
Lateral 1	5300	.035	.03	.035			
Lateral 1	5200	.035	.03	.035	.04	.035	.035
Lateral 1	5100	.035	.04	.035	.035		
Lateral 1	5000	.035	.04	.035			

SUMMARY OF REACH LENGTHS

River: Unnamed Lateral

Reach	River Sta.	Left	Channel	Right
Lateral 1	5400	211	96	93.25
Lateral 1	5300	181.6	103	49.77
Lateral 1	5200	101.72	101.18	99.54
Lateral 1	5100	49.87	50.66	49.68
Lateral 1	5000			

SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS

River: Unnamed Lateral

Reach	River Sta.	Contr.	Expan.
Lateral 1	5400	.1	.3
Lateral 1	5300	.1	.3
Lateral 1	5200	.1	.3
Lateral 1	5100	.1	.3
Lateral 1	5000	.3	.5

ERRORS WARNINGS AND NOTES

Errors Warnings and Notes for Plan : Current mode

River: Unnamed Lateral Reach: Lateral 1 RS: 5300 Profile: PF 1

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

River: Unnamed Lateral Reach: Lateral 1 RS: 5200 Profile: PF 1

Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Note: Manning's n values were composited to a single value in the main channel.

River: Unnamed Lateral Reach: Lateral 1 RS: 5100 Profile: PF 1

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

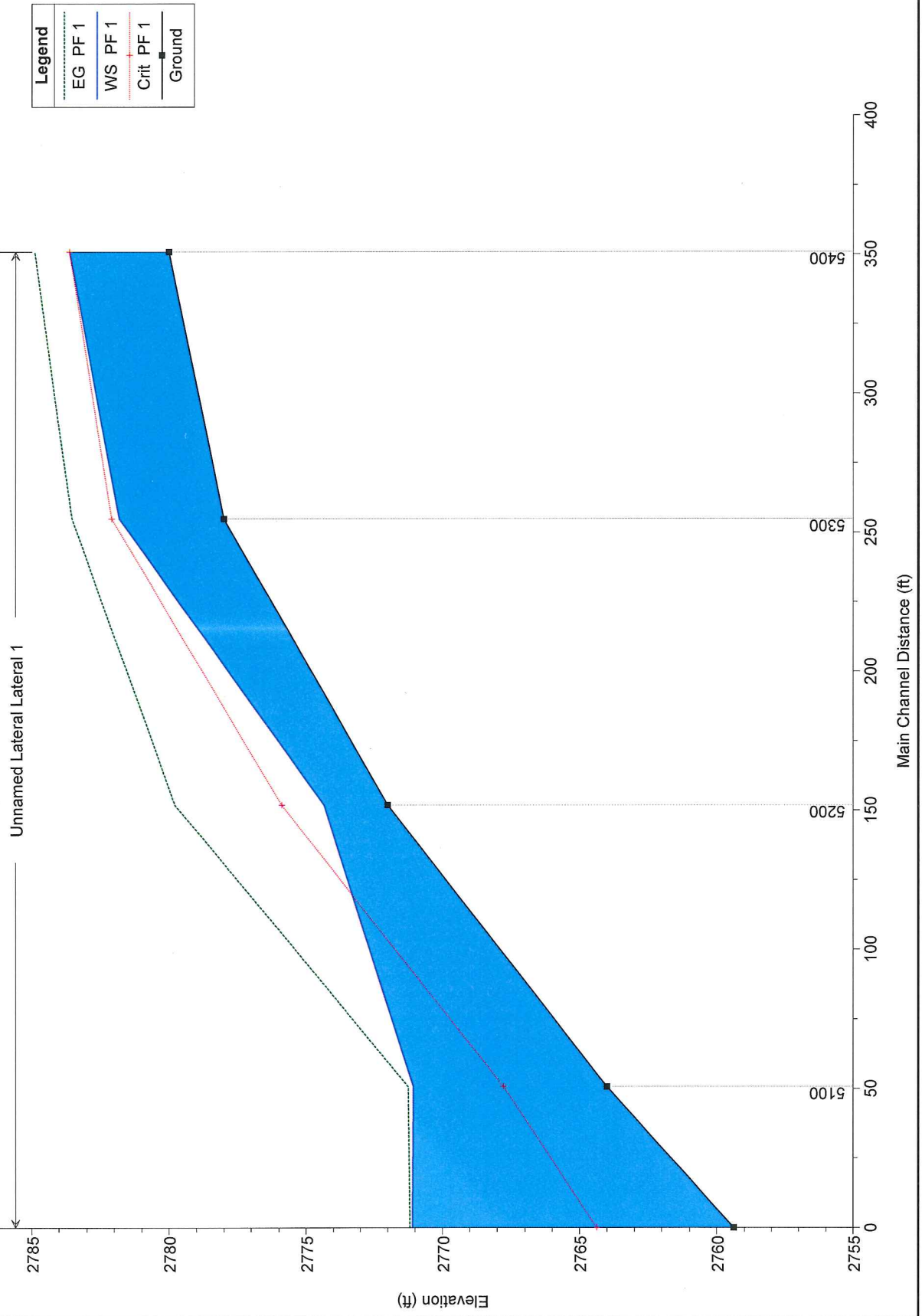
This may indicate the need for additional cross sections.

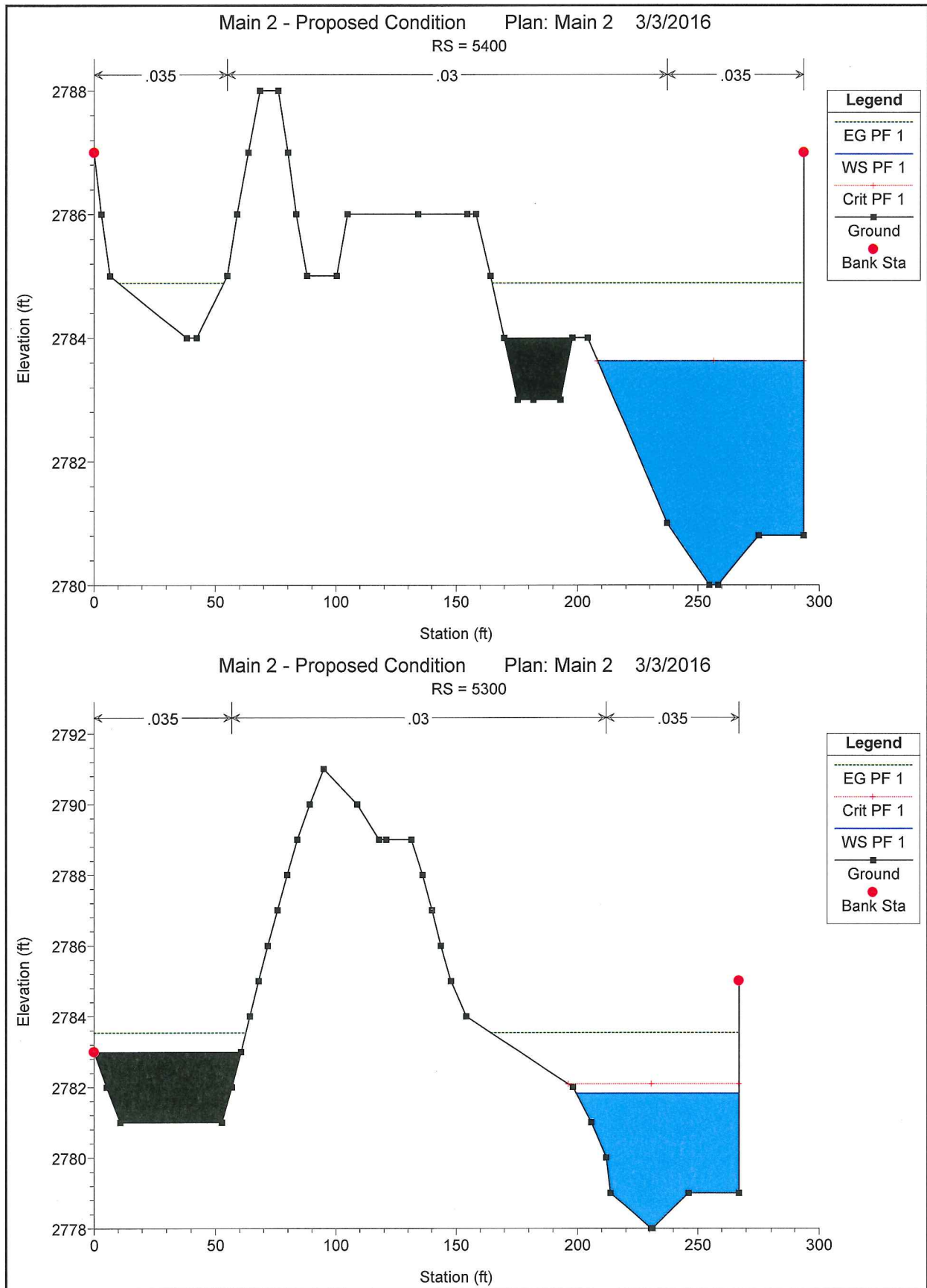
Note: Hydraulic jump has occurred between this cross section and the previous upstream section.

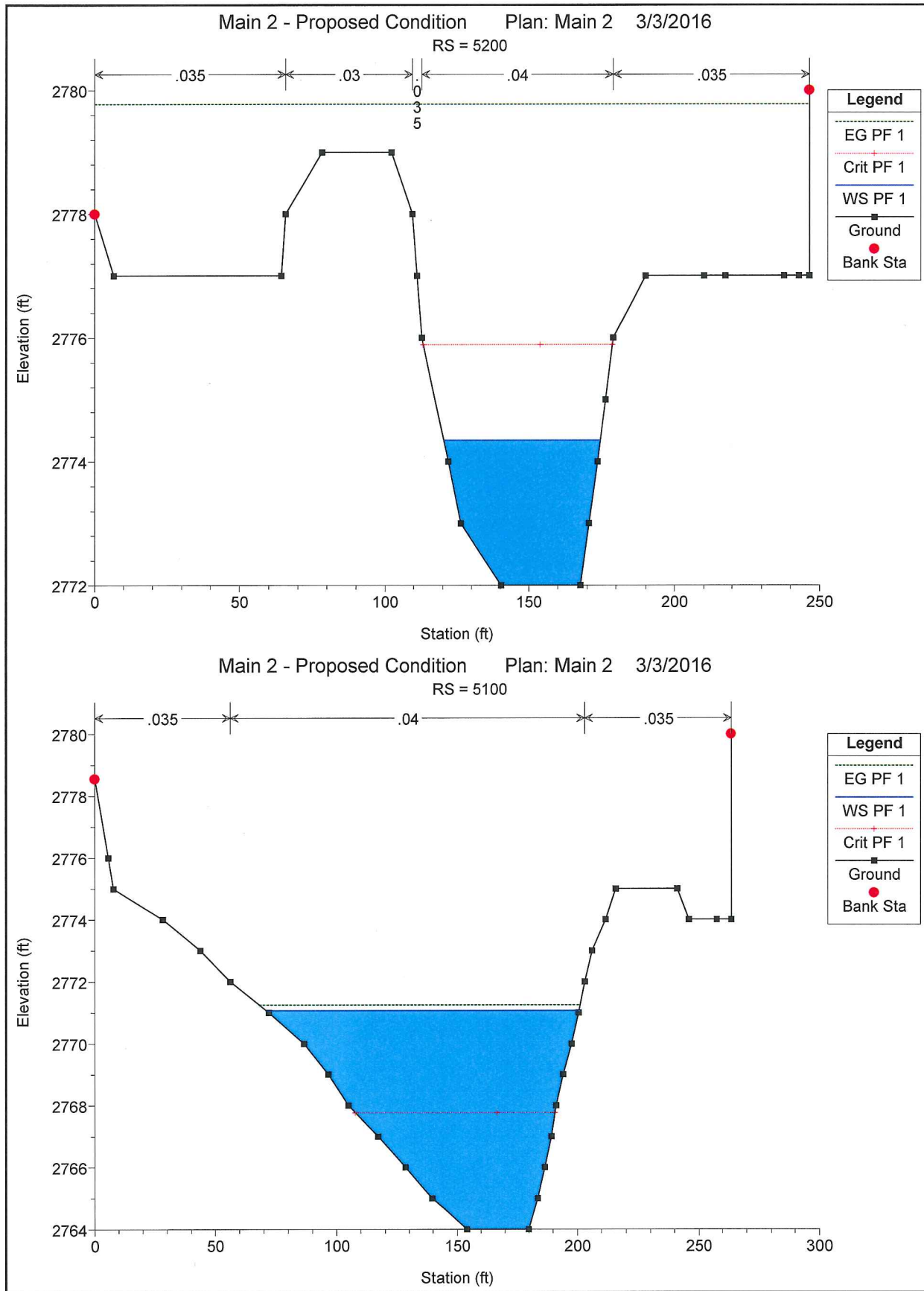
HEC-RAS Plan: Current mode River: Unnamed Lateral Reach: Lateral 1 Profile: PF 1

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Lateral 1	5400	PF 1	1910.00	2780.00	2783.62	2783.62	2784.89	0.012079	9.02	211.82	85.32	1.01
Lateral 1	5300	PF 1	1910.00	2778.00	2781.81	2782.08	2783.53	0.015570	10.53	181.35	67.56	1.13
Lateral 1	5200	PF 1	1910.00	2772.00	2774.34	2775.89	2779.78	0.110770	18.71	102.10	54.29	2.40
Lateral 1	5100	PF 1	1910.00	2764.00	2771.06	2767.76	2771.25	0.001256	3.44	554.72	129.63	0.29
Lateral 1	5000	PF 1	1910.00	2759.39	2771.09	2764.36	2771.19	0.000416	2.48	771.61	127.62	0.18

Main 2 - Proposed Condition Plan: Main 2 3/3/2016



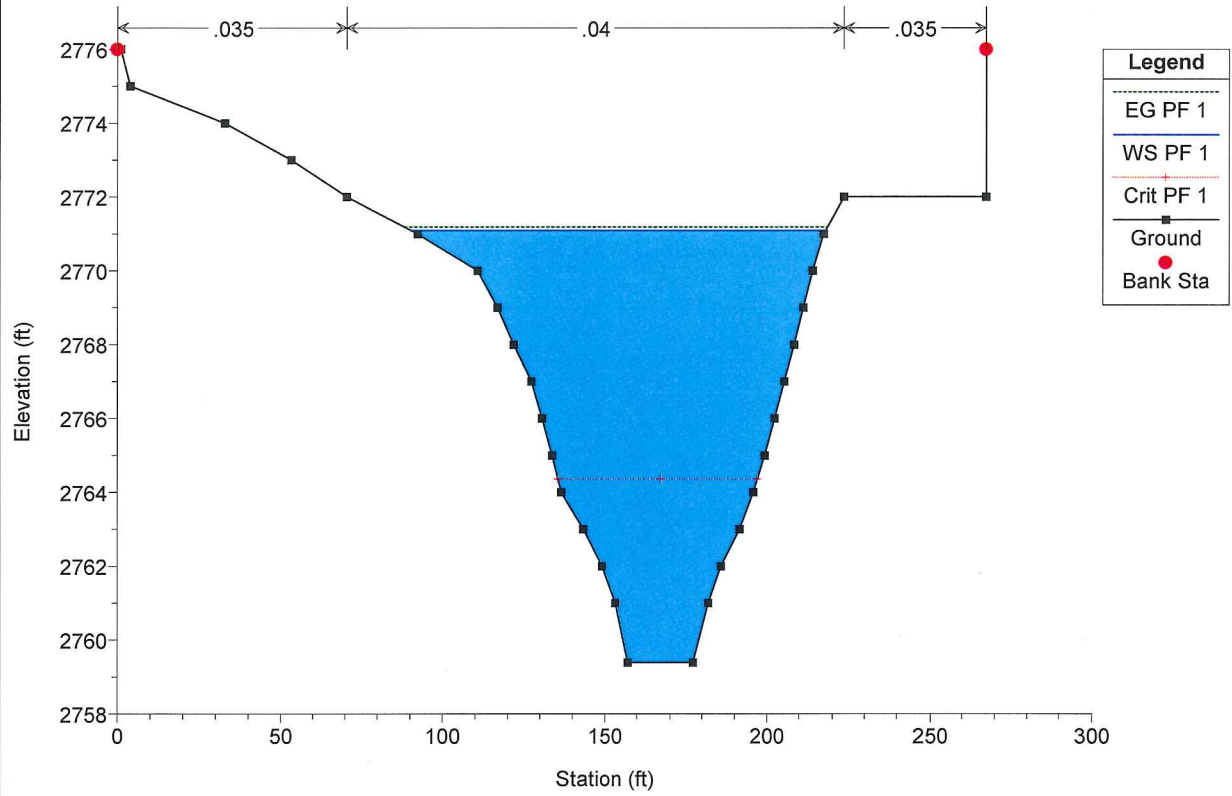




Main 2 - Proposed Condition

Plan: Main 2 3/3/2016

RS = 5000



PROPOSED NDOT TYPE 2 DROP INLET W/ 18" RCP

FACILITY #2

	WEIR		ORIFICE
Q100 =	<u>1</u>	Q100 =	<u>1</u>
L =	<u>8.69</u>	CLEAR AREA =	<u>3.5</u>
		C =	<u>0.65</u>
CLOGGING FACTOR	<u>50%</u>	CLOGGING FACTOR	<u>50%</u>
ASSUME H1 =	<u>0.19</u>	ASSUME H1 =	<u>0.19</u>
C (FOR H1) =	<u>2.7</u>		
$Q_F = CL(H)^{3/2}$	<div>1.0</div>	$Q = CA(64.4 H)^{1/2}$	<div>6.1</div>
	CONTROL =	WEIR	
	Q INT =	<div>1.0</div>	

Note: H1 is measured from the top of the grate. Orifice calculations accounts for the 3-inch thickness of the grate

PIPE CULVERT

57B-1A: 48-inch RCP

INPUT

Pipe Diameter	48 in
Number of Pipes	1
Length	355.0 ft
Slope	6.13 %
Manning's 'n'	0.013
Flow "Q"	54 cfs
Entrance Coef.	0.35
Tail Water	0 ft

INLET

Thin Edge	3.41 ft
Sq. Edge	3.16 ft
Beveled	3.03 ft
Tapered	3.27 ft.

OUTLET

Head Water	N/A ft
Critical	2.21 ft
Velocity	4.30 ft/s



G. C. WALLACE COMPANIES
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PIPE CULVERT

DON1: 48-INCH RCP

INPUT

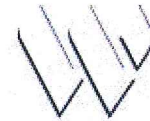
Pipe Diameter	48 in
Number of Pipes	1
Length	30.0 ft
Slope	3.57 %
Manning's 'n'	0.013
Flow "Q"	34 cfs
Entrance Coef.	0.35
Tail Water	0 ft

INLET

Thin Edge	2.53 ft
Sq. Edge	2.39 ft
Beveled	2.34 ft
Tapered	2.53 ft.

OUTLET

Head Water	N/A ft
Critical	1.73 ft
Velocity	2.71 ft/s



G. C. WALLACE COMPANIES
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PIPE CULVERT

DON2: 48-inch RCP

INPUT

Pipe Diameter	48 in
Number of Pipes	1
Length	30.0 ft
Slope	3.57 %
Manning's 'n'	0.013
Flow "Q"	60 cfs
Entrance Coef.	0.35
Tail Water	0 ft

INLET

Thin Edge	3.73 ft
Sq. Edge	3.45 ft
Beveled	3.29 ft
Tapered	3.46 ft.

OUTLET

Head Water	N/A ft
Critical	2.33 ft
Velocity	4.77 ft/s



G. C. WALLACE COMPANIES
ENGINEERS | PLANNERS | SURVEYORS

PIPE CULVERT

1/4 DON3: 24-INCH RCP

INPUT

Pipe Diameter	24 in
Number of Pipes	1
Length	127.0 ft
Slope	0.30 %
Manning's 'n'	0.013
Flow "Q"	16 cfs
Entrance Coef.	0.35
Tail Water	0 ft

INLET

Thin Edge	2.58 ft
Sq. Edge	2.37 ft
Beveled	2.20 ft
Tapered	2.20 ft.

OUTLET

Head Water	2.52 ft
Critical	1.44 ft
Velocity	5.09 ft/s



G. C. WALLACE COMPANIES
ENGINEERS | PLANNERS | SURVEYORS

PIPE CULVERT

DON3: 48-INCH RCP

INPUT

Pipe Diameter	48 in
Number of Pipes	1
Length	30.0 ft
Slope	2.00 %
Manning's 'n'	0.013
Flow "Q"	33 cfs
Entrance Coef.	0.35
Tail Water	0 ft

INLET

Thin Edge	2.52 ft
Sq. Edge	2.38 ft
Beveled	2.33 ft
Tapered	2.48 ft.

OUTLET

Head Water	N/A ft
Critical	1.71 ft
Velocity	2.63 ft/s



G. C. WALLACE COMPANIES
ENGINEERS | PLANNERS | SURVEYORS

PIPE CULVERT

DON3: 48-INCH RCP

INPUT

Pipe Diameter	48 in
Number of Pipes	1
Length	30.0 ft
Slope	2.00 %
Manning's 'n'	0.013
Flow "Q"	38 cfs
Entrance Coef.	0.35
Tail Water	0 ft

INLET

Thin Edge	2.76 ft
Sq. Edge	2.59 ft
Beveled	2.52 ft
Tapered	2.69 ft.

OUTLET

Head Water	N/A ft
Critical	1.84 ft
Velocity	3.02 ft/s



G. C. WALLACE COMPANIES
ENGINEERS | PLANNERS | SURVEYORS

PIPE CULVERT

DON4

INPUT

Pipe Diameter	36 in
Number of Pipes	1
Length	30.0 ft
Slope	2.00 %
Manning's 'n'	0.013
Flow "Q"	22 cfs
Entrance Coef.	0.35
Tail Water	0 ft

INLET

Thin Edge	2.32 ft
Sq. Edge	2.17 ft
Beveled	2.09 ft
Tapered	2.22 ft.

OUTLET

Head Water	N/A ft
Critical	1.51 ft
Velocity	3.11 ft/s



G. C. WALLACE COMPANIES
ENGINEERS | PLANNERS | SURVEYORS

PIPE CULVERT

CON3R: 72-inch RCP

INPUT

Pipe Diameter	72 in
Number of Pipes	1
Length	115.7 ft
Slope	1.00 %
Manning's 'n'	0.013
Flow "Q"	191 cfs
Entrance Coef.	0.35
Tail Water	0 ft

INLET

Thin Edge	6.29 ft
Sq. Edge	5.81 ft
Beveled	5.50 ft
Tapered	5.63 ft.

OUTLET

Head Water	4.92 ft
Critical	3.77 ft
Velocity	6.76 ft/s



G. C. WALLACE COMPANIES
ENGINEERS | PLANNERS | SURVEYORS

BOX CULVERT

CCON10_20x9RCB

INPUT

Width of Box	20.00 ft
Height of Box	9.00 ft
Number of Barrels	1
Length	50.00 ft
Slope	0.99 %
Manning's 'n'	0.015
Flow "Q"	2128 cfs
Entrance Coef.	0.35
Tail Water	0 ft

Non Standard Box Span

INLET

45d WWall	12.08 ft
Sq. Edge	12.72 ft
Beveled	11.71 ft
Tapered	58.70 ft

OUTLET

Head Water	10.62 ft
Critical	7.06 ft
Velocity	11.82 ft/s



G. C. WALLACE COMPANIES
ENGINEERS | PLANNERS | SURVEYORS

PIPE CULVERT

CON15R: 72-inch RCP

INPUT

Pipe Diameter	72 in
Number of Pipes	1
Length	92.9 ft
Slope	1.14 %
Manning's 'n'	0.013
Flow "Q"	344 cfs
Entrance Coef.	0.35
Tail Water	0 ft

INLET

Thin Edge	11.39 ft
Sq. Edge	9.88 ft
Beveled	8.85 ft
Tapered	8.27 ft.

OUTLET

Head Water	8.17 ft
Critical	5.03 ft
Velocity	12.17 ft/s



G. C. WALLACE COMPANIES
ENGINEERS | PLANNERS | SURVEYORS

BOX CULVERT

CON18R_20x9RCB

INPUT

Width of Box	20.00 ft
Height of Box	9.00 ft
Number of Barrels	1
Length	18.23 ft
Slope	9.59 %
Manning's 'n'	0.015
Flow "Q"	1910 cfs
Entrance Coef.	0.35
Tail Water	0 ft

Non Standard Box Span

INLET

45d WWall	10.26 ft
Sq. Edge	10.85 ft
Beveled	9.92 ft
Tapered	42.32 ft

OUTLET

Head Water	8.44 ft
Critical	6.57 ft
Velocity	10.61 ft/s



G. C. WALLACE COMPANIES
ENGINEERS | PLANNERS | SURVEYORS

PIPE CULVERT

ON16R: 48-inch RCP

INPUT

Pipe Diameter	48 in
Number of Pipes	1
Length	96.1 ft
Slope	0.50 %
Manning's 'n'	0.013
Flow "Q"	23 cfs
Entrance Coef.	0.35
Tail Water	0 ft

INLET

Thin Edge	2.04 ft
Sq. Edge	1.96 ft
Beveled	1.93 ft
Tapered	2.03 ft.

OUTLET

Head Water	N/A ft
Critical	1.41 ft
Velocity	1.83 ft/s



G. C. WALLACE COMPANIES
ENGINEERS | PLANNERS | SURVEYORS

BOX CULVERT

CON22: Existing (2)12x12RCB

INPUT

Width of Box	12.00 ft
Height of Box	12.00 ft
Number of Barrels	2
Length	100.00 ft
Slope	1.00 %
Manning's 'n'	0.013
Flow "Q"	4209 cfs
Entrance Coef.	0.35
Tail Water	0 ft

INLET

45d WWall	17.07 ft
Sq. Edge	18.08 ft ←
Beveled	16.49 ft
Tapered	15.40 ft

OUTLET

Head Water	14.78 ft
Critical	12.00 ft
Velocity	14.61 ft/s



G. C. WALLACE COMPANIES
ENGINEERS | PLANNERS | SURVEYORS

$$\begin{array}{r} \text{INV} = 2666.75 \\ 18.08 \\ \hline 2684.83 \text{ WSE} \end{array}$$

design data 7

depth to top of pipe,
not invert

american
concrete
Pipe
association

CONCRETE PIPE SELECTION: Trench Installations

Trench conduits are usually installed in relatively narrow trenches excavated in undisturbed soil and backfilled to the original ground surface.

When a rigid conduit is installed in a narrow trench and backfilled, the backfill material will tend to settle. This downward movement generates frictional forces along the trench walls, which act upward to help support the weight of the backfill material. The magnitude of the frictional forces depends on the unit weight of the backfill material w , the value of Rankine's lateral pressure ratio K , and the coefficient of sliding friction μ between the backfill material and the trench walls.

The backfill load on a conduit installed in a trench condition is equal to the weight of the mass of fill material within the trench less the summation of the frictional load transfers, and is expressed by the equation:

$$W_d = C_d w B_d$$

where

W_d = backfill load, pounds per linear foot

C_d = load coefficient for trench condition

w = unit weight of backfill material, pounds per cubic foot

B_d = width of trench at the top of the conduit, feet

Figures 2 through 5, based on the above equation, enable a direct determination of backfill load for a given trench width and depth of cover. As the trench width increases for a given depth of cover and pipe diameter, a point is reached at which an embankment condition develops. The curves showing pipe size indicate the limiting trench width for each pipe diameter beyond which greater trench widths will not affect the load. When this condition occurs, the load on the conduit remains constant. This load should be determined by the intersection of the vertical line representing the depth of cover and the dashed line representing the particular pipe diameter under consideration. For intermediate pipe sizes not shown in Figures 2 through 5, interpolation should be used.

The field supporting strength of a concrete pipe line is dependent on the inherent strength of the pipe, the type of foundation on which the pipe is installed and the compaction of the sidefill material adjacent to the pipe. A common method used to determine the inherent strength of a pipe is the three-edge bearing test, in which the pipe is subjected to concentrated loads at the crown and invert. The load that a pipe will support under this condition of loading is called the *three-edge bearing strength* and is expressed in pounds per linear foot.

ASTM Specification C14 covers three strength classes for non-reinforced concrete pipe — Class 1, 2 and 3. These three classes are specified to meet ultimate loads, expressed in terms of minimum strength in three-edge-bearing as listed in Table I.

TABLE I: Strength Requirements Non-reinforced Concrete Pipe ASTM C14

Pipe Diameter, inches	Minimum Three-Edge Bearing Strengths, Pounds per Linear Foot		
	Class 1	Class 2	Class 3
4	1500	2000	2400
6	1500	2000	2400
8	1500	2000	2400
10	1600	2000	2400
12	1800	2250	2600
15	2000	2600	2900
18	2200	3000	3300
21	2400	3300	3850
24	2600	3600	4400
27	2800	3950	4600
30	3000	4300	4750
33	3150	4400	4875
36	3300	4500	5000

Another means of expressing pipe strength is in terms of D-load. The D-load of a pipe is the supporting strength of a pipe loaded under three-edge-bearing test conditions expressed in pounds per linear foot per foot of inside diameter. Thus the bearing strength may be converted to D-load by dividing by the inside diameter in feet.

ASTM Specification C76 specifies five strength classes reinforced concrete pipe. These strength classes are expressed in terms of D-load at 0.01-inch crack and for ultimate load. The D-load to produce the 0.01-inch crack $D_{0.01}$ is the maximum load applied to the concrete pipe before a crack occurs having a width of 0.01-inch measured at close intervals, throughout a length of at least 1-foot. The D-load to produce ultimate load D_u is the maximum three-edge-bearing test load carried by a pipe, expressed as D-load. Table II lists 0.01-inch crack and ultimate D-loads for the strength classes covered by ASTM Specification C76.

TABLE II: Strength Requirements Reinforced Concrete Pipe ASTM C76

Strength Class	Minimum D-Load in Three-Edge Bearing Pounds per Linear Foot per Foot of Internal Diameter	
	0.01 Inch Crack- $D_{0.01}$	Ultimate- D_u
I	800	1200
II	1000	1500
III	1350	2000
IV	2000	3000
V	3000	3750

Class III 0-1350
Class IV 1350-2000
Class V 2000-3000

PROGRAM SAMM

D-LOAD REQUIREMENTS FOR A 24 IN. DIAMETER CIRCULAR PIPE

 P I P E D A T A

DIAMETER (in.)	24.00
WALL B, THICKNESS (in.)	3.000

I N S T A L L A T I O N C O N D I T I O N S

MINIMUM DEPTH OF FILL (ft.)	1.00
MAXIMUM DEPTH OF FILL (ft.)	20.00
SOIL DENSITY (lb/cu. ft.)	140.0
SPECIFIED BEDDING FACTOR	1.90
INSTALLATION TYPE	TRENCH
TRENCH WIDTH (ft.)	6.50
SOIL LATERAL PRESSURE/FRICTION TERM (KMU')	0.0165
PARAMETERS TO COMPUTE TRANSITION WIDTH	
POSITIVE PROJECTION RATIO	1.00
POSITIVE SETTLEMENT RATIO	0.50
SOIL LATERAL PRESSURE/FRICTION TERM (KMU)	0.1924
SOIL LATERAL PRESSURE COEFFICIENT	0.33

A D D I T I O N A L L O A D S

LIVE LOAD	AASHTO HS-20
NO SURCHARGE LOAD	

F A C T O R S O F S A F E T Y

FACTOR OF SAFETY ON 0.01 INCH CRACK D-LOAD (EARTH,LIVE)	1.00; 1.00
FACTOR OF SAFETY ON ULTIMATE LOAD (EARTH,LIVE) IN ACCORDANCE WITH ASTM C 76	
DL.01 LESS THAN 2000 LBS/FT/FT	1.5
DL.01 GREATER THAN 3000 LBS/FT/FT	1.25
DL.01 BETWEEN 2000 AND 3000 LBS/FT/FT	INTERPOLATED

RESULTS OF ANALYSIS

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SSSSSSSSS  AAAAAAAAA  MMM  MMM  MMM  MMM
SS          AA    AA    MM M M MM  MM M M MM
SSSSSSSSS  AAAAAAAAA  MM  M  MM  MM  M  MM
          SS  AA    AA  MM    MM  MM    MM
SSSSSSSSS  AA    AA  MM    MM  MM    MM

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PROGRAM SAMM

AMERICAN CONCRETE PIPE ASSOCIATION
VERSION 2.0 - 1 SEPTEMBER 1990

Program SAMM computes earth loads on concrete pipe in accordance with the methods presented in the Concrete Pipe Design Manual (March 1990) and the Concrete Pipe Handbook (January 1988), published by the American Concrete Pipe Association. The user must select input values suitable to his specific installation. The information presented in the computer output is for review, interpretation, application and approval by a qualified engineer who must assume full responsibility for verifying that said output is appropriate and correct. There are no express or implied warranties. The use of this product does not constitute endorsement by ACPA or any other agents.

PIPE DEPTH (ft.)	-----EARTH LOAD-----			LIVE	SURCH	TOTAL	BED	REQUIRED D-LOAD	
	ARCHING	>TRANS	LOAD	LOAD	LOAD	LOAD	FACT	0.01 in. ULT.	
(ft.)	FACTOR		(lb/ft)	(lb/ft)	(lb/ft)	(lb/ft)		(lb/ft/ft)	
1.0	1.08	Y	378.	3008.	0.	3386.	1.90	891.	1337.
1.5	1.12	Y	591.	2400.	0.	2991.	1.90	787.	1181.
2.0	1.17	Y	820.	1781.	0.	2600.	1.90	684.	1026.
2.5	1.22	Y	1067.	1269.	0.	2336.	1.90	615.	922.
3.0	1.27	Y	1334.	927.	0.	2261.	1.90	595.	893.
3.5	1.33	Y	1623.	763.	0.	2386.	1.90	628.	942.
4.0	1.38	Y	1935.	641.	0.	2575.	1.90	678.	1017.
4.5	1.44	Y	2272.	546.	0.	2818.	1.90	742.	1112.
5.0	1.46	Y	2562.	472.	0.	3034.	1.90	798.	1197.
5.5	1.47	Y	2827.	412.	0.	3239.	1.90	852.	1278.
6.0	1.47	Y	3091.	363.	0.	3454.	1.90	909.	1363.
6.5	1.47	Y	3356.	322.	0.	3678.	1.90	968.	1452.
7.0	1.48	Y	3625.	288.	0.	3913.	1.90	1030.	1545.
7.5	1.48	Y	3889.	260.	0.	4149.	1.90	1092.	1638.
8.0	1.48	Y	4153.	235.	0.	4388.	1.90	1155.	1732.
8.5	1.48	Y	4417.	214.	0.	4631.	1.90	1219.	1828.
9.0	1.49	Y	4682.	195.	0.	4877.	1.90	1283.	1925.
9.5	1.49	Y	4946.	179.	0.	5125.	1.90	1349.	2023.
10.0	1.49	Y	5210.	165.	0.	5375.	1.90	1414.	2122.
10.5	1.49	Y	5474.	152.	0.	5627.	1.90	1481.	2221.
11.0	1.49	Y	5738.	141.	0.	5880.	1.90	1547.	2321.
11.5	1.49	Y	6003.	131.	0.	6134.	1.90	1614.	2421.
12.0	1.49	Y	6267.	122.	0.	6389.	1.90	1681.	2522.
12.5	1.49	Y	6531.	114.	0.	6645.	1.90	1749.	2623.
13.0	1.49	Y	6795.	107.	0.	6902.	1.90	1816.	2725.
13.5	1.49	Y	7060.	100.	0.	7160.	1.90	1884.	2826.

IV

14.0	1.49	Y	7324.	94.	0.	7418.	1.90	1952.	2928.
14.5	1.50	Y	7588.	89.	0.	7677.	1.90	2020.	3020.
15.0	1.50	Y	7853.	84.	0.	7937.	1.90	2089.	3087.
15.5	1.50	Y	8117.	79.	0.	8196.	1.90	2157.	3151.
16.0	1.49	Y	8369.	75.	0.	8444.	1.90	2222.	3210.
16.5	1.49	Y	8633.	71.	0.	8704.	1.90	2291.	3269.
17.0	1.50	Y	8897.	68.	0.	8964.	1.90	2359.	3327.
17.5	1.50	Y	9160.	64.	0.	9225.	1.90	2428.	3382.
18.0	1.50	Y	9424.	61.	0.	9485.	1.90	2496.	3435.
18.5	1.50	Y	9688.	58.	0.	9746.	1.90	2565.	3485.
19.0	1.50	Y	9952.	56.	0.	10008.	1.90	2634.	3533.
19.5	1.50	Y	10216.	53.	0.	10269.	1.90	2702.	3579.
20.0	1.50	Y	10480.	51.	0.	10530.	1.90	2771.	3622.

PROGRAM SAMM-

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DESIGNER:

PAGE 2

PROGRAM SAMM-

PROGRAM SAMM

D-LOAD REQUIREMENTS FOR A 36 IN. DIAMETER CIRCULAR PIPE

P I P E D A T A

DIAMETER (in.)	36.00
WALL B, THICKNESS (in.)	4.000

I N S T A L L A T I O N C O N D I T I O N S

MINIMUM DEPTH OF FILL (ft.)	1.00
MAXIMUM DEPTH OF FILL (ft.)	20.00
SOIL DENSITY (lb/cu. ft.)	140.0
SPECIFIED BEDDING FACTOR	1.90
INSTALLATION TYPE	TRENCH
TRENCH WIDTH (ft.)	7.67
SOIL LATERAL PRESSURE/FRICTION TERM (KMU')	0.1650
PARAMETERS TO COMPUTE TRANSITION WIDTH	
POSITIVE PROJECTION RATIO	1.00
POSITIVE SETTLEMENT RATIO	0.50
SOIL LATERAL PRESSURE/FRICTION TERM (KMU)	0.1650
SOIL LATERAL PRESSURE COEFFICIENT	0.33

A D D I T I O N A L L O A D S

LIVE LOAD
NO SURCHARGE LOAD

AASHTO HS-20

F A C T O R S O F S A F E T Y

FACTOR OF SAFETY ON 0.01 INCH CRACK D-LOAD (EARTH, LIVE)	1.00;	1.00
FACTOR OF SAFETY ON ULTIMATE LOAD (EARTH, LIVE) IN ACCORDANCE WITH ASTM C 76		1.5
DL.01 LESS THAN 2000 LBS/FT/FT		1.25
DL.01 GREATER THAN 3000 LBS/FT/FT		INTERPOLATED
DL.01 BETWEEN 2000 AND 3000 LBS/FT/FT		

PAGE 3

PROGRAM SAMM-

RESULTS OF ANALYSIS

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SSSSSSSSS  AAAAAAAAAA  MMM  MMM  MMM  MMM
SS          AA          MM M M MM  MM M M MM
SSSSSSSSS  AAAAAAAAAA  MM  M  MM  MM  M  MM
SS          AA          MM          MM  MM  MM
SSSSSSSSS  AA          MM          MM  MM  MM

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PROGRAM SAMM

AMERICAN CONCRETE PIPE ASSOCIATION
VERSION 2.0 - 1 SEPTEMBER 1990

Program SAMM computes earth loads on concrete pipe in accordance with the methods presented in the Concrete Pipe Design Manual (March 1990) and the Concrete Pipe Handbook (January 1988), published by the American Concrete Pipe Association. The user must select input values suitable to his specific installation. The information presented in the computer output is for review, interpretation, application and approval by a qualified engineer who must assume full responsibility for verifying that said output is appropriate and correct. There are no express or implied warranties. The use of this product does not constitute endorsement by ACPA or any other agents.

PIPE DEPTH (ft.)	-----EARTH LOAD----- ARCHING >TRANS FACTOR	LOAD (lb/ft)	LIVE LOAD (lb/ft)	SURCH LOAD (lb/ft)	TOTAL LOAD (lb/ft)	BED FACT	REQUIRED D-LOAD 0.01 in. ULT. (lb/ft/ft)
1.0	1.05 Y	537.	2814.	0.	3351.	1.90	588. 882.
2.0	1.10 Y	1125.	2326.	0.	3450.	1.90	605. 908.
3.0	1.15 Y	1768.	1227.	0.	2995.	1.90	525. 788.
4.0	1.20 Y	2472.	857.	0.	3329.	1.90	584. 876.
5.0	1.26 Y	3241.	637.	0.	3878.	1.90	680. 1021.
6.0	1.33 Y	4084.	494.	0.	4577.	1.90	803. 1205.
7.0	1.39 Y	5006.	395.	0.	5400.	1.90	947. 1421.
8.0	1.43 Y	5871.	323.	0.	6194.	1.90	1087. 1630.
9.0	1.43 Y	6630.	270.	0.	6899.	1.90	1210. 1816.
10.0	1.44 Y	7387.	229.	0.	7616.	1.90	1336. 2004.
11.0	1.44 Y	8154.	197.	0.	8351.	1.90	1465. 2198.
12.0	1.45 Y	8911.	171.	0.	9082.	1.90	1593. 2390.
13.0	1.45 Y	9668.	150.	0.	9817.	1.90	1722. 2584.
14.0	1.45 Y	10424.	132.	0.	10557.	1.90	1852. 2778.
15.0	1.45 Y	11181.	118.	0.	11298.	1.90	1982. 2973.
16.0	1.45 Y	11937.	106.	0.	12043.	1.90	2113. 3110.
17.0	1.45 Y	12693.	95.	0.	12789.	1.90	2244. 3229.
18.0	1.46 N	13446.	86.	0.	13533.	1.90	2374. 3339.
19.0	1.43 N	13930.	79.	0.	14009.	1.90	2458. 3405.
20.0	1.40 N	14394.	72.	0.	14466.	1.90	2538. 3466.

PROGRAM SAMM-

PAGE 1

DATE: / /

DESIGNER:

SSSSSSSSS	AAAAAAAAA	MMM	MMM	MMM	MMM
SS	AA AA	MM M M MM	MM M M MM		
SSSSSSSSS	AAAAAAAAA	MM M MM	MM M MM		
SS	AA AA	MM MM	MM MM		
SSSSSSSSS	AA AA	MM MM	MM MM		

P R O G R A M S A M M

AMERICAN CONCRETE PIPE ASSOCIATION
VERSION 2.0 - 1 SEPTEMBER 1990

Program SAMM computes earth loads on concrete pipe in accordance with the methods presented in the Concrete Pipe Design Manual (March 1990) and the Concrete Pipe Handbook (January 1988), published by the American Concrete Pipe Association. The user must select input values suitable to his specific installation. The information presented in the computer output is for review, interpretation, application and approval by a qualified engineer who must assume full responsibility for verifying that said output is appropriate and correct. There are no express or implied warranties. The use of this product does not constitute endorsement by ACPA or any other agents.

DATE:

DESIGNER:

PROGRAM SAMM

D-LOAD REQUIREMENTS FOR A 48 IN. DIAMETER CIRCULAR PIPE

 PIPE DATA

DIAMETER (in.)	48.00
WALL B, THICKNESS (in.)	5.000

INSTALLATION CONDITIONS

MINIMUM DEPTH OF FILL (ft.)	0.50
MAXIMUM DEPTH OF FILL (ft.)	20.00
SOIL DENSITY (lb/cu. ft.)	140.0
SPECIFIED BEDDING FACTOR	1.90
INSTALLATION TYPE	TRENCH
TRENCH WIDTH (ft.)	8.83
SOIL LATERAL PRESSURE/FRICTION TERM (KMU')	0.1650
PARAMETERS TO COMPUTE TRANSITION WIDTH	
POSITIVE PROJECTION RATIO	1.00
POSITIVE SETTLEMENT RATIO	0.50
SOIL LATERAL PRESSURE/FRICTION TERM (KMU)	0.1924
SOIL LATERAL PRESSURE COEFFICIENT	0.33

ADDITIONAL LOADS

LIVE LOAD	AASHTO HS-20
NO SURCHARGE LOAD	

FACTORS OF SAFETY

FACTOR OF SAFETY ON 0.01 INCH CRACK D-LOAD (EARTH, LIVE)	1.00; 1.00
FACTOR OF SAFETY ON ULTIMATE LOAD (EARTH, LIVE) IN ACCORDANCE WITH ASTM C 76	
DL.01 LESS THAN 2000 LBS/FT/FT	1.5
DL.01 GREATER THAN 3000 LBS/FT/FT	1.25
DL.01 BETWEEN 2000 AND 3000 LBS/FT/FT	INTERPOLATED

RESULTS OF ANALYSIS

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SSSSSSSSSS  AAAAAAAAAA  MMM  MMM  MMM  MMM
SS           AA    AA    MM M M MM  MM M M MM
SSSSSSSSSS  AAAAAAAAAA  MM  M  MM  MM  M  MM
           SS    AA    MM    MM    MM    MM
SSSSSSSSSS  AA    AA    MM    MM    MM    MM

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PROGRAM SAMM

AMERICAN CONCRETE PIPE ASSOCIATION
VERSION 2.0 - 1 SEPTEMBER 1990

Program SAMM computes earth loads on concrete pipe in accordance with the methods presented in the Concrete Pipe Design Manual (March 1990) and the Concrete Pipe Handbook (January 1988), published by the American Concrete Pipe Association. The user must select input values suitable to his specific installation. The information presented in the computer output is for review, interpretation, application and approval by a qualified engineer who must assume full responsibility for verifying that said output is appropriate and correct. There are no express or implied warranties. The use of this product does not constitute endorsement by ACPA or any other agents.

PIPE DEPTH (ft.)	EARTH LOAD			LIVE LOAD	SURCH LOAD	TOTAL LOAD	BED FACT	REQUIRED D-LOAD 0.01 in. ULT. (lb/ft/ft)	
	ARCHING FACTOR	>TRANS Y	LOAD (lb/ft)	(lb/ft)	(lb/ft)	(lb/ft)			
0.5	1.02	Y	345.	2584.	0.	2929.	1.90	385.	578.
1.0	1.04	Y	704.	2331.	0.	3035.	1.90	399.	599.
1.5	1.06	Y	1078.	2623.	0.	3701.	1.90	487.	731.
2.0	1.08	Y	1467.	2475.	0.	3942.	1.90	519.	778.
2.5	1.11	Y	1872.	1994.	0.	3866.	1.90	509.	763.
3.0	1.13	Y	2293.	1474.	0.	3766.	1.90	496.	743.
3.5	1.15	Y	2731.	1226.	0.	3957.	1.90	521.	781.
4.0	1.18	Y	3187.	1039.	0.	4226.	1.90	556.	834.
4.5	1.20	Y	3662.	893.	0.	4555.	1.90	599.	899.
5.0	1.23	Y	4156.	778.	0.	4933.	1.90	649.	974.
5.5	1.25	Y	4670.	684.	0.	5353.	1.90	704.	1057.
6.0	1.28	Y	5204.	606.	0.	5811.	1.90	765.	1147.
6.5	1.31	Y	5761.	542.	0.	6303.	1.90	829.	1244.
7.0	1.34	Y	6340.	487.	0.	6827.	1.90	898.	1348.
7.5	1.37	Y	6943.	441.	0.	7384.	1.90	972.	1457.
8.0	1.40	Y	7570.	401.	0.	7971.	1.90	1049.	1573.
8.5	1.43	Y	8222.	366.	0.	8589.	1.90	1130.	1695.
9.0	1.46	Y	8884.	336.	0.	9220.	1.90	1213.	1820.
9.5	1.46	Y	9394.	309.	0.	9703.	1.90	1277.	1915.
10.0	1.47	Y	9917.	286.	0.	10203.	1.90	1343.	2014.
10.5	1.47	Y	10429.	265.	0.	10694.	1.90	1407.	2111.
11.0	1.47	Y	10940.	246.	0.	11187.	1.90	1472.	2208.
11.5	1.47	Y	11452.	230.	0.	11681.	1.90	1537.	2306.
12.0	1.47	N	11954.	215.	0.	12169.	1.90	1601.	2402.
12.5	1.46	N	12345.	201.	0.	12546.	1.90	1651.	2476.
13.0	1.45	N	12729.	189.	0.	12918.	1.90	1700.	2550.

13.5	1.43	N	13106.	177.	0.	13283.	1.90	1748.	2622.
14.0	1.42	N	13475.	167.	0.	13643.	1.90	1795.	2693.
14.5	1.41	N	13838.	158.	0.	13996.	1.90	1842.	2762.
15.0	1.40	N	14195.	149.	0.	14344.	1.90	1887.	2831.
15.5	1.39	N	14544.	141.	0.	14685.	1.90	1932.	2898.
16.0	1.38	N	14887.	134.	0.	15021.	1.90	1976.	2965.
16.5	1.36	N	15224.	127.	0.	15351.	1.90	2020.	3020.
17.0	1.35	N	15555.	121.	0.	15676.	1.90	2063.	3062.
17.5	1.34	N	15879.	115.	0.	15994.	1.90	2105.	3102.
18.0	1.33	N	16197.	110.	0.	16307.	1.90	2146.	3140.
18.5	1.32	N	16510.	105.	0.	16615.	1.90	2186.	3177.
19.0	1.31	N	16817.	100.	0.	16917.	1.90	2226.	3213.
19.5	1.30	N	17118.	96.	0.	17213.	1.90	2265.	3247.
20.0	1.29	N	17413.	92.	0.	17505.	1.90	2303.	3280.

GRAM SAMM-

PAGE 1

DATE: / /

DESIGNER:

PROGRAM SAMM

D-LOAD REQUIREMENTS FOR A 72 IN. DIAMETER CIRCULAR PIPE

P I P E D A T A

DIAMETER (in.)	72.00
WALL B, THICKNESS (in.)	7.000

I N S T A L L A T I O N C O N D I T I O N S

MINIMUM DEPTH OF FILL (ft.)	1.00
MAXIMUM DEPTH OF FILL (ft.)	25.00
SOIL DENSITY (lb/cu. ft.)	140.0
SPECIFIED BEDDING FACTOR	1.90
INSTALLATION TYPE	TRENCH
TRENCH WIDTH (ft.)	11.17
SOIL LATERAL PRESSURE/FRICTION TERM (KMU')	0.1650
PARAMETERS TO COMPUTE TRANSITION WIDTH	
POSITIVE PROJECTION RATIO	1.00
POSITIVE SETTLEMENT RATIO	0.50
SOIL LATERAL PRESSURE/FRICTION TERM (KMU)	0.1924
SOIL LATERAL PRESSURE COEFFICIENT	0.33

A D D I T I O N A L L O A D S

LIVE LOAD	AASHTO HS-20
NO SURCHARGE LOAD	

F A C T O R S O F S A F E T Y

FACTOR OF SAFETY ON 0.01 INCH CRACK D-LOAD (EARTH, LIVE)	1.00; 1.00
FACTOR OF SAFETY ON ULTIMATE LOAD (EARTH, LIVE) IN ACCORDANCE WITH ASTM C 76	
DL.01 LESS THAN 2000 LBS/FT/FT	1.5
DL.01 GREATER THAN 3000 LBS/FT/FT	1.25
DL.01 BETWEEN 2000 AND 3000 LBS/FT/FT	INTERPOLATED

RESULTS OF ANALYSIS

PIPE DEPTH (ft.)	-----EARTH LOAD----- ARCHING > TRANS FACTOR	LOAD (lb/ft)	LIVE LOAD (lb/ft)	SURCH LOAD (lb/ft)	TOTAL LOAD (lb/ft)	BED FACT	REQUIRED D-LOAD 0.01 in. ULT. (lb/ft/ft)
1.0	1.03 Y	1031.	1735.	0.	2766.	1.90	243.
1.5	1.04 Y	1567.	2580.	0.	4147.	1.90	364.
2.0	1.06 Y	2118.	2185.	0.	4303.	1.90	377.
2.5	1.07 Y	2684.	1810.	0.	4494.	1.90	394.
3.0	1.09 Y	3266.	1574.	0.	4840.	1.90	425.
3.5	1.10 Y	3863.	1509.	0.	5373.	1.90	471.
4.0	1.12 Y	4477.	1327.	0.	5804.	1.90	509.
4.5	1.13 Y	5107.	1148.	0.	6255.	1.90	549.
5.0	1.15 Y	5755.	1005.	0.	6759.	1.90	593.
5.5	1.16 Y	6420.	888.	0.	7308.	1.90	641.
6.0	1.18 Y	7103.	791.	0.	7894.	1.90	692.
6.5	1.20 Y	7805.	710.	0.	8515.	1.90	747.
7.0	1.21 Y	8525.	642.	0.	9167.	1.90	804.
7.5	1.23 Y	9266.	583.	0.	9849.	1.90	864.
8.0	1.25 Y	10026.	532.	0.	10558.	1.90	926.
8.5	1.27 Y	10808.	488.	0.	11295.	1.90	991.
9.0	1.29 Y	11610.	449.	0.	12059.	1.90	1058.
9.5	1.30 Y	12435.	414.	0.	12849.	1.90	1127.
10.0	1.32 Y	13281.	384.	0.	13665.	1.90	1199.
10.5	1.34 N	14117.	357.	0.	14474.	1.90	1270.
11.0	1.33 N	14686.	333.	0.	15019.	1.90	1317.
11.5	1.32 N	15247.	311.	0.	15558.	1.90	1365.
12.0	1.31 N	15800.	291.	0.	16091.	1.90	1411.
12.5	1.30 N	16344.	273.	0.	16618.	1.90	1458.
13.0	1.29 N	16881.	257.	0.	17138.	1.90	1503.
13.5	1.29 N	17409.	242.	0.	17652.	1.90	1548.
14.0	1.28 N	17930.	229.	0.	18159.	1.90	1593.
14.5	1.27 N	18444.	216.	0.	18660.	1.90	1637.
15.0	1.26 N	18949.	205.	0.	19154.	1.90	1680.
15.5	1.25 N	19448.	194.	0.	19642.	1.90	1723.
16.0	1.24 N	19939.	185.	0.	20123.	1.90	1765.
16.5	1.23 N	20422.	176.	0.	20598.	1.90	1807.
17.0	1.23 N	20899.	167.	0.	21066.	1.90	1848.
17.5	1.22 N	21369.	160.	0.	21528.	1.90	1888.
18.0	1.21 N	21832.	152.	0.	21984.	1.90	1928.
18.5	1.20 N	22288.	146.	0.	22433.	1.90	1968.
19.0	1.19 N	22737.	139.	0.	22876.	1.90	2007.
19.5	1.18 N	23180.	133.	0.	23313.	1.90	2045.
20.0	1.18 N	23616.	128.	0.	23744.	1.90	2083.
20.5	1.17 N	24046.	123.	0.	24168.	1.90	2120.
21.0	1.16 N	24469.	118.	0.	24587.	1.90	2157.
21.5	1.15 N	24887.	113.	0.	25000.	1.90	2193.
22.0	1.15 N	25298.	109.	0.	25407.	1.90	2229.
22.5	1.14 N	25703.	105.	0.	25808.	1.90	2264.
23.0	1.13 N	26102.	101.	0.	26203.	1.90	2299.
23.5	1.12 N	26496.	97.	0.	26593.	1.90	2333.
24.0	1.12 N	26883.	94.	0.	26977.	1.90	2366.



24.5	1.11	N	27265.	91.	0.	27356.	1.90	2400.	3360.
25.0	1.10	N	27642.	87.	0.	27729.	1.90	2432.	3386.

PROGRAM SAMM-

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DATE: / /

DESIGNER:

APPENDIX C

Referenced Material and Supporting Documents (On CD)

**SUPPLEMENT NO. 1 TO THE
2nd UPDATE TO THE
TECHNICAL DRAINAGE STUDY
FOR
QUEENS BOROUGH CULVERT**

619.295

MARCH 2006

Prepared for:

**JMA Architecture Studios
10150 Covington Cross Drive
Las Vegas, Nevada 89144
Phone: (702) 731- 2033
Fax: (702) 731- 2039**

Prepared by:

**G. C. Wallace, Inc.
1555 S. Rainbow Blvd.
Las Vegas, Nevada 89146
Phone: (702) 804-2000
Fax: (702) 804-2297**

619.295
RECEIVED

APR 26 2006

CITY OF LAS VEGAS		DATE:
INTER-OFFICE MEMORANDUM		April 21, 2006 G.C. WALLACE
TO: Land Development Services Department of Public Works		FROM: Albert Sung, P.E. Flood Control Project Engineer Department of Public Works
SUBJECT:	Technical Drainage Study for:	COPIES TO:
Queens Borrough Culvert (Plans AKA : The Village at Queensridge Culvert)		G. C. Wallace, Inc.
Cross Streets:	NEC of Alta Drive & Rampart Boulevard	JMA Architecture
File Number:	F:\Depot\DSMEMOS\DS3674F.ZNA.doc	Bart Anderson, P.E., DevCo
Parcel Number:	138-32-601-003	CCRFGD
FEMA Flood Zone	YES X NO	
Proposed Storm Drain	YES X NO	

HISTORY	DATE RECEIVED	DATE REVIEWED	COMMENTS	REVIEW FEES	FEES PAID Trn. No.
1 st Submittal	10/25/2004	11/9/2004	Not Approved	\$400.00	11413: \$400
2 nd Submittal	12/6/2004	12/20/2004	See Comments Below	\$400.00	13199: \$400
3 rd Submittal	3/4/2005	3/18/2005	Conditionally Approved	N/C	--
4 th Submittal	8/9/2005	8/23/2005	See Comments Below	\$400.00	27281: \$400
5 th Submittal	12/15/2005	12/30/2005	See Comments Below	\$400.00	35359: \$400
6 th Submittal	2/28/2006 3/30/2006 & 4/20/2006	4/21/2006	See Comments Below	N/C	N/C
TOTAL FEES (LDDRS):				\$1,600.00	----

REMARKS: 6th Submittal: Revised the on-site RCB alignment at the northeast corner of the site. Revised the RCB outfall structure, to include additional grading within Angel Park and the relocation of the concrete access road.

The Drainage Study for the subject project has been reviewed and:

X	is approved subject to conformance to all City standards and the following conditions:
	must be resubmitted or supplemented including the following:
	is conditionally approved subject to Clark County Regional Flood Control District concurrence.

1. The existing 48'-public drainage easement (Doc # 20051129:04185) must be vacated and a new easement dedicated to reflect the revised storm drain location. Provide a new legal description and exhibit to the Right-of-Way Section with a copy to Flood Control for review and approval. The revised easement must record concurrently with the vacated easement. The new easement must record prior to the final approval of the future technical drainage study needed for onsite development or approval of any final maps. **It is noted that the public drainage easement must be privately maintained both on the surface and within the box culvert.**
2. The revised plans for the storm drain system (CLV # 107y4889-CUL) must be submitted to Land Development for approval of this proposed revision.

3. The engineer has provided a copy of the FEMA Conditional Letter of Map Revision (CLOMR), Case No. 05-09-0420R for the subject project. The engineer is advised that they are required to obtain FEMA approval for this revision as well as the completed "As-Built" condition in order to obtain the Letter of Map Revision (LOMR). **The approved LOMR must be submitted to the City of Las Vegas prior to the release of the bond.**

NOTE: The engineer must submit the drainage study to FEMA for a Conditional Letter of Map Revision (CLOMR). A favorable CLOMR must be obtained prior to the issuance of any permits. This site is located in a FEMA Zone A. Clark County Regional Flood Control District (CCRFCD) review and approval is required prior to recordation of final map or issuance of building/grading permits. The Engineer must send a copy of the report to the CCRFCD for review. **The developer/engineer must also obtain a Letter of Map Revision (LOMR) using the approved drainage study as technical support to inform FEMA of the modifications within the flood zone. The approved LOMR must be submitted to the City of Las Vegas prior to the release of the bond.** FEMA Elevation Certificates, showing as-built finish floor elevations, must be completed for each building in the FEMA A Zone. The certificate must be submitted to the City of Las Vegas Flood Control Section prior to scheduling a framing inspection.

NOTE: Please be advised that all land surface area disturbances over 1 acre or any area adjacent to a water way must submit to the Nevada Division of Environmental Protection a "Notice of Intent" to discharge that certifies a stormwater pollution prevention plan has been developed and is maintained on site; for inclusion in the Stormwater General Permit No. NVR100000. A phased construction unit in a contiguous subdivision is considered under construction until all stripped or disturbed surface areas have been covered by paving, building construction or planting. For more information, including forms and applications see <http://ndep.nv.gov/bwpc/storm01.htm> or call (775) 687-9429.

END OF REMARKS
B&H/ays/pbj

T/R/S: T20S/R60E/32
AREA L-32

619.295

March 30, 2006



G. C. WALLACE, INC.

Albert Sung, PE
Flood Control Project Manager
City of Las Vegas Land Development Services
731 South Fourth Street
Las Vegas, Nevada 89101

Writer's Contact Information:
804-2029

**Re: Supplement No. 1 to the 2nd Update to the Technical Drainage Study for
Queens Borough Culvert (DS3674)**

Dear Mr. Sung:

The purpose of this letter is to amend the design submitted within the *2nd Update to the Technical Drainage Study for Queens Borough Culvert (DS3674)*. The proposed amendments are at the City of Las Vegas' request and are as follows:

The existing embankment, located approximately 180 feet east of the RCB headwall, will be removed. Since removal of this embankment section produces increased flow velocity within the channel, a 95-foot long riprap pad (d50 = 24-inches; thickness = 48-inches) is proposed at the RCB outlet. The WSPGW calculations have been revised to model the embankment removal.

As a result of the proposed channel improvements, the RCB access road alignment has been shifted. The revised access road cross-section detail and profile are provided with the grading packet. The proposed revisions do not adversely impact the adjacent properties or downstream facilities and are in agreement with the City of Las Vegas' drainage criteria.

Copies of the water surface profile model, RCB outlet protection calculations, and proposed grading plans are provided in the Appendix.

If you have any questions or require additional information, please contact me at 804-2029.

Very truly yours,

G. C. WALLACE, INC.

Cindy Kinzer, EI
Designer

CML/CK/jj

Christopher M. Luquette, PE, CFM
Project Manager
Flood Control Division

Enc.

c: Roy Clark, GCW

WATER SURFACE PROFILE LISTING
QUEENSBOROUGH CULVERT - JMA ARCH STUDIOS
GCWALLACE PROJECT # 619.295

Date: 3-16-2006 Time: 10: 6: 6

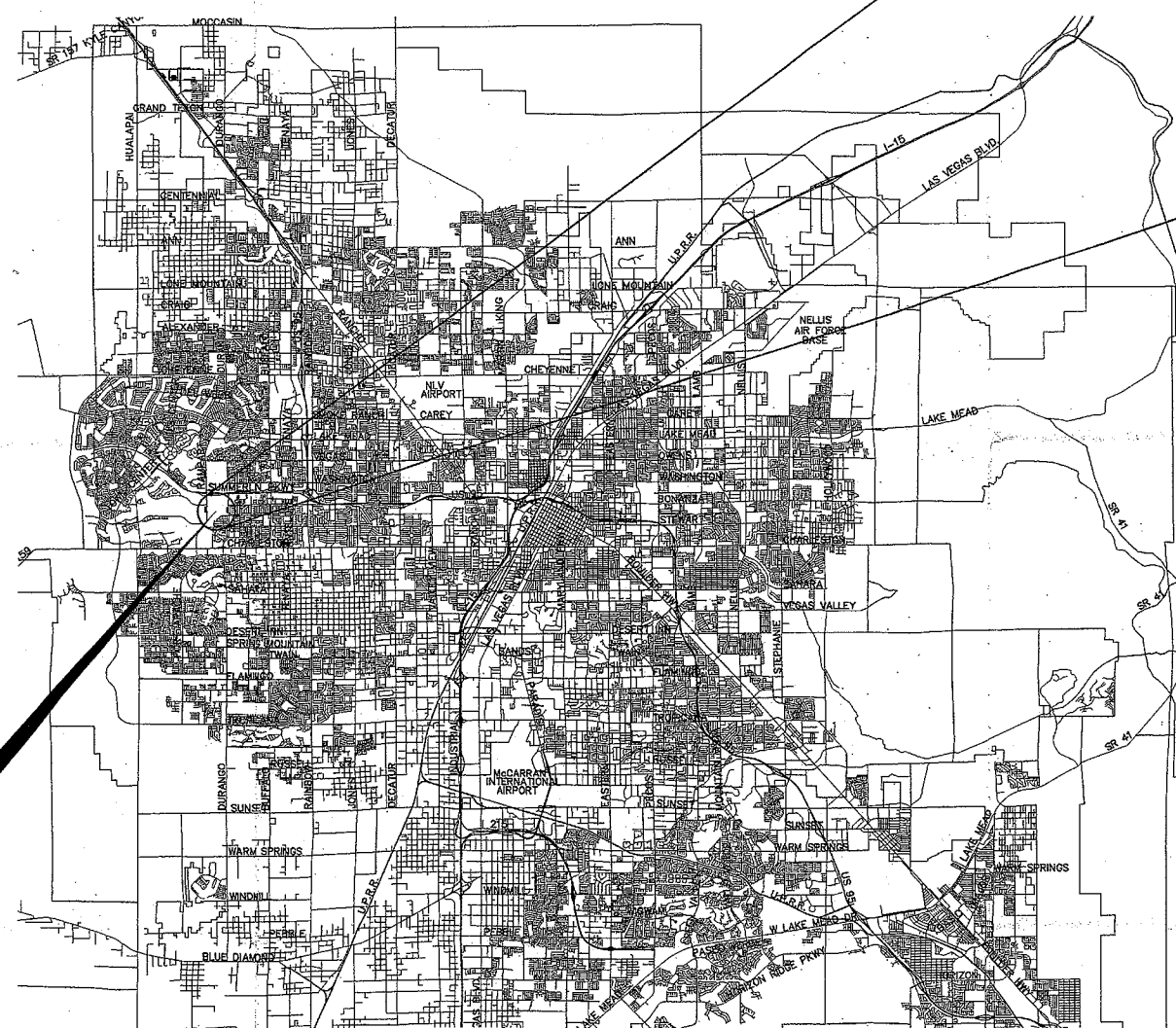
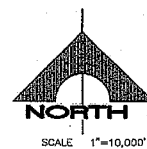
FILENAME: QB12X12-U2.WSW CJK

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd. E1	Super Elev	Critical Depth	Flow Top Width	Height/Dia. -FT	Base Wt or I.D.	ZL	No wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-3625.000	14.000	7.834	21.834	4497.00	17.38	4.69	26.53	.00	9.28	62.96	-	1	-	0 .0
TRANS STR	.0400	-	-	-	-	.0187	1.41	7.83	1.51	-	.035	-	-	IR-
OPEN														
-3550.000	17.000	8.266	25.266	4497.00	13.55	2.85	28.12	.00	8.27	58.19	-	2	-	0 .0
TRANS STR	.0100	-	-	-	-	.0070	.35	8.27	1.00	-	.035	-	-	IR-
OPEN														
-3500.000	17.500	10.031	27.531	4497.00	8.46	1.11	28.64	.00	7.33	75.12	-	3	-	0 .0
TRANS STR	.0328	-	-	-	-	-	-	10.031	.561	-	.040	-	-	IR-
OPEN														
-3401.010	20.750	2.481	23.231	4497.00	31.66	15.56	38.79	.00	5.67	63.50	-	4	-	0 .0
TRANS STR	.0110	-	-	-	-	.0371	1.86	2.48	3.73	-	.015	-	-	IR-
OPEN														
-3350.810	21.300	2.522	23.822	4497.00	33.25	17.16	40.99	.00	5.89	59.13	-	5	-	0 .0
TRANS STR	.0141	-	-	-	-	.0413	1.03	2.52	3.87	-	.015	-	-	IR-
OPEN														
-3325.950	21.650	2.323	23.973	4497.00	34.29	18.26	42.23	.00	5.71	60.97	-	6	-	0 .0
TRANS STR	.0160	-	-	-	-	.0340	.34	2.32	4.12	-	.015	-	-	IR-
OPEN														
-3315.950	21.810	5.925	27.735	4497.00	31.62	15.53	43.26	.00	10.29	25.00	12.000	25.000	.00	1 1.0
90.310	.0152	-	-	-	-	.0249	2.24	5.93	2.34	7.02	.015	.00	.00	BOX
-3225.640	23.180	5.731	28.911	4497.00	32.69	16.60	45.51	.00	10.29	25.00	12.000	25.000	.00	1 1.0
2.320	-.0776	-	-	-	-	.0263	.06	5.73	2.46	.00	.015	.00	.00	BOX
-3223.320	23.000	5.682	28.682	4497.00	32.98	16.89	45.57	12.00	10.29	25.00	12.000	25.000	.00	1 1.0
70.620	.0283	-	-	-	-	.0264	1.86	12.00	2.49	5.55	.015	.00	.00	BOX

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd. El.	Super Elev	Critical Depth	Flow Top width	Height/Dia. - FT	Base Wt or I.D.	ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-3152.700	25.000	5.709	30.709	4497.00	32.82	16.73	47.44	.00	10.29	25.00	12.000	25.000	.00	1 1.0
17.410	.0276					.0262	.46	5.71	2.47	5.60	.015	.00	.00	BOX
-3135.290	25.480	5.714	31.194	4497.00	32.79	16.70	47.89	12.00	10.29	25.00	12.000	25.000	.00	1 1.0
85.300	.0279					.0260	2.21	12.00	2.47	5.58	.015	.00	.00	BOX
-3049.990	27.860	5.748	33.608	4497.00	32.60	16.50	50.11	.00	10.29	25.00	12.000	25.000	.00	1 1.0
143.470	.0279					.0253	3.63	5.75	2.45	5.58	.015	.00	.00	BOX
-2906.520	31.860	5.829	37.689	4497.00	32.15	16.05	53.73	.40	10.29	25.00	12.000	25.000	.00	1 1.0
203.401	.0278					.0238	4.83	6.22	2.39	5.58	.015	.00	.00	BOX
-2703.119	37.523	6.024	43.546	4497.00	31.11	15.02	58.57	.37	10.29	25.00	12.000	25.000	.00	1 1.0
165.794	.0278					.0214	3.54	6.39	2.28	5.58	.015	.00	.00	BOX
-2537.325	42.138	6.318	48.456	4497.00	29.66	13.66	62.11	.34	10.29	25.00	12.000	25.000	.00	1 1.0
103.695	.0278					.0188	1.95	6.65	2.12	5.58	.015	.00	.00	BOX
-2433.630	45.025	6.626	51.651	4497.00	28.28	12.42	64.07	12.00	10.29	25.00	12.000	25.000	.00	1 1.0
60.182	.0278					.0168	1.01	12.00	1.98	5.58	.015	.00	.00	BOX
-2373.448	46.700	6.888	53.588	4497.00	27.20	11.49	65.08	12.00	10.29	25.00	12.000	25.000	.00	1 1.0
55.228	.0278					.0150	.83	12.00	1.86	5.58	.015	.00	.00	BOX
-2318.220	48.238	7.224	55.462	4497.00	25.94	10.45	65.91	.00	10.29	25.00	12.000	25.000	.00	1 1.0
26.702	.0278					.0136	.36	7.22	1.74	5.58	.015	.00	.00	BOX

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base wt or I.D.	ZL	No wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-2291.518	48.982	7.440	56.421	4497.00	25.19	9.85	66.27	.00	10.29	25.00	12.000	25.000	.00	1 1.0
34.206	.0278					.0123	.42	7.44	1.66	5.58	.015	.00	.00	BOX
-2257.313	49.934	7.803	57.737	4497.00	24.01	8.95	66.69	.00	10.29	25.00	12.000	25.000	.00	1 1.0
25.506	.0278					.0109	.28	7.80	1.55	5.58	.015	.00	.00	BOX
-2231.807	50.644	8.184	58.828	4497.00	22.90	8.14	66.97	.00	10.29	25.00	12.000	25.000	.00	1 1.0
18.679	.0278					.0096	.18	8.18	1.44	5.58	.015	.00	.00	BOX
-2213.128	51.164	8.583	59.748	4497.00	21.83	7.40	67.15	.00	10.29	25.00	12.000	25.000	.00	1 1.0
13.128	.0278					.0085	.11	8.58	1.34	5.58	.015	.00	.00	BOX
-2200.000	51.530	9.002	60.532	4497.00	20.81	6.73	67.26	.00	10.29	25.00	12.000	25.000	.00	1 1.0
60.785	.0080					.0080	.49	9.00	1.25	9.00	.015	.00	.00	BOX
-2139.215	52.016	9.002	61.018	4497.00	20.81	6.73	67.75	.00	10.29	25.00	12.000	25.000	.00	1 1.0
405.355	.0080					.0077	3.13	9.00	1.25	9.00	.015	.00	.00	BOX
-1733.860	55.259	9.255	64.514	4497.00	20.24	6.36	70.88	12.00	10.29	25.00	12.000	25.000	.00	1 1.0
54.700	.0080					.0074	.40	12.00	1.20	9.00	.015	.00	.00	BOX
-1679.160	55.697	9.355	65.051	4497.00	20.03	6.23	71.28	12.00	10.29	25.00	12.000	25.000	.00	1 1.0
95.423	.0080					.0069	.65	12.00	1.18	9.00	.015	.00	.00	BOX
-1583.737	56.460	9.811	66.271	4497.00	19.10	5.66	71.93	12.00	10.29	25.00	12.000	25.000	.00	1 1.0
18.737	.0080					.0061	.11	12.00	1.10	9.00	.015	.00	.00	BOX

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd. El.	Super Elev	Critical Depth	Flow Top width	Height/Dia. - FT	Base wt or I.D.	ZL	No wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
-1565.000	56.610	10.291	66.901	4497.00	18.21	5.15	72.05	.00	10.29	25.00	12.000	25.000	.00	1 1.0
88.377	.0050					.0051	.45	10.29	1.02	10.85	.015	.00	.00	Box
-1476.623	57.053	10.793	67.846	4497.00	17.36	4.68	72.53	.00	10.29	25.00	12.000	25.000	.00	1 1.0
257.531	.0050					.0050	1.29	10.79	.95	10.85	.015	.00	.00	Box
-1219.092	58.343	10.853	69.196	4497.00	17.26	4.63	73.82	.00	10.29	25.00	12.000	25.000	.00	1 1.0
219.092	.0050					.0050	1.10	10.85	.94	10.85	.015	.00	.00	Box
----- WARNING - Flow depth near top of box conduit -----														
-1000.000	59.440	10.853	70.293	4497.00	17.26	4.63	74.92	.00	10.29	25.00	12.000	25.000	.00	1 1.0



NOTE: ALL LAND SURFACE AREA DISTURBANCES OVER 1 ACRE REQUIRE A STORMWATER DISCHARGE PERMIT ISSUED BY THE NEVADA DIVISION OF ENVIRONMENTAL PROTECTION (NDEP). A PHASED CONSTRUCTION DISTURBANCE PERMIT MAY BE OBTAINED PRIOR TO UNDER CONSTRUCTION UNTIL ALL STRIPPED OR DISTURBED SURFACES HAVE BEEN COVERED BY PAVING, BUILDING CONSTRUCTION OR PLANTING. A STORMWATER DISCHARGE PERMIT APPLICATION AND ASSOCIATED FEE MUST BE SUBMITTED TO THE NDEP WEBSITE: [HTTP://WWW.STATE.NV.US/NDEP/BWSC/STORMDO.HTM](http://www.state.nv.us/ndep/bwsc/stormdo.htm) PROJECTS THAT DISTURB MORE THAN ONE ACRE OF LAND MUST SUBMIT TO NDEP A "NOTICE OF INTENT" FOR INCLUSION UNDER STORMWATER PERMIT NO. NVR100000 ALONG WITH THE APPROPRIATE FILING FEE.

BASIS OF BEARING

SOUTH 00°32'07" EAST, BEING THE BEARING OF THE CENTERLINE OF "RAMPART BOULEVARD" AS SHOWN BY MAP THEREOF ON FILE IN FILE 64, PAGE 93 OF SURVEYS IN THE COUNTY RECORDER'S OFFICE, CLARK COUNTY, NEVADA, LYING WITHIN THE NORTH HALF (N 1/2) OF SECTION 32, TOWNSHIP 20, SOUTH, RANGE 60 EAST, M.D.M., CITY OF LAS VEGAS, CLARK COUNTY, NEVADA.

BENCHMARK

RIVET AND PLATE IN TOP OF CURB @ TOWN CENTER AND VILLAGE CENTER ON WEST EDGE OF ROUNDABOUT.

CITY OF LAS VEGAS BENCHMARK 0LV00 3266
LOCATED ON THE NORTHEAST CORNER OF ALTA DR. AND UPPER HILL
NAVD 88 ELEVATION = 814.1281 METERS, 2671.02 FEET
SUMMERLIN ELEVATION 2726.11 FEET

NOTE: ADD 2.2' TO THE CURRENTLY USED SUMMERLIN BENCHMARK
TO EQUAL TO THE APPROVED CITY OF LAS VEGAS BENCHMARK.

CITY OF LAS VEGAS

"APPROVAL OF THESE PLANS BY THE CITY ENGINEER IS LIMITED TO THOSE IMPROVEMENTS CONSTRUCTED IN THE DEDICATED RIGHTS-OF-WAY AND/OR DEDICATED EASEMENTS. THIS APPROVAL DOES NOT AUTHORIZE THE CONSTRUCTION OF ANY IMPROVEMENTS THAT DEVIATE FROM ADOPTED STANDARDS AND/OR SPECIFICATIONS EXCEPT THOSE SPECIFICALLY LISTED UNDER "DEVIATION FROM STANDARDS." THE ENGINEER SHALL RESOLVE ANY DEVIATION OTHER THAN THOSE LISTED IN "DEVIATION FROM STANDARDS" IN FAVOR OF THE SUMMERLIN IMPROVEMENT STANDARDS AND SPECIFICATIONS. CLARK COUNTY AREA NEVADA."

CHARLES KAJKOWSKI, JR.; P.E. #4784
CITY ENGINEER

CITY OF LAS VEGAS, NEVADA

M. MARGO WHEELER, AICP, DIRECTOR OF PLANNING AND DEVELOPMENT DATE
THIS PLAN MEETS THE APPLICABLE STANDARDS OF THE PLANNING AND DEVELOPMENT DEPARTMENT

NEVADA POWER CO. _____ DATE _____

NEVADA POWER COMPANY ACKNOWLEDGES THAT WE HAVE RECEIVED YOUR PLANS AND WILL PROVIDE SERVICE TO ALL ELECTRICAL NEEDS ASSOCIATES WITH THIS PROJECT. NEVADA POWER COMPANY RESERVES THE RIGHT TO ADDRESS ANY EXISTING OR FUTURE CONFLICTS ONCE THE FINAL DESIGN IS COMPLETED. THE NEW SERVICE AND THE RESOLUTION OF ANY CONFLICTS WILL BE ACCOMPLISHED PURSUANT TO THE NEVADA PUBLIC UTILITY COMMISSION'S RULES AND REGULATIONS.

SPRINT _____ **DATE** _____

"THE AFFIXED SPRINT NEVADA APPROVAL DOES NOT ASSUME OR GUARANTEE LIABILITY FOR KNOWN OR UNKNOWN CONFLICTS WITH EXISTING OR PROPOSED IMPROVEMENTS. RESOLUTION OF ANY CONFLICT WILL BE ACCOMPLISHED PURSUANT TO LOCAL ORDINANCES, NEVADA REVISED STATUTES AND/OR PUBLIC UTILITY COMMISSION RULES AND REGULATIONS"

SOUTHWEST GAS CORP. DATE

COX COMMUNICATIONS LAS VEGAS, INC. DATE

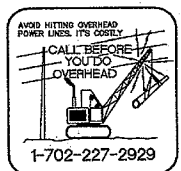
SEE SHEET
 LAS VEGAS VALLEY WATER DISTRICT C-X, C-X, C-X DATE
 PROJ. #XXXXX

INDEX OF DRAWINGS	
NO.	TITLE AND DESCRIPTION
C-1	COVER SHEET
C-2	GENERAL NOTES
C-3	MASTER GRADING PLAN
C-4	STORM DRAIN PLAN & PROFILE (STA. 10+00.00 TO 17+00.00)
C-5	STORM DRAIN PLAN & PROFILE (STA. 17+00.00 TO 24+00.00)
C-6	STORM DRAIN PLAN & PROFILE (STA. 24+00.00 TO 33+00.00)
C-7	DETAIL SHEET
C-8	DETAIL SHEET
C-9	STORM DRAIN PLAN & PROFILE (STA. 31+50.00 TO 36+00.00)
S-1	STRUCTURAL SECTION AND DETAILS
S-2	STRUCTURAL SECTION AND DETAILS



G.C. WALLACE, INC.
 Engineering/Planners/Surveyors
 1555 SOUTH RAINBOW BLVD. / LAS VEGAS, NEVADA 89146

JMA ARCHITECTURE STUDIOS
10150 COVINGTON CROSS
LAS VEGAS NV 89144
(702)731-2033



THE VILLAGE AT QUEENSPRIDGE CULVERT

COVER SHEET

DRAWING
C-1

1 OF 11 SHTS

CITY OF LAS VEGAS GENERAL NOTES

- ALL CONSTRUCTION AND MATERIALS SHALL BE IN ACCORDANCE WITH THE "UNIFORM STANDARD SPECIFICATIONS FOR PUBLIC WORKS CONSTRUCTION OFF-SITE IMPROVEMENTS, CLARK COUNTY AREA, NEVADA," LATEST EDITION, THE "UNIFORM STANDARD SPECIFICATIONS FOR PUBLIC WORKS CONSTRUCTION, CLARK COUNTY AREA, NEVADA," LATEST EDITION, THE "SUMMERLIN IMPROVEMENT STANDARDS" FOR WORK IN THE SUMMERLIN AREA, AND OTHER APPLICABLE APPROVED STANDARDS ISSUED BY THE CONTROLLING AGENCY, THE UNIFORM BUILDING CODE, AND ALL LOCAL CITY CODES AND ORDINANCES APPLICABLE, EXCEPT AS NOTED ON THIS SHEET AS "DEVIATIONS FROM STANDARDS".
- THE EXISTENCE AND LOCATION OF ANY OVERHEAD OR UNDERGROUND UTILITY LINES, PIPES, OR STRUCTURES SHOWN ON THESE PLANS ARE OBTAINED BY A RESEARCH OF THE AVAILABLE RECORDS. EXISTING UTILITIES AS SHOWN FROM CLV PLANS LIBRARY ARE APPROXIMATE AND FOR RECORD PURPOSES. EXISTING UTILITIES ARE LOCATED ON PLANS ONLY FOR THE CONVENIENCE OF THE CONTRACTOR. THE CONTRACTOR SHALL NOT BE RESPONSIBLE FOR THE LOCATION OF UTILITIES SHOWN ON THE PLANS. AT HIS OWN EXPENSE, LOCATE ALL UNDERGROUND AND OVERHEAD INTERFERENCE WHICH MAY AFFECT HIS OPERATION DURING CONSTRUCTION AND SHALL TAKE ALL NECESSARY PRECAUTIONS TO AVOID DAMAGE TO SAME. THE CONTRACTOR SHALL USE EXTREME CAUTION WHEN WORKING NEAR OVERHEAD UTILITIES SO AS TO SAFELY PROTECT ALL PERSONNEL AND EQUIPMENT, AND SHALL BE RESPONSIBLE FOR ALL COST AND LIABILITY IN CONNECTION THEREWITH.
- THE CONTRACTOR SHALL TAKE ALL PRECAUTIONARY MEASURES NECESSARY TO PROTECT EXISTING UTILITY LINES, STRUCTURES AND STREET IMPROVEMENTS WHICH ARE TO REMAIN IN PLACE FROM DAMAGE, AND ALL SUCH IMPROVEMENTS OR STRUCTURES DAMAGED BY THE CONTRACTOR'S OPERATIONS SHALL BE REQUIRED OR REPLACED SATISFACTORY TO THE CITY ENGINEER AND OWNING UTILITY COMPANY AT THE EXPENSE OF THE CONTRACTOR.
- ALL CONSTRUCTION SHALL BE SHOWN ON THESE PLANS, ANY REVISIONS SHALL HAVE THE PRIOR WRITTEN APPROVAL OF THE CITY ENGINEER.
- TYPE V CEMENT SHALL BE USED IN ALL OFF-SITE CONCRETE WORK. CONCRETE TO BE 3000 P.S.I. MINIMUM 98 DAYS. MIX DESIGN TO BE APPROVED BY THE CITY ENGINEER, PRIOR TO THE USE ON THE PROJECT.
- PERMITS ARE REQUIRED FOR ANY WORK IN THE PUBLIC RIGHT-OF-WAY. THE CONTRACTOR SHALL SECURE ALL PERMITS AND INSPECTIONS REQUIRED FOR THIS CONSTRUCTION.
- EXPANSION JOINTS REQUIRED, MAXIMUM EVERY 150' IN EXTRUDED-TYPE CURB, PER SUMMERLIN IMPROVEMENT STANDARDS.
- AC PAVEMENT TO BE ONE-HALF INCH (1/2") ABOVE LIP OF ALL GUTTERS AFTER COMPACTION, EXCEPT AT SIDEWALK RAMPS AND CROSS GUTTERS.
- CURB AND GUTTER FOUND TO BE UNACCEPTABLE TO THE CITY OF LAS VEGAS SHALL BE REMOVED AND REPLACED PER SUMMERLIN STANDARD DRAWING S-47.
- SIDEWALK RAMPS SHALL BE CONSTRUCTED IN EACH QUADRANT OF AN INTERSECTION PER STANDARD SUMMERLIN DRAWINGS. EXACT LOCATION OF RAMPS MAY BE ADJUSTED IN THE FIELD BY A CITY INSPECTOR.
- CONTRACTOR SHALL PROVIDE ALL NECESSARY HORIZONTAL AND VERTICAL TRANSITIONS BETWEEN NEW CONSTRUCTION AND EXISTING SURFACES TO PROVIDE FOR PROPER DRAINAGE AND FOR INGRESS AND EGRESS TO NEW CONSTRUCTION. THE EXTENT OF TRANSITIONS TO BE AS SHOWN ON PLANS.
- ALL GRADING WORK SHALL CONFORM TO THE SOILS REPORT AS PREPARED BY TERRACON, PROJECT NO. 64985481, APPROVED BY THE CITY ENGINEER AND AS SHOWN ON THESE PLANS.
- EXACT LOCATION OF ALL SAWCUT LINES MAY BE ADJUSTED OR DETERMINED IN THE FIELD BY A CITY OF LAS VEGAS ENGINEER IF LOCATION ON PLANS IS NOT CLEARLY SHOWN, OR EXISTING PAVEMENT CONDITION REQUIRES RELOCATIONS.
- THE CONTRACTOR SHALL TAKE ALL PRECAUTIONS NECESSARY TO PROTECT EXISTING PERMANENT SURVEY MONUMENTS. ANY MONUMENTS DISTURBED SHALL BE REPLACED AND ADJUSTED PER AVAILABLE RECORDS IN ACCORDANCE WITH N.R.S. NO. 225.550.
- UTILITY COMPANY METER BOXES, MANHOLE LIDS, VALVE COVERS, ETC., SHALL BE LOCATED OUT OF DRIVEWAYS, DRIVEWAY APRONS, FLOWLINES, AND CROSS GUTTERS UNLESS WRITTEN APPROVAL IS GRANTED BY THE UTILITY COMPANY AND THE CITY ENGINEER.
- WALL NOTES: ALL WALLS, NEW OR EXISTING, ARE ONLY SHOWN ON CIVIL PLANS FOR THE PURPOSE OF REVIEWING GRADING RELATIONSHIPS; FLOOD CONTROL AND SIGHT DISTANCE AT INTERSECTIONS. NEW WALLS REQUIRE A SEPARATE PERMIT AND FLOOD CONTROL AND SIGHT DISTANCE AT INTERSECTIONS. NEW WALLS REQUIRE A SEPARATE PERMIT AND INSPECTION BY THE BUILDING DEPARTMENT.
- ASPHALT MIX DESIGN MUST BE SUBMITTED AND APPROVED BY THE CITY ENGINEER PRIOR TO THE PLACEMENT OF ASPHALT WITHIN CITY RIGHT-OF-WAY.
- CONTRACTOR SHALL ADJUST ALL NEW AND EXISTING INLETS, VALVE BOXES, MANHOLE RIMS, AND SEWER CLEAN OUTS, ETC. TO FINISH GRADE AS APPLICABLE WHETHER OR NOT THEY ARE SHOWN ON THE PLANS.
- MATERIALS, HANDLING AND PLACEMENT OF PORTLAND CEMENT CONCRETE SHALL BE IN ACCORDANCE WITH APPLICABLE SPECIFICATIONS OF MDOT OR THE CLARK COUNTY AREA SPECIFICATIONS (AS APPLICABLE) AND THE PLANS AND DETAILS SHOWN HEREON.

CITY OF LAS VEGAS GRADING NOTES

- IN THE EVENT THAT ANY UNFORESEEN CONDITIONS NOT COVERED BY THESE NOTES ARE ENCOUNTERED DURING GRADING OPERATIONS, THE OWNER/ENGINEER SHALL BE IMMEDIATELY NOTIFIED FOR DIRECTION.
 - IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO PERFORM ALL NECESSARY CUTS AND FILLS WITHIN THE LIMITS OF THIS PROJECT AND THE RELATED OFF-SITE WORK, SO AS TO GENERATE THE DESIRED SUBGRADE, FINISH GRADES AND SLOPES.
 - CONTRACTOR SHALL TAKE FULL RESPONSIBILITY FOR ALL EXCAVATION. ADEQUATE SHORING SHALL BE DESIGNED AND PROVIDED BY THE CONTRACTOR TO PREVENT UNDERMINING OF ANY ADJACENT FEATURES OR FACILITIES AND/OR CAVING OF THE EXCAVATION.
 - THE CONTRACTOR IS WARNED THAT AN EARTHWORK BALANCE WAS NOT NECESSARILY THE INTENT OF THIS PROJECT. ANY ADDITIONAL MATERIAL REQUIRED OR LEFTOVER MATERIAL FOLLOWING EARTHWORK OPERATIONS BECOMES THE RESPONSIBILITY OF THE CONTRACTOR.
 - THE GRADING CONTRACTOR IS RESPONSIBLE TO COORDINATE WITH THE OWNER TO PROVIDE FOR THE REQUIREMENTS OF THE PROJECT STORM WATER POLLUTION PREVENTION PLAN (SWPPP) AND ASSOCIATED PERMIT.
 - CONTRACTOR SHALL GRADE TO THE LINES AND ELEVATIONS SHOWN ON THE PLANS WITHIN THE FOLLOWING HORIZONTAL AND VERTICAL TOLERANCES AND DEGREES OF COMPACTION, IN THE AREAS INDICATED:
- | | HORIZONTAL | VERTICAL COMPACTION | SEE SOILS REPORT |
|---------------------------|------------|---------------------|------------------|
| A. PAVEMENT AREA SUBGRADE | 0.1" | +0.0' TO -0.1' | SEE SOILS REPORT |
| B. ENGINEERED FILL | 0.5" | +0.1' TO -0.1' | SEE SOILS REPORT |
- COMPACTION TESTING WILL BE PERFORMED BY THE OWNER OR HIS REPRESENTATIVE.
- ALL CUT AND FILL SLOPES SHALL BE PROTECTED UNTIL EFFECTIVE EROSION CONTROL HAS BEEN ESTABLISHED.
 - THE USE OF POTABLE WATER WITHOUT A SPECIAL PERMIT FOR BUILDING OR CONSTRUCTION PURPOSES INCLUDING CONSOLIDATION OF BACKFILL OR DUST CONTROL IS PROHIBITED. THE CONTRACTOR SHALL OBTAIN ALL NECESSARY PERMITS FOR CONSTRUCTION WATER.
 - THE CONTRACTOR SHALL MAINTAIN THE STREETS, SIDEWALKS AND ALL OTHER PUBLIC RIGHT-OF-WAY IN A CLEAN, SAFE AND USABLE CONDITION. ALL SPILLS OF SOIL, ROCK OR CONSTRUCTION DEBRIS SHALL BE PROMPTLY REMOVED FROM THE PUBLICLY OWNED PROPERTY DURING CONSTRUCTION AND UPON COMPLETION OF THE PROJECT. ALL ADJACENT PROPERTY, PRIVATE OR PUBLIC, SHALL BE MAINTAINED IN A CLEAN, SAFE AND USABLE CONDITION.
 - IN THE EVENT THAT ANY TEMPORARY CONSTRUCTION ITEM IS REQUIRED THAT IS NOT SHOWN ON THESE DRAWINGS, THE OWNER AGREES TO PROVIDE AND INSTALL SUCH ITEM AT HIS OWN EXPENSE AT THE DIRECTION OF THE CITY ENGINEER. TEMPORARY CONSTRUCTION INCLUDES DITCHES, BERMS, ROAD SIGNS AND BARRICADES, ETC.

CITY OF LAS VEGAS SEWER NOTES

- ALL CONSTRUCTION AND MATERIALS SHALL BE IN ACCORDANCE WITH THE LATEST EDITION OF THE DESIGN AND CONSTRUCTION STANDARDS FOR WASTEWATER COLLECTION SYSTEMS AND THE UNIFORM STANDARD SPECIFICATIONS FOR PUBLIC WORKS CONSTRUCTION OFF-SITE IMPROVEMENTS, CLARK COUNTY AREA, NEVADA, AS AMENDED. IT WILL BE THE RESPONSIBILITY OF THE CONTRACTOR TO BE AWARE OF THE CONTENTS OF THE ABOVE SPECIFICATIONS.
- IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO PERFORM CONSTRUCTION AS PER PLANS. ANY ADDITIONS, DELETIONS, OR CHANGES SHALL FIRST MEET WITH THE APPROVAL OF THE CITY ENGINEER.
- CHISEL "S" OR "G" IN CURBS WHERE SEWER OR GAS LATERALS PASS UNDER THE CURB.
- POLYVINYL (PVC) SEWER PIPE SHALL MEET ASTM D-3034 SDR 35 SPECIFICATIONS, INSTALLED WITH SAND BEDDING AND BACKFILL OF TYPE II AGGREGATE BASE.
- ALL MANHOLES PAVED IN STREETS EIGHTY (80') FOOT R/W AND LARGER SHALL HAVE CONCRETE COLLARS. STREETS LESS THAN EIGHTY (80') FOOT R/W WILL REQUIRE RETROFIT IF PAVING DOES NOT CONFORM TO CITY STANDARDS AT THE MANHOLE.
- TEE SADDLES SHALL BE USED TO CONNECT SEWER LATERALS TO EXISTING MAIN LINES UP TO TWELVE INCH (12") DIAMETER. CONNECTIONS TO FIFTEEN INCH (15") OR LARGER MAINS SHALL REQUIRE SPECIAL PROCEDURES. IN LINE 7" S SHALL BE USED ON LINES TWELVE INCHES (12") OR ABOVE.
- WATER MAINS SHALL BE PROTECTED IN ACCORDANCE WITH LVVWD STANDARDS WHENEVER A SEWER MAIN CROSSES OVER A WATER MAIN OR THE SEWER IS LESS THAN EIGHTEEN INCH (18") UNDER A WATER MAIN.
- ALL CONTRACTORS INSTALLING SEWER MAINS THAT WILL BE UNDER THE JURISDICTION OF THE CITY OF LAS VEGAS MUST BE STATE OF NEVADA CLASS "C" CONTRACTORS.
- THE CITY OF LAS VEGAS WILL NOT ACCEPT ANY SEWER MAINS WHICH HAVE A VERTICAL DEFLECTION OF MORE THAN ONE TENTH (0.1) OF A FOOT FROM THE APPROVED CONSTRUCTION PLANS AT ANY LOCATION. SEWER MAINS FOUND TO EXCEED THIS TOLERANCE WILL HAVE TO BE REPAIRED OR REMOVED OR REPLACED TO THE SATISFACTION OF THE CITY ENGINEER PRIOR TO ACCEPTANCE BY THE CITY OF LAS VEGAS.
- INSTALLATION OF CURVED SEWER REQUIRES THE USE OF C-900 PVC PIPE WHICH ALLOWS FOR PIPE DEFLECTION AT THE JOINTS.

CITY OF LAS VEGAS FIRE DEPARTMENT NOTES

- ALL WORK SHALL BE DONE IN STRICT ACCORDANCE WITH THE CITY OF LAS VEGAS FIRE DEPARTMENT'S ORDINANCE # 5687, "HYDRANT SPECIFICATIONS", AND "HYDRANT INSTALLATION SPECIFICATION".
- AUTHORIZED HYDRANTS FOR THIS PROJECT ARE:
A. KENNEDY - GUARDIAN MODELS KB1A AND KB1D
B. MUELLER - SUPER CENTURION 250 MODEL A-423
C. CLOW - MEDALLION MODEL F-2548LV
D. U.S. PIPE - METROFLOW/M-03
E. TROY VALVE - PATRIOT MODEL PTB100N NEVADA HYDRANT
- ON ANY RESIDENTIAL OR COMMERCIAL INSTALLATIONS FIRE HYDRANTS SHALL BE INSTALLED AND FIRE APPARATUS ACCESS ROADS SHALL BE MAINTAINED BEFORE COMMENCEMENT OF ANY COMBUSTIBLE CONSTRUCTION. ALL FIRE HYDRANTS SHALL BE IN GOOD WORKING ORDER AND SHALL BE CAPABLE OF DELIVERING THE REQUIRED FIRE FLOW.
- TO IDENTIFY THE FIRE HYDRANT LOCATIONS, CONTRACTOR SHALL PLACE A BLUE REFLECTIVE MARKER AT THE CENTER LINE OF STREET ADJACENT TO THE FIRE HYDRANTS AS REQUIRED BY ORDINANCE # 5687.
- ALL UNDERGROUND INSPECTIONS, PRESSURE AND FLUSH VERIFICATIONS OF ALL FIRE HYDRANTS AND FIRE LINES, SHALL BE CONDUCTED BEFORE COVERING THE LINES. CALL THE CITY OF LAS VEGAS INSPECTION HOT-LINE AT 229-2071 TO REQUEST AN INSPECTION BY THE CITY OF LAS VEGAS FIRE DEPARTMENT.
- PAINTING OF THE CURBS AND FIRE HYDRANTS AND ALL OTHER WORK NECESSARY AS REQUIRED BY ORDINANCE # 5687, FOR THE PROTECTION OF FIRE HYDRANTS FROM PHYSICAL DAMAGE, SHALL BE COMPLETED BEFORE APPROVAL BY THE CITY OF LAS VEGAS FIRE DEPARTMENT.
- A PERMIT IS REQUIRED FROM THE CITY OF LAS VEGAS FIRE DEPARTMENT FOR THE ON-SITE WATER LINES AND FIRE HYDRANTS. THE PERMIT AND CONTRACTOR'S MATERIAL AND TEST CERTIFICATE FOR UNDERGROUND PIPING FORM SHALL BE OBTAINED FROM THE FIRE PROTECTION ENGINEER BEFORE COMMENCEMENT OF WORK.
- PRIVATE FIRE HYDRANTS SHALL BE PAINTED RED.
- PRIOR TO THE FINAL OCCUPANCY, A FLOW TEST MUST BE WITNESSED BY THE CITY OF LAS VEGAS FIRE DEPARTMENT TO VERIFY AVAILABILITY OF THE REQUIRED FIRE FLOW.
- ALL ON-SITE UNDERGROUND WATER MAINS AND MATERIALS SHALL BE U.L. LISTED, A.W.W.A. APPROVED, AND SHALL BE RATED FOR THE APPROPRIATE WORKING PRESSURE.
- FIRE HYDRANTS SPACING SHALL BE:
RESIDENTIAL - 500 FEET UNSPRINKLERED; 800 FEET SPRINKLERED.
COMMERCIAL - 300 FEET UNSPRINKLERED; 400 FEET SPRINKLERED.
- WHERE NEW WATER MAINS ARE EXTENDED ALONG STREETS OR NEW STREETS ARE INSTALLED WHERE FIRE HYDRANTS ARE NOT NEEDED FOR PROTECTION OF THE STRUCTURES, FIRE HYDRANTS SHALL BE INSTALLED AT MAXIMUM 1,000 FOOT SPACING, TO PROVIDE FOR TRANSPORTATION HAZARDS. WHERE STREETS ARE PROVIDED WITH MEDIAN DIVIDERS OR HAVE FOUR OR MORE TRAFFIC LANES AND HAVE A TRAFFIC COUNT OF MORE THAN 30,000 PER DAY, HYDRANTS ARE REQUIRED ON EACH SIDE OF THE STREET SPACED AT 500 FEET ON AN ALTERNATING BASIS.
- NO FIRE HYDRANTS SHALL BE LOCATED WITHIN THE REQUIRED RADIUS OF A CUL-DE-SAC OR WITHIN 20 FEET OF THE PERIMETER OF THE RADIUS OF THE CUL-DE-SAC.
- NO FIRE HYDRANT SHALL BE LOCATED WITHIN 6 FEET OF ANY CURB RETURN, DRIVEWAY, POWER POLE, STREET LIGHT OR ANY OTHER OBSTRUCTION.
- THE MAXIMUM DISTANCE FROM A FIRE HYDRANT TO A ONE-TWO FAMILY DWELLING SHALL NOT EXCEED 300 FEET, AS MEASURED BY AN APPROVED ROUTE.
- THE MAXIMUM DISTANCE FROM A FIRE HYDRANT TO A FIRE DEPARTMENT CONNECTION (FDC) SHALL NOT EXCEED 100 FEET, AS MEASURED BY AN APPROVED ROUTE.
- THE MAXIMUM DISTANCE FROM A FIRE HYDRANT TO THE END OF A DEAD-END STREET SHALL NOT EXCEED 200 FEET.
- TWO SOURCES OF SUPPLY ARE REQUIRED WHENEVER THERE ARE 4 OR MORE FIRE HYDRANTS/SPRINKLER LEAD-INS ARE INSTALLED ON A SINGLE SYSTEM. SECTIONAL CONTROL VALVES SHALL BE INSTALLED SO THAT NO MORE THAN 2 FIRE HYDRANTS CAN BE OUT OF SERVICE DUE TO A BREAK IN A WATER MAIN.
- ALL FIRE APPARATUS ACCESS ROADS SHALL BE PAVED TO PROVIDE ALL-WEATHER DRIVING CAPABILITIES, AND SHALL BE DESIGNED AND MAINTAINED TO SUPPORT THE IMPOSED LOADS OF THE FIRE APPARATUS.
- THE GRADIENT FOR THE FIRE APPARATUS ACCESS ROADS SHALL NOT EXCEED 12% ANGLES OF APPROACH AND ANGLES OF DEPARTURE SHALL NOT EXCEED 8% FOR 25 FEET PRIOR TO OR AFTER THE GRADE CHANGE. ADJACENT TO THE STRUCTURES GRADIENT SHALL NOT EXCEED 6%.
- THE TURNING RADIUS OF THE FIRE APPARATUS ACCESS ROADS SHALL BE NO LESS THAN 52 FEET OUTSIDE AND 28 FEET INSIDE TURNING RADIUS.
- VERTICAL CLEARANCE OF ALL FIRE APPARATUS ACCESS ROADS SHALL BE NOT LESS THAN 13 FEET 6 INCHES.
- FIRE DEPARTMENT ACCESS ROADS IN ALL RESIDENTIAL DEVELOPMENTS (EXCEPT FOR THE APARTMENT BUILDINGS) SHALL HAVE A MINIMUM UNOBSTRUCTED WIDTH OF NOT LESS THAN 36 FEET FLOW LINE TO THE FLOW LINE (THIS WIDTH MAY BE REDUCED TO 24 FEET, IF ALL BUILDINGS FRONTING THE STREET ARE SPRINKLERED) FOR MAIN RESIDENTIAL STREETS, WITH PARKING PERMITTED ON BOTH SIDES OF THE STREET. PRIVATE DRIVE AISLES, DRIVEWAYS, ETC. SHALL BE ALLOWED TO BE REDUCED TO 24 FEET FLOW LINE TO THE FLOW LINE TO THE FLOW LINE WHEN SERVING NO MORE THAN 6 RESIDENCES, AND WHEN ON STREET PARKING IS DISALLOWED.
- ALL FIRE APPARATUS ACCESS ROADS IN COMMERCIAL DEVELOPMENTS AND APARTMENT COMPLEXES SHALL HAVE A MINIMUM UNOBSTRUCTED WIDTH OF NOT LESS THAN 24 FEET (FLOW LINE TO THE FLOW LINE), PROVIDED NO PARKING IS ALLOWED ON EITHER SIDE; 32 FEET (FLOW LINE TO THE FLOW LINE) IF PARALLEL PARKING IS ALLOWED ON ONE SIDE ONLY; AND 40 FEET (FLOW LINE TO THE FLOW LINE), IF PARALLEL PARKING IS ALLOWED ON BOTH SIDES. THESE WIDTHS MAY BE REDUCED BY 4 FEET IF ALL BUILDINGS ARE SPRINKLERED.
- A FIRE DEPARTMENT ACCESS ROAD SHALL EXTEND TO WITHIN 50 FEET OF A SINGLE EXTERIOR DOOR PROVIDING ACCESS TO THE INTERIOR OF THE BUILDING.
- A FIRE APPARATUS ACCESS ROAD SHALL BE REQUIRED WHEN ANY PORTION OF AN EXTERIOR WALL OF THE FIRST STORY IS LOCATED MORE THAN 150 FEET FROM A FIRE DEPARTMENT VEHICLE ACCESS. THIS DISTANCE COULD BE INCREASED TO 250 FEET IF THE BUILDING IS SPRINKLERED.
- APPROVED SECONDARY FIRE APPARATUS ACCESS SHALL BE PROVIDED FOR 100 OR MORE DWELLING UNITS, ROAD(S) WITH DEAD-ENDS OR WITH A SINGLE POINT OF ACCESS IN EXCESS OF 600 FEET, AND FOR ALL COMMERCIAL, INDUSTRIAL, AND MULTI-FAMILY RESIDENTIAL DEVELOPMENTS.
- ALL DEAD-END FIRE APPARATUS ACCESS ROADS AND/OR FIRE LANES, PUBLIC OR PRIVATE, IN EXCESS OF 150 FEET IN LENGTH SHALL BE PROVIDED WITH AN APPROVED TURN AROUND AREA HAVING A MINIMUM DIAMETER OF 81 FEET.
- ALL FIRE APPARATUS ACCESS ROADS SHALL BE MARKED BY PLACING APPROVED SIGNS AT THE START OF THE DESIGNATED FIRE LANE, ONE SIGN AT THE END OF THE FIRE LANE AND WITH SIGNS AT INTERVALS 100 FEET ALONG ALL DESIGNATED FIRE LANES. SIGNS TO BE PLACED ON BOTH SIDES OF AN ACCESS ROADWAY IF NEEDED TO PREVENT PARKING ON EITHER SIDE. SIGNS TO BE INSTALLED NO HIGHER THAN 10 FEET OR LESS THAN 6 FEET FROM ROADWAY LEVEL. THE CURB ALONG OR ON THE PAVEMENT OR CEMENT IF A CURB IS NOT PROVIDED SHALL BE PAINTED WITH A RED WEATHER RESISTANT PAINT IN ADDITION TO THE SIGNS.
- ELECTRICALLY CONTROLLED ACCESS GATES SHALL BE PROVIDED WITH AN APPROVED EMERGENCY VEHICLE DETECTOR/RECEIVER SYSTEM. SAID SYSTEM SHALL BE INSTALLED IN ACCORDANCE WITH THE CITY OF LAS VEGAS GUIDELINES FOR AUTOMATIC EMERGENCY VEHICLE ACCESS GATES.

CITY FIRE MARSHAL

DATE

REVISED 03/19/04

CITY OF LAS VEGAS STREETLIGHT NOTES

- ALL STREET LIGHTING INSTALLATIONS SHALL BE IN ACCORDANCE WITH THE STREET LIGHTING PLANS, THE "UNIFORM STANDARD SPECIFICATIONS FOR PUBLIC WORKS CONSTRUCTION OFF-SITE IMPROVEMENTS, CLARK COUNTY AREA, NEVADA," LATEST EDITION, AND THE "UNIFORM STANDARD DRAWINGS FOR PUBLIC WORKS CONSTRUCTION OFF-SITE IMPROVEMENTS, CLARK COUNTY AREA, NEVADA," LATEST EDITION.
- NO DEVIATION OF STREET LIGHT, PULL BOX, CONDUITS (ETC.) LOCATIONS SHALL BE PERMITTED WITHOUT WRITTEN APPROVAL OF THE TRAFFIC/ELECTRICAL FIELD OPERATIONS DIVISION AND THE CITY ENGINEER. ANY DEVIATION FROM THE PLAN LOCATION WILL REQUIRE COMPLIANCE WITH SECTION 623.10.03 (E) OF THE SPECIFICATIONS.
- ALL EXISTING STREET LIGHTING SHALL REMAIN OPERATIONAL DURING CONSTRUCTION.
- ALL EMPTY CONDUIT SHALL HAVE PULL STRINGS INSTALLED PRIOR TO FINAL INSPECTION.
- ANY STRUCTURE SUCH AS BLOCK WALLS, CHAIN LINK FENCES, RETAINING WALLS, ETC., SHALL LEAVE A MINIMUM CLEARANCE OF EIGHTEEN INCHES (18") TO THE FACE OF STREET LIGHTING POLE ON ALL SIDES WHEN STREETLIGHT IS INSTALLED BEHIND SIDEWALK, AND SHALL AT NO TIME COMPLETELY ENCLOSE THE STREET LIGHTING POLE.
- AS-BUILT DRAWINGS SHALL BE SUPPLIED TO THE ELECTRICAL SERVICES SECTION PRIOR TO ANY PRE-FINAL INSPECTION. THE AS-BUILT DRAWING NEEDS TO BE STAMPED AS-BUILT AND SIGNED BY THE PREPARER.
- SERVICE POINT SHALL BE COORDINATED WITH NEVADA POWER COMPANY, AND WHEREVER POSSIBLE, BE LOCATED NEAR THE CENTER OF THE CIRCUIT. SERVICE POINTS SHALL BE SHOWN ON THE PLANS.
- IT SHALL BE ASSUMED THAT IN THE ABSENCE OF AN EXISTING WORKABLE CIRCUIT TO ATTACH TO, ALL INSTALLATIONS SHALL REQUIRE A NEW SERVICE FOR OPERATION OF THE CIRCUIT.
- WHEREVER THERE IS AN OVERHEAD UTILITY THAT MAY CONFLICT WITH THE INSTALLATION OF STREET LIGHTING CIRCUITS AND/OR POLES, THESE CONFLICTS MUST BE RESOLVED BETWEEN THE DEVELOPER AND THE UTILITIES INVOLVED BEFORE STREETLIGHT BASES ARE INSTALLED AT NO EXPENSE TO THE CITY OF LAS VEGAS.
- THE CONTRACTOR SHALL FURNISH COMPLETE SERVICE TO TRANSFORMERS AND CONTROL SYSTEMS IF REQUIRED ON PLANS.

LAS VEGAS VALLEY WATER DISTRICT STANDARD NOTES

LVVWD PROJECT#

- NO WORK SHALL BEGIN UNTIL THE WATER PLANS HAVE BEEN APPROVED FOR CONSTRUCTION BY THE LVVWD. FOLLOWING WATER PLAN APPROVAL, NOTICE SHALL BE GIVEN TO THE LVVWD COMMUNICATION SUPPORT CENTER (258-7171) TWO (2) WORKING DAYS PRIOR TO THE START OF CONSTRUCTION. FOR FUTURE INSPECTIONS, NOTICE MUST BE GIVEN BY 2:00 P.M. THE BUSINESS DAY PRIOR TO THE REQUESTED LVVWD WHEN REQUESTING INSPECTIONS, PLEASE REFER TO THE PROJECT # IDENTIFIED ABOVE.
- ALL WORK SHALL CONFORM TO LVVWD STANDARD PLATES, DRAWINGS, AND SPECIFICATIONS, AND TO THE 2003 EDITION OF THE UNIFORM DESIGN AND CONSTRUCTION STANDARDS FOR POTABLE WATER SYSTEMS.
- ALL WORK, EXCEPT AS MODIFIED BY THESE PLANS OR BY NOTE 2 ABOVE, SHALL BE DONE IN ACCORDANCE WITH THE MOST RECENT DRAFT OR EDITION OF THE UNIFORM STANDARD SPECIFICATION FOR PUBLIC WORKS CONSTRUCTION OFFSITE IMPROVEMENT, CLARK COUNTY AREA.
- A SINGLE PIPE MATERIAL SHALL BE USED THROUGHOUT THE PROJECT UNLESS OTHERWISE APPROVED BY (UDACS).
- ALL SERVICE LATERALS TWO (2) INCHES IN DIAMETER AND SMALLER SHALL BE TYPE K COPPER TUBING WITH LVVWD APPROVED SERVICE SADDLES.
- ALL WATER METER BOXES SHALL BE LOCATED OUTSIDE OF DRIVEWAYS, VALLEY AND CURB GUTTERS.
- THE VALVES SHALL BE LOCATED OUTSIDE OF DRIVEWAYS, VALLEY AND CURB GUTTERS.
- ALL WATER AND STORM DRAIN OR SANITARY SEWER CROSSINGS SHALL CONFORM TO SECTION 2.19 OF THE 2003 EDITION OF THE UDACS.
- ALL WATER FACILITIES SHALL BE FILLED, DISINFECTED, PRESSURE TESTED, FLUSHED, FILLED, AND AN ACCEPTABLE WATER SAMPLE OBTAINED, PRIOR TO CONNECTION TO THE LVVWD DISTRIBUTION SYSTEM.
- THE CONTRACTOR MUST OBTAIN ALL METERS TWO (2) INCHES AND SMALLER FROM LVVWD CENTRAL STORES. TELEPHONE 258-3152 OR 258-3802, TWO (2) WORKING DAYS PRIOR TO METER PICKUP.
- ANY INTERRUPTION OF SERVICE MUST BE APPROVED BY THE LVVWD INSPECTION DIVISION PRIOR TO SHUTDOWN. PROPER WRITTEN NOTIFICATION MUST BE GIVEN TO ALL AFFECTED CUSTOMERS.
- ALL WATER FACILITY CONSTRUCTION MATERIALS USED MUST BE AS LISTED ON THE LVVWD PRE-APPROVED MATERIALS AND MANUFACTURER'S LISTING FOR NEW FACILITIES, LATEST REVISION, OR SPECIFICALLY APPROVED ON THESE PLANS.
- TELEPHONE "CALL BEFORE YOU DIG" AT 1-800-227-2600.

LAS VEGAS VALLEY WATER DISTRICT

DATE

CITY OF LAS VEGAS TRAFFIC NOTES

- ALL CONSTRUCTION SIGNING, BARRICADE AND TRAFFIC DELINEATION SHALL CONFORM TO THE "MANUAL ON UNIFORM TRAFFIC DEVICES", LATEST EDITION.
- THE STREET SIGN CONTRACTOR SHALL OBTAIN STREET NAMES AND BLOCK NUMBERING FROM THE PLANNING DEPARTMENT PRIOR TO CONSTRUCTION.
- BEFORE ANY WORK IS STARTED IN THE RIGHT-OF-WAY, THE CONTRACTOR SHALL INSTALL ALL ADVANCED WARNING SIGNS FOR THE CONSTRUCTION ZONES. THE CONTRACTOR SHALL INSTALL TEMPORARY STOP SIGNS AT ALL NEW STREET ENCROACHMENTS INTO EXISTING CITY STREETS WHERE WARRANTED IMMEDIATELY AFTER FIRST GRADING WORK IS COMPLETED, AND SHALL MAINTAIN SAID SIGNS UNTIL PERMANENT SIGNS ARE INSTALLED.
- WHEN A DESIGNATED "SAFE ROUTE TO SCHOOL" IS ENCRONCHED UPON BY A CONSTRUCTION WORK ZONE AND PUBLIC WORKS STAFF IDENTIFIES A NEED FOR STUDENTS TO BE ASSISTED IN THE SAFE CROSSING THROUGH THAT WORK ZONE, THE CONTRACTOR SHALL BE REQUIRED TO PROVIDE A QUALIFIED "CROSSING GUARD". THE GUARD SHALL BE PRESENT FOR THE FULL DURATION OF TIME THAT CHILDREN ARE LIKELY TO BE PRESENT.
- IF THE IMPROVEMENTS NECESSITATE THE OBLITERATION, TEMPORARY OBSTRUCTION, TEMPORARY REMOVAL OR RELOCATION OF ANY EXISTING TRAFFIC PAVEMENT MARKING, SUCH PAVEMENT MARKING SHALL BE RESTORED OR REPLACED WITH LIKE MATERIALS TO THE SATISFACTION OF THE CITY TRAFFIC ENGINEER.
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR PROVIDING AND INSTALLING ALL PERMANENT SIGNS SHOWN ON THE PLANS. STREET NAMES SIGNS SHALL CONFORM IN THEIR ENTIRETY TO CURRENT CITY STANDARDS. ALL OTHER SIGNS SHALL BE STANDARD SIZE UNLESS OTHERWISE SPECIFIED ON THE PLANS. ALL SIGN POSTS SHALL BE INSTALLED IN ACCORDANCE WITH THE CURRENT CITY STANDARDS.
- WHEN A PROPOSED STREET LIGHT STANDARD IS LOCATED WITHIN FIVE (5') FEET OF ANY PROPOSED SIGN SHOWN ON THE PLANS TO BE MOUNTED ON A SIGNPOST, THE SIGN SHALL BE MOUNTED ON THE STREET LIGHT STANDARD AND THE SIGNPOST SHALL BE ELIMINATED.
- ALL PERMANENT TRAFFIC CONTROL DEVICES CALLED FOR HEREON SHALL BE IN PLACE AND IN FINAL POSITION PRIOR TO ALLOWING ANY PUBLIC TRAFFIC CONTROL OF THE PORTIONS OF THE ROAD(S) BEING IMPROVED HEREUNDER, REGARDLESS OF THE STATUS OF COMPLETION OF PAVING OR OTHER OFF-SITE IMPROVEMENTS CALLED FOR BY THESE PLANS.
- STREET SIGNS AND STOP SIGNS SHALL BE INSTALLED PER CITY STANDARD SPECIFICATIONS FOR PLACEMENT OF STREET NAME SIGNS.
- THE CONTRACTOR SHALL PROVIDE ALL NECESSARY TRAFFIC CONTROL DEVICES AND FLAGGERS TO ENSURE THE SAFETY OF THE PUBLIC IN OR AROUND THE WORK AREA. THE CONTRACTOR SHALL HAVE A CERTIFIED ATSSA TRAFFIC CONTROL TECHNICIAN OR IMSA WORK ZONE SAFETY SPECIALIST SET-UP, MAINTAIN AND/OR REMOVE ALL TRAFFIC CONTROL DEVICES IN THE CITY OF LAS VEGAS RIGHTS OF WAY.
- WORK IN THE PUBLIC STREETS, ONCE BEGUN, SHALL BE EXPEDITED TO COMPLETION SO AS TO PROVIDE MINIMUM INCONVENIENCE TO ADJACENT PROPERTY OWNERS AND TO THE TRAVELING PUBLIC.
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR NOTIFYING CITIZENS AREA TRANSIT (C.A.T.) IF THE CONSTRUCTION INTERRUPTS OR RELOCATES A BUS STOP OR HAS AN ADVERSE EFFECT ON BUS SERVICE ON THAT STREET TO ARRANGE FOR TEMPORARY RELOCATION OF STOP.
- GUARDS SHALL BE OBTAINED BY CONTACTING THE METROPOLITAN POLICE DEPARTMENT SPECIAL EVENTS UNIT (PHONE NO. 229-3442) WHO WILL PROVIDE OFFICERS PROPERLY TRAINED IN TRAFFIC CONTROL FEES FOR THE USE OF THESE OFFICERS SHALL BE SET UP BY METRO AND WILL BE PAID BY THE CONTRACTOR. THE CONTRACTOR IS RESPONSIBLE FOR ALL ARRANGEMENTS WITH METRO.
- ANY WORK WITHIN 300' OF A SIGNALIZED INTERSECTION WILL BE NIGHT WORK, UNLESS DIRECTED BY THE CITY OF LAS VEGAS TRAFFIC ENGINEER.

DEVIATION FROM STANDARDS

NONE - (PUBLIC)

BASIS OF BEARING

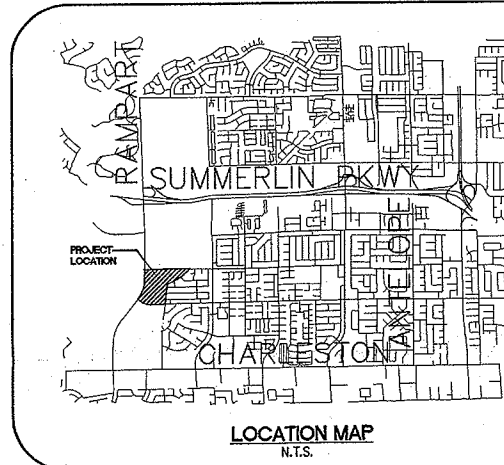
SOUTH 03°32'07" EAST, BEING THE BEARING OF THE CENTERLINE OF "RAMPAUT BOULEVARD" AS SHOWN BY MAP THEREOF ON FILE IN FILE 64, PAGE 03 OF SURVEYS IN THE COUNTY RECORDER'S OFFICE, CLARK COUNTY, NEVADA, LYING WITHIN THE NORTH HALF (N 1/2) OF SECTION 32, TOWNSHIP 20 SOUTH, RANGE 60 EAST, M.D.M., CITY OF LAS VEGAS, CLARK COUNTY, NEVADA.

BENCHMARK

RIVET AND PLATE IN TOP OF CURB @ TOWN CENTER AND VILLAGE CENTER ON WEST EDGE OF ROUNDABOUT.

CITY OF LAS VEGAS BENCHMARK 01V00 32E6
LOCATED ON THE NORTHEAST CORNER OF ALTA DR. AND UPPER HILL
NAVD 88 ELEVATION = 814.1261 METERS, 2671.02 FEET
SUMMERLIN ELEVATION: 2728.11 FEET

NOTE: ADD 2.27 TO THE CURRENTLY USED SUMMERLIN BENCHMARK TO EQUAL TO THE APPROVED CITY OF LAS VEGAS BENCHMARK.



LEGEND AND ABBREVIATIONS

1 DETAIL DRAWING NUMBER

1 DRAWING NUMBER FOR DETAIL

1 DRAWN ON SAME SHEET

1 DRAWING NUMBER FOR DETAIL WITH REFERENCE TO IT'S SHEET

INDICATES SEWER MANHOLE IN PROFILE

INDICATES STORM DRAIN MANHOLE IN PROFILE

EXIST. ELEVATION

PROPOSED ELEVATION

EXIST. SPOT ELEVATION

AS-BUILT ELEVATION

SUBDIVISION BOUNDARY

EASEMENT LINE

FUTURE LINE

STREET CENTERLINE

CONCRETE CURB & GUTTER

EXISTING IMPROVEMENTS

EXISTING ASPHALT

EXISTING GROUND CONTOURS

FINISH GROUND CONTOUR

DRAINAGE FLOW LINE

RETAINING WALL

EXISTING BLOCK WALL

EXISTING LOT NUMBER

LOT NUMBER

PAD ELEVATION

FINISH FLOOR ELEVATION

SCARP

EXISTING PAD ELEVATION

BLOCK NUMBER

PROPERTY LINE

FIRE HYDRANT

ABBREVIATIONS

HOA = HOME OWNER ASSOCIATION

W = WATER

SS = SEWER

G = GAS

SD = STORM DRAIN

SL = STREET LIGHT

SMH = SEWER MANHOLE

SDMH = STORM DRAIN MH

CLV = CITY OF LAS VEGAS

LVVWD = LAS VEGAS VALLEY

WATER DISTRICT

EX = EXISTING

FL = FLOW LINE

HP = HIGH POINT

R/W = RIGHT-OF-WAY

TO = TOP BACK OF CURB

FG = FINISHED GRADE

BOR = BEGIN CURB RETURN

DS = DOWN SPOUT

USDOCA = UNIFORM STANDARD

DRAWING CLARK

COUNTY AREA

CF = CURB FACE

BW = BACK OF WALK

FS = FINISH SURFACE

NG = NATURAL GRADE

FF = FINISH FLOOR

GB = GRADE BREAK

FUT = FUTURE

EP = EDGE OF PAVEMENT

NP = NEVADA POWER

UDACS = UNIFORM DESIGN

AND CONSTRUCTION

STANDARDS

TR = TOP OF RETAINING

FN = FENCE

HDPE = HIGH DENSITY

POLYETHYLENE

THE VILLAGE AT QUEENSBIDGE CULVERT

JMA ARCHITECTURE STUDIOS

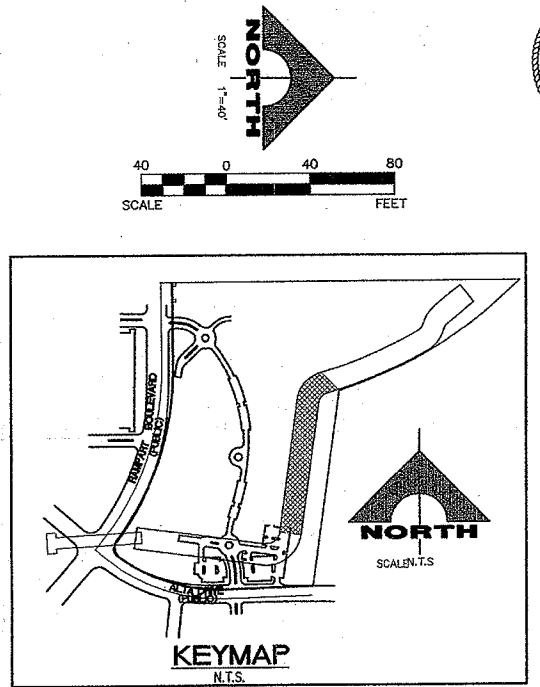
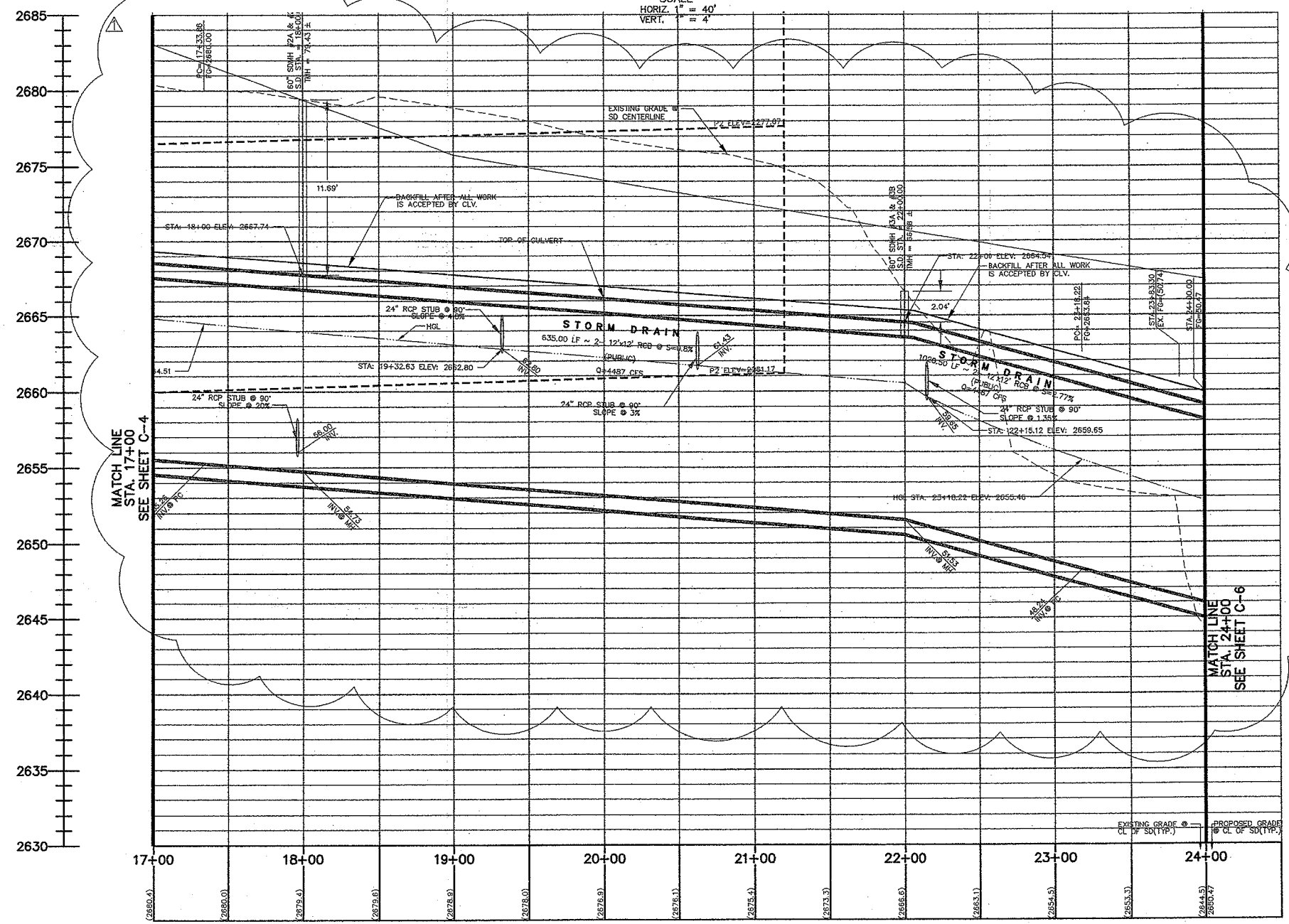
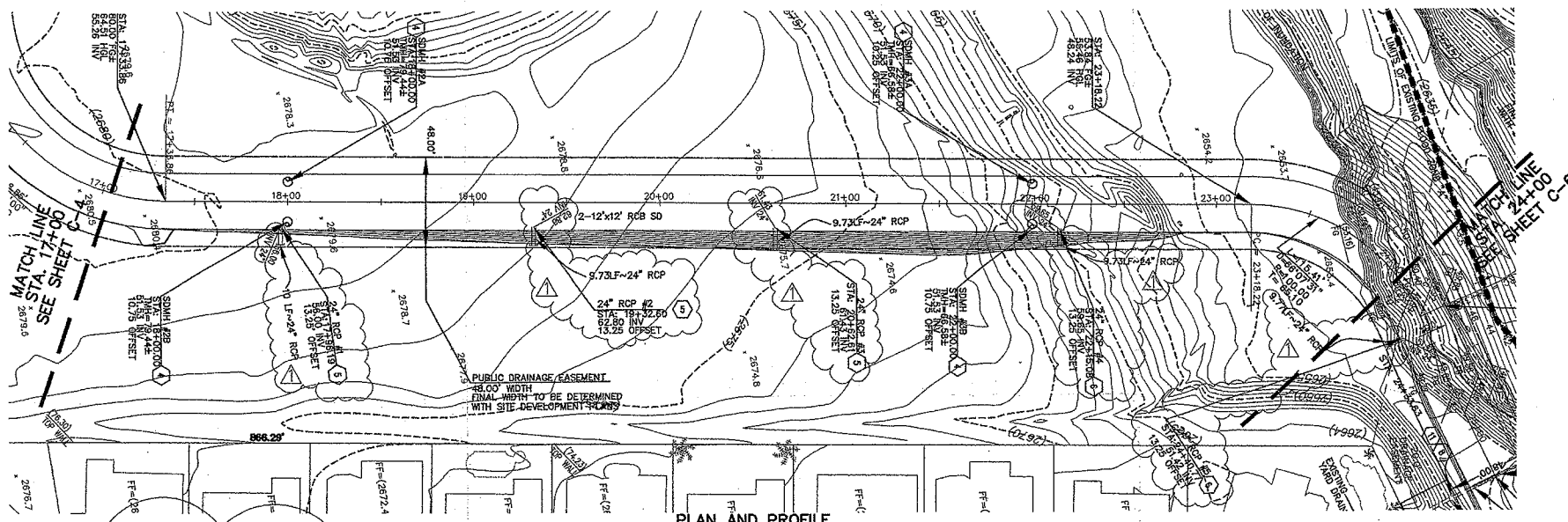
GENERAL NOTES

DRAWING

C-2

2 OF 11 SHTS

CLV DWG #



BASIS OF BEARING
 SOUTH 00°32'07" EAST, BEING THE BEARING OF THE CENTERLINE OF "RAMPART BOULEVARD" AS SHOWN BY MAP THEREOF ON FILE IN FILE 64, PAGE 93 OF SURVEYS IN THE COUNTY RECORDER'S OFFICE, CLARK COUNTY, NEVADA, LYING WITHIN THE NORTH HALF (N 1/2) OF SECTION 32, TOWNSHIP 20 SOUTH, RANGE 60 EAST, M.D.M., CITY OF LAS VEGAS, CLARK COUNTY, NEVADA.

BENCHMARK
 RIVET AND PLATE IN TOP OF CURB @ TOWN CENTER AND VILLAGE CENTER ON WEST EDGE OF ROUNDABOUT.
 CITY OF LAS VEGAS BENCHMARK 01V00 3265
 LOCATED ON THE NORTHEAST CORNER OF ALTA DR. AND UPPER HILL. NAVD 88 ELEVATION = 514.1251 METERS, 2671.02 FEET. SUMMERLIN ELEVATION: 2726.11 FEET
 NOTE: ADD 2.27' TO THE CURRENTLY USED SUMMERLIN BENCHMARK TO EQUAL TO THE APPROVED CITY OF LAS VEGAS BENCHMARK.

- GRADING CONSTRUCTION NOTES**
- CONTRACTOR TO MATCH TO EXISTING 2'-12" RCP CULVERT.
 - CONSTRUCT 2'-12" RCP CULVERT PER DETAIL 8-201.3 & TRENCH RCP SECTION PER DETAIL 1, SHEET C-7.
 - CONTRACTOR TO FIELD VERIFY LOCATION OF EXISTING 60" RCP.
 - INSTALL 60" STORM DRAIN MANHOLE PER DETAIL 8-4.7.1, OR CLARK COUNTY STANDARD DRAWING #403.
 - INSTALL 24" CLASS V RCP STUB PER DETAIL 2, SHEET C-7.
 - INSTALL 24" CLASS IV RCP STUB PER DETAIL 2, SHEET C-7.
 - INSTALL EQUALIZATION CHAMBER PER DETAIL A, SHEET C-7.
 - CONTRACTOR TO FIELD VERIFY LOCATION OF EXISTING 18" RCP.
 - CONSTRUCT RCP CULVERT TYPE I HEADWALLS PER DETAIL 8-201.3.
 - NOT USED
 - CONSTRUCT LATERAL PER DETAIL 2, SHEET C-7.
 - CONCRETE PAD PER DETAIL "C" SHEET C-7.

NOTE
 12" X 12" BOX IS DESIGNED FOR MAX 20' OF FILL PER NEVADA DEPARTMENT OF TRANSPORTATION STANDARDS.

NOTE
 THIS PROJECT SITE IS LOCATED WITHIN "THE LIMITS OF EXISTING FLOOD ZONE A".



DATE: 12/14/05

DESIGNED/DESIGNED/ENR: [blank]

DRAWN/DESIGNED/ENR: [blank]

CHECKED/DESIGNED/ENR: [blank]

ISSUE DATE: [blank]

ISSUE DATE: [blank]

PLOT DATE: 12/13/05

PLOT TIME: 11:30:45

THE VILLAGE AT QUEENSRIDGE CULVERT

JMA ARCHITECTURE STUDIOS

STORM DRAIN PLAN AND PROFILE

STA. 17+00.00 TO 24+00.00

DRAWING

C-5

5 OF 11 SHTS

ISSUED FOR DRAINAGE SUBMITTAL



DATE: 3/21/09

DATE: 3/21/09

DATE: 3/21/09

DATE: 3/21/09

DATE: 3/21/09

DATE: 3/21/09

DATE: 3/21/09

DATE: 3/21/09

DATE: 3/21/09

DATE: 3/21/09

THE VILLAGE AT QUEENSHIRE CULVERT

JMA ARCHITECTURE STUDIOS

DETAILS SHEET

G.C. WALLACE, INC.
Engineers/Planners/Surveyors
1555 SOUTH RANCHO BLVD., LAS VEGAS, NEVADA 89146
TELEPHONE: (702) 804-2000 • FAX: (702) 804-2299
G:\e19-295\Drawings\DRAINAGE\1105\QUEENSHIRE.dwg

DESIGN: JG/GS

DRAWN: GOS

CHECKED: RUC

ISSUE DATE:

PLOT DATE: 03-29-09

PLOT TIME: 13:19:56

DESCRIPTION

ISSUED FOR DRAINAGE SUBMITTAL

BASIS OF BEARING
SOUTH 00°32'07" EAST, BEING THE BEARING OF THE CENTERLINE OF "RAMPART BOULEVARD" AS SHOWN BY MAP THEREOF ON FILE IN FILE 64, PAGE 93 OF SURVEYS IN THE COUNTY RECORDER'S OFFICE, CLARK COUNTY, NEVADA, LYING WITHIN THE NORTH HALF (N 1/2) OF SECTION 32, TOWNSHIP 20 SOUTH, RANGE 60 EAST, M.D.M., CITY OF LAS VEGAS, CLARK COUNTY, NEVADA.

BENCHMARK
RIVET AND PLATE IN TOP OF CURB @ TOWN CENTER AND VILLAGE CENTER ON WEST EDGE OF ROUNDABOUT.

CITY OF LAS VEGAS BENCHMARK QLV00 3266
LOCATED ON THE NORTHEAST CORNER OF ALTA DR. AND UPPER HILL
NAVD 88 ELEVATION = 814.1261 METERS, 2671.02 FEET
SUMMERLIN ELEVATION: 2726.11 FEET
NOTE: ADD 2.27' TO THE CURRENTLY USED SUMMERLIN BENCHMARK TO EQUAL TO THE APPROVED CITY OF LAS VEGAS BENCHMARK.

Avoid cutting underground utility lines. It's costly.
Call before you Dig.
1-800-227-2600
UNDERGROUND SERVICE (USA)

AVOID HITTING OVERHEAD POWER LINES. IT'S COSTLY.
CALL BEFORE YOU DIG OVERHEAD
1-702-227-2929

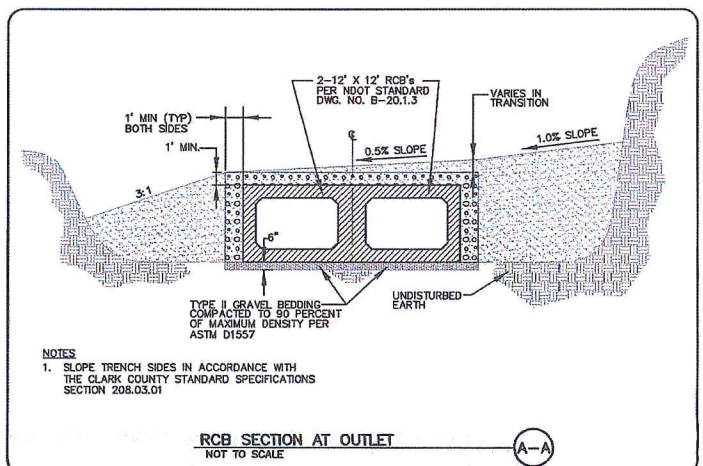
Call before you UnderGround
1-702-455-7511
1-702-229-6611

NOTE
THIS PROJECT SITE IS LOCATED WITHIN "THE LIMITS OF EXISTING FLOOD ZONE A".

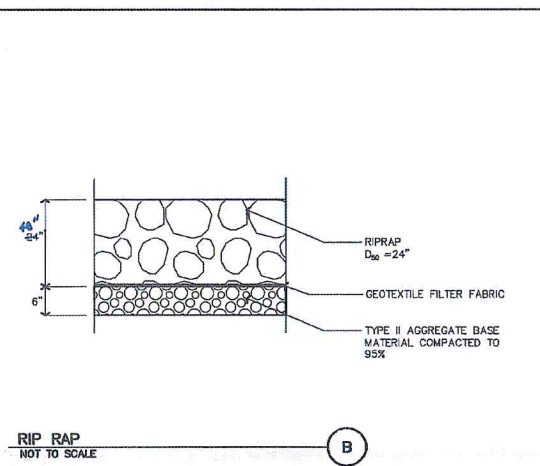
CLV DWG #

DRAWING
C-7

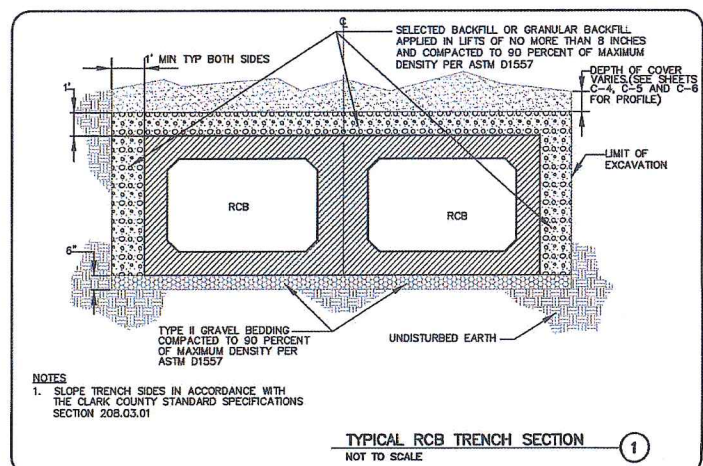
7 OF 11 SHTS



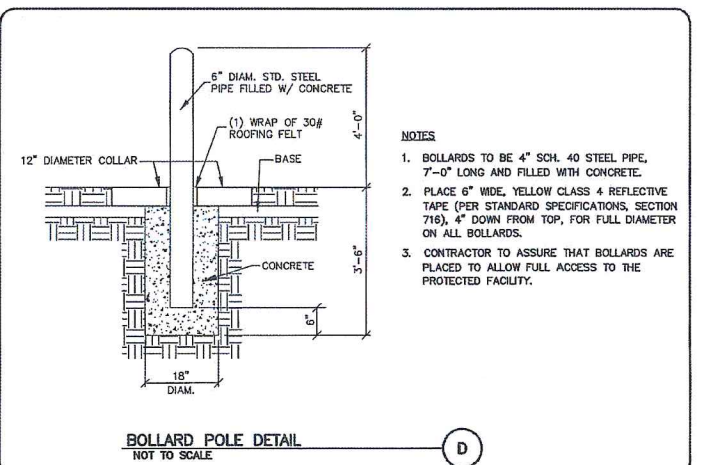
RCB SECTION AT OUTLET
NOT TO SCALE



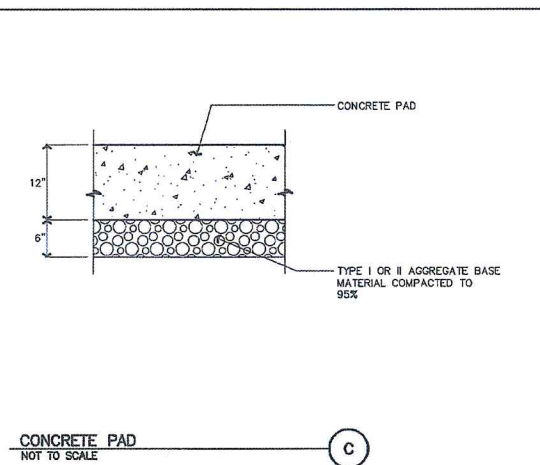
RIP RAP
NOT TO SCALE



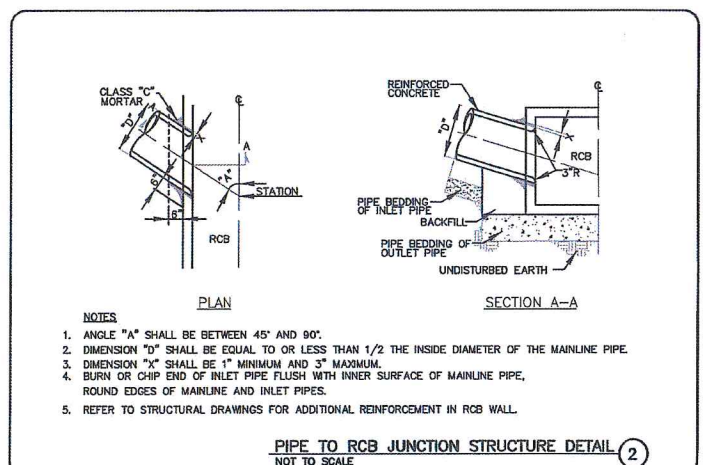
TYPICAL RCB TRENCH SECTION
NOT TO SCALE



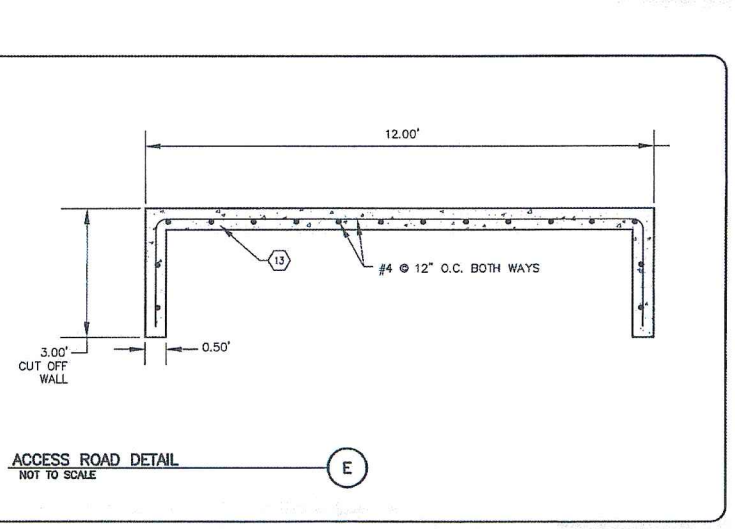
BOLLARD POLE DETAIL
NOT TO SCALE



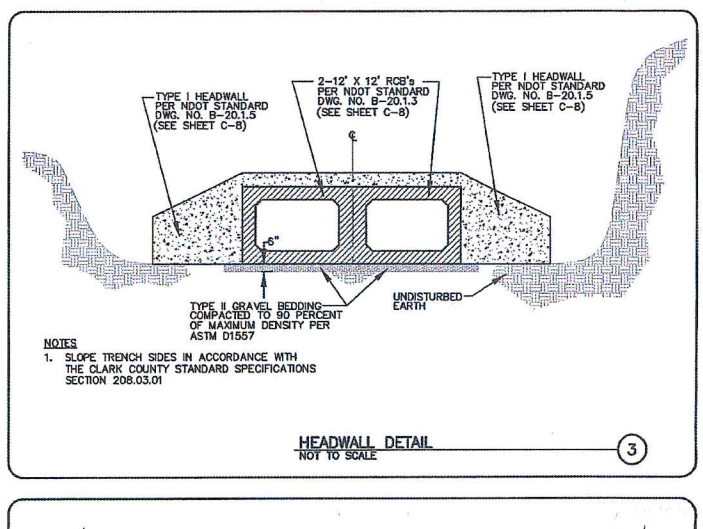
CONCRETE PAD
NOT TO SCALE



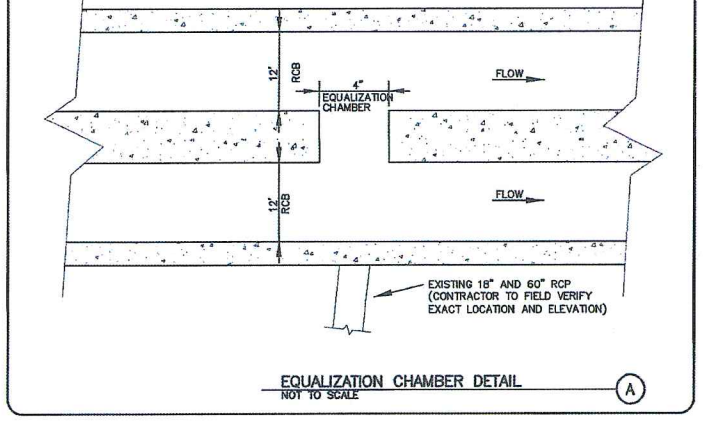
PIPE TO RCB JUNCTION STRUCTURE DETAIL
NOT TO SCALE



ACCESS ROAD DETAIL
NOT TO SCALE



HEADWALL DETAIL
NOT TO SCALE



EQUALIZATION CHAMBER DETAIL
NOT TO SCALE

TYPICAL SECTION - SPANS 5' THRU 8'

TYPICAL SECTION - SPANS 10' THRU 14'

NOTES:

- FOR BOXES WITH SPAN OR HEIGHT LESS THAN ANY OF THOSE SHOWN IN TABLE, USE NEXT GREATER SIZE BOX. PROVIDE SLOTTED END RINGS AND REINFORCEMENT, MAKE NECESSARY CHANGES IN BAR LENGTHS AND QUANTITIES.
- FOR BOXES WITH SPAN OR HEIGHT OR COVER GREATER THAN THOSE SHOWN IN TABLE, A SPECIAL DESIGN IS REQUIRED.
- QUANTITIES ARE APPROXIMATE AND FOR DESIGN PURPOSES ONLY.
- IT IS FEASIBLE TO ENLARGE THE 180° HOLES ON EVERY OTHER "B" BAR.
- "B" BARS ARE AT HALF SPACING.
- PROVIDE PAVING THICKNESS TOP SLAB IS EXPOSED AND WORKS P.L.C. PAYMENT OR APPROACH ROAD IS USED, ADJUST THE QUANTITIES.
- WHEN TOP IS EXPOSED, THE TOP SLAB CONCRETE SHALL BE "C", $f_c=4500$ PSI, OR "A", $f_c=4000$ PSI, AS DETERMINED BY THE ENGINEER. IF "A" CONCRETE IS TO BE USED, THE TOP SLAB REINFORCING STEEL SHALL HAVE AN EPOXY COATING.

STATE OF INDIANA
DEPARTMENT OF TRANSPORTATION
**DOUBLE
RCB CULVERTS**

DATE: 8-28-13 (S)
DRAWN: BRIDGE DESIGN GROUP
CHECKED: J. L. HARRIS

SOUTH 00°32'07" EAST, BEING THE BEARING OF THE CENTERLINE OF "RAMPART BOULEVARD" AS SHOWN BY MAP THEREON ON FILE IN FILE 64, PAGE 93 OF SURVEYS IN THE COUNTY RECORDER'S OFFICE, CLARK COUNTY, NEVADA, LYING WITHIN THE NORTH HALF (N. 1/2) OF SECTION 32, TOWNSHIP 20 SOUTH, RANGE 60 EAST, M.D.M., CITY OF LAS VEGAS, CLARK COUNTY, NEVADA.

RIVET AND PLATE IN TOP OF CURB @ TOWN CENTER AND VILLAGE CENTER ON WEST EDGE OF ROUNDABOUT.

CITY OF LAS VEGAS BENCHMARK GLV00 32E6
LOCATED ON THE NORTHEAST CORNER OF ALTA DR. AND UPPER HILL.
NAVD 88 ELEVATION = 814.1281 METERS, 2671.02 FEET
SUMMERLIN ELEVATION: 2726.11 FEET

NOTE: ADD 2.27' TO THE CURRENTLY USED SUMMERLIN BENCHMARK TO EQUAL TO THE APPROVED CITY OF LAS VEGAS BENCHMARK.

NOTE
THIS PROJECT SITE IS LOCATED WITHIN
"THE LIMITS OF EXISTING FLOOD ZONE A".

**Call
before you
Dig.
1-800-227-2600
UNDERGROUND SERVICE (USA)**



CLY DWG #

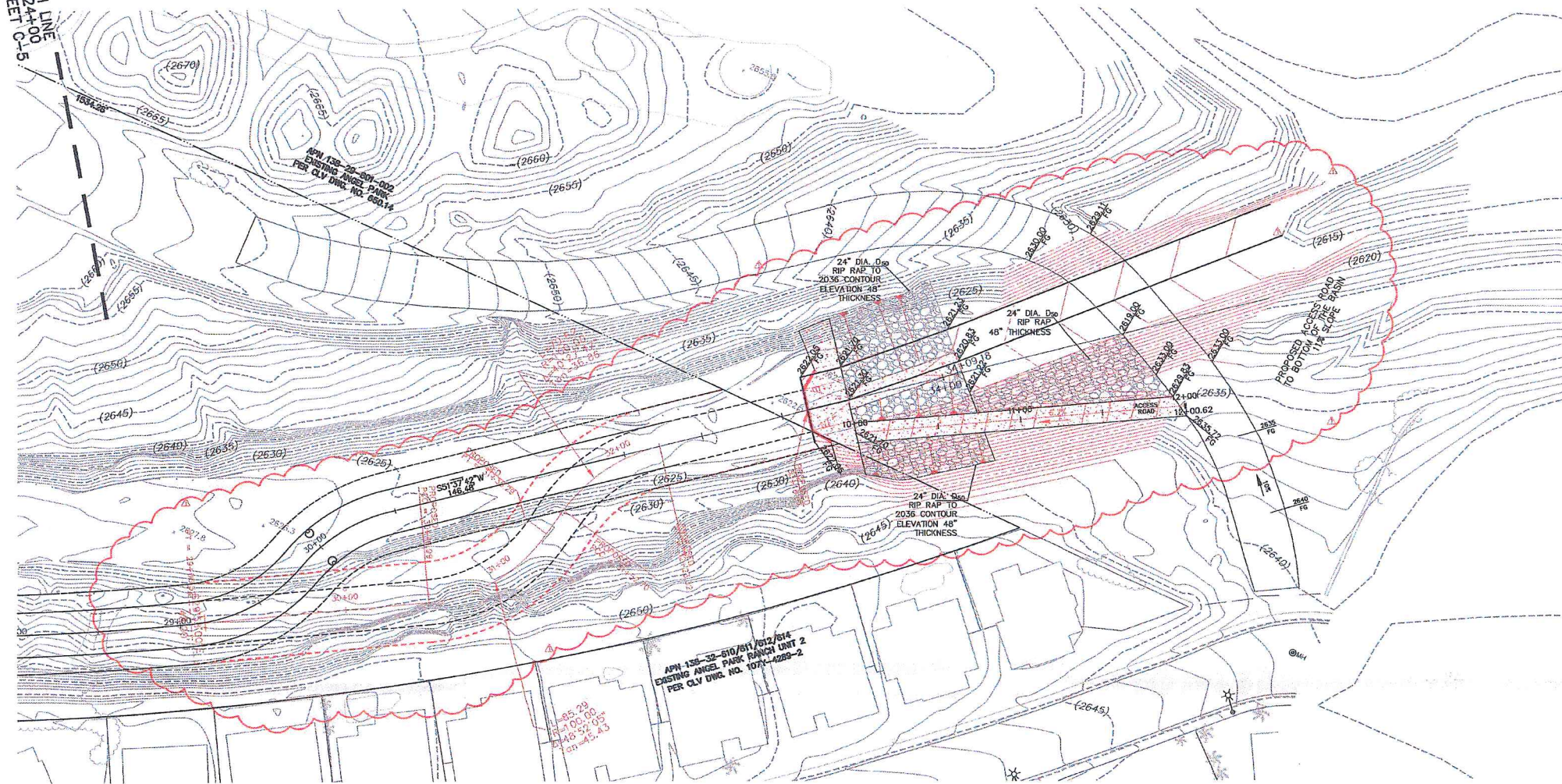
THE VILLAGE AT QUEENSBIDGE CULVERT

JMA ARCHITECTURE STUDIOS

DRAWING
C-8

8 OF 11 SHOTS

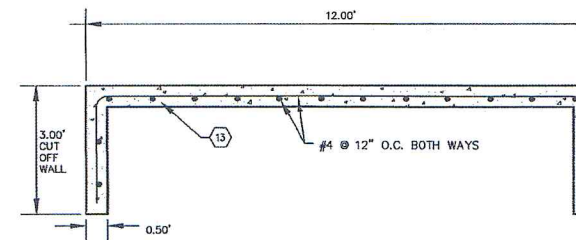
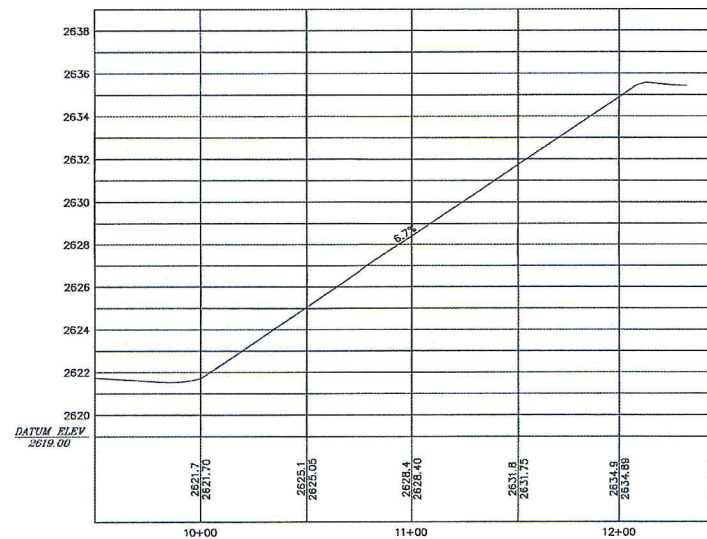
MATCH LINE
STA. 24+00
SEE SHEET C-5



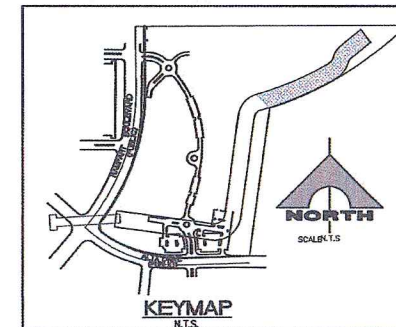
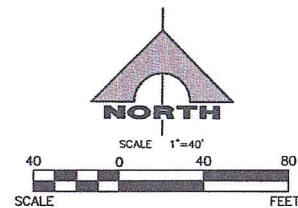
ACCESS ROAD
PLAN AND PROFILE
SCALE
HORIZ. 1" = 40'
VERT. 1" = 4'

**GRADING
CONSTRUCTION NOTES**

- (1) CONTRACTOR TO MATCH TO EXISTING 2'-12"x12" RCB CULVERT.
- (2) CONSTRUCT 2'-12"x12" RCB CULVERT PER NDOT DETAIL B-20.1.3 & TRENCH RCB SECTION PER DETAIL 1, SHEET C-7.
- (3) CONTRACTOR TO FIELD VERIFY LOCATION OF EXISTING 60" RCP.
- (4) INSTALL 60" STORM DRAIN MANHOLE PER CLARK COUNTY STANDARD DRAWING #403.
- (5) INSTALL 24" CLASS V RCP STUB PER DETAIL 2, SHEET C-7.
- (6) INSTALL 24" CLASS IV RCP STUB PER DETAIL 2, SHEET C-7.
- (7) INSTALL EQUALIZATION CHAMBER PER DETAIL A, SHEET C-7.
- (8) CONTRACTOR TO FIELD VERIFY LOCATION OF EXISTING 18" RCP.
- (9) CONSTRUCT RCB CULVERT TYPE I HEADWALLS PER NDOT DETAIL B-20.1.5.
- (10) NOT USED.
- (11) CONSTRUCT LATERAL PER DETAIL 2, SHEET C-7.
- (12) CONCRETE PAD PER DETAIL "C" SHEET C-7.
- (13) 6" CLASS "A" CONCRETE, #4 BARS 12" O.C. BOTH WAYS AT THE CENTER OF SLAB. SEE DETAIL ON SHEET C-9.



ACCESS ROAD DETAIL
SECTION "A"



BASIS OF BEARING

SOUTH 00°32'07\"/>

BENCHMARK

RIVET AND PLATE IN TOP OF CURB @ TOWN CENTER AND VILLAGE CENTER ON WEST EDGE OF ROUNDABOUT.

CITY OF LAS VEGAS BENCHMARK 01V00 3268
LOCATED ON THE NORTHEAST CORNER OF ALTA DR. AND UPPER HILL.
NAVD 88 ELEVATION = 814.1281 METERS, 2671.02 FEET
SUMMERLIN ELEVATION: 2726.11 FEET

NOTE: ADD 2.27' TO THE CURRENTLY USED SUMMERLIN BENCHMARK TO EQUAL TO THE APPROVED CITY OF LAS VEGAS BENCHMARK.

NOTE

THIS PROJECT SITE IS LOCATED WITHIN "THE LIMITS OF EXISTING FLOOD ZONE A".



Call before you Dig.
1-800-227-2600
UNDERGROUND SERVICE (USA)



CLV DWG # 107Y-4889-CUL



DATE: 12/1/06

REV.	DATE	DESCRIPTION
1	12/1/06	ISSUED FOR DRAINAGE SUBMITTAL

G. C. WALLACE, INC.
Engineers/Planners/Surveyors
1555 SOUTH RANCHO BLVD., LAS VEGAS, NEVADA 89109
TEL: (702) 731-1100 FAX: (702) 731-1101
E-mail: gwallace@wallaceinc.com

THE VILLAGE AT QUEENSBIDGE CULVERT
JMA ARCHITECTURE STUDIOS
CHANNEL REGRADING PLAN
STA. 24+00.00 TO 39+00.00

DRAWING
C-9

9 OF 11 SHTS


```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   JUN 1998
*   VERSION 4.1
*
* RUN DATE 23JUN08 TIME 10:11:08
*
*****
ALLGOW3.OUT
*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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X   X   XXXXXX   XXXXX   X
X   X   X   X   X   XX
X   X   X   X   X   X
XXXXXX XXXX   X   XXXXX   X
X   X   X   X   X   X
X   X   X   X   X   X
X   X   XXXXXX   XXXXX   XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*** FREE ***
1 ID CLARK COUNTY REGIONAL FLOOD CONTROL DISTRICT 2008 MASTER PLAN UPDATE
2 ID GOWAN WATERSHED (ALL)
3 ID RECOMMENDED DRAINAGE SYSTEM WITH ULTIMATE DEVELOPMENT
4 ID INPUT FILE = ALLGOW3.DAT
5 ID INPUT FILE DATE = MAY 5, 2008
6 ID DESIGN STORM = 100-YEAR 6-HR STORM
7 ID STORM DISTRIBUTION = SDN #3
8 ID MODELED BY PBS&J (MICHELE L. D'ALESSANDRO, E.I., CFM)
9 ID CHECKED BY PBS&J (HARSHAL B. DESAI, P.E., CFM)
10 ID STORM CENTERING = FULL WATERSHED
11 ID
12 ID REFERENCED HYDROLOGIC MODELS:
13 ID CITY OF LAS VEGAS CITY WIDE HYDROLOGY ANALYSIS (PBS&J 1997)
14 ID NORTHWEST NEIGHBORHOOD STUDY PHASE 1 (PBS&J 1997)
15 ID RESPONSE TO COMMENTS ON THE 2006 SUMMERLIN WEST PLANNING AREA FLOOD
16 ID CONTROL MASTER PLAN UPDATE (G.C. WALLACE 2006)
17 ID 3RD RESPONSE TO COMMENTS ON THE 2006 SUMMERLIN WEST PLANNING AREA FLOOD
18 ID CONTROL MASTER PLAN UPDATE (G.C. WALLACE 2006)
19 ID SUPPLEMENT FOR THE 2006 SUMMERLIN WEST PLANNING AREA FLOOD CONTROL
20 ID MASTER PLAN UPDATE (G.C. WALLACE 2006)
21 ID GOWAN OUTFALL - LONE MOUNTAIN BRANCH PRELIMINARY DESIGN REPORT
22 ID (G.C. WALLACE 2007)
23 ID LONE MOUNTAIN WESTERN BELTWAY DETENTION BASIN PARAMETERS (RECEIVED
24 ID FROM G.C. WALLACE ON JANUARY 31, 2008)
25 ID US 95/RANCHO FIS RESTUDY (PBS&J 1998)
26 ID JR CARDS CONTAIN DARFS BASED ON THE FOLLOWING VALUES:
27 ID
28 ID AREA DARF
29 ID SQ. MI.
30 ID 0-0.5 0.99
31 ID 0.5-1 0.975
32 ID 1-2 0.95
33 ID 2-3 0.925
34 ID 3-4 0.915
35 ID 4-5 0.908
36 ID 5-6 0.903
37 ID 6-7 0.895
38 ID 7-8 0.885
39 ID
40 ID JR CARD RATIOS REPRESENT DEPTH-AREA REDUCTION FACTORS (DARF'S)
41 ID
42 ID 100-YEAR, 6-HOUR STORM, SDN3
43 ID
44 ID IT 5 0 0 650
45 ID IO 5 0 0
46 ID IN 5 0 0
47 ID JR PREC 0.99 0.975 0.95 0.925 0.915 0.908 0.903 0.895 0.885
*

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1 HEC-1 INPUT PAGE 2

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
48 KK LV29-C
49 BA 0.277
50 PB 2.80
51 PC 0 0.02 0.057 0.07 0.087 0.108 0.124 0.13 0.13 0.13
52 PC 0.13 0.13 0.13 0.133 0.14 0.142 0.148 0.158 0.172 0.181
53 PC 0.19 0.197 0.199 0.2 0.201 0.204 0.214 0.229 0.241 0.249
54 PC 0.251 0.256 0.27 0.278 0.281 0.283 0.295 0.322 0.352 0.409
55 PC 0.499 0.59 0.71 0.744 0.781 0.812 0.819 0.835 0.851 0.856
56 PC 0.86 0.868 0.876 0.888 0.91 0.926 0.937 0.95 0.97 0.976
57 PC 0.982 0.985 0.987 0.989 0.99 0.993 0.993 0.994 0.995 0.998
58 PC 0.998 0.999 1
59 LS 0 90.6
60 UD 0.409
*
61 KK RLV29-C
62 KM ROUTE LV29-C TO CLV30-C
63 KM FACILITY = GOWAN - TENAYA BRANCH
64 KM FACILITY # = GOTE 0000

```

1850 KM CONVERTED TO MUSKINGUM-CUNGE TO ALLGOW3.OUT
1851 RD 1559 0.02 0.04 0 TO ACHIEVE STABILITY 3
* TRAP 100

1

HEC-1 INPUT

PAGE 50

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1852 KK SW11
1853 BA 0.589
1854 PB 3.34
1855 LS 0 87.8
1856 UD 0.311
*

1857 KK RSW11
1858 KM ROUTE SW11 TO CSW17
1859 KM FACILITY = ANGEL PARK - CHARLESTON BOULEVARD
1860 KM FACILITY # = APCB 0064, 0080
1861 KM LINING = RCB
1862 RD 2338 0.0167 0.015 0 TRAP 7 0
*

1863 KK SW17
1864 BA 0.356
1865 PB 3.30
1866 LS 0 87.8
1867 UD 0.271
*

1868 KK CSW17
1869 KM COMBINE RSW11 AND SW17
1870 HC 2
*

1871 KK RCSW17
1872 KM ROUTE CSW17 TO CSW18
1873 KM FACILITY = ANGEL PARK - CHARLESTON BOULEVARD
1874 KM FACILITY # = APCB 0000,0001,0019,0050
1875 KM LINING = RCB
1876 RD 3600 0.014 0.015 0 TRAP 11 0
*

1877 KK SW18
1878 BA 0.405
1879 PB 3.27
1880 LS 0 86.8
1881 UD 0.271
*

1882 KK CSW18
1883 KM COMBINE RCSW17 AND SW18
1884 HC 2
*

1885 KK RCSW18
1886 KM ROUTE CSW18 TO C12A
1887 KM FACILITY = ANGEL PARK SOUTH
1888 KM FACILITY # = APSO 0254,0255,0258,0345,0346; APCB 0000
1889 KM NATURAL WASH
1890 KM LENGTH = 5,200
1891 KM SLOPE = 1.4%

1

HEC-1 INPUT

PAGE 51

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1892 KM N = 0.040
1893 KM HYDRAULIC RADIUS = 1.5
1894 KM VELOCITY = 9.2
1895 RM 2 0.157 0.15
*

1896 KK 12A
1897 BA 0.392
1898 PB 3.20
1899 LS 0 91.2
1900 UD 0.264
*

1901 KK C12A
1902 KM COMBINE 12A AND RCSW18
1903 HC 2
*

1904 KK RC12A
1905 KM ROUTE THRU 12B
1906 KM FACILITY = ANGEL PARK SOUTH
1907 KM FACILITY # = APSO 0204, 0205
1908 KM NATURAL WASH
1909 KM LENGTH = 2,600
1910 KM SLOPE = 3.5%
1911 KM N = 0.040
1912 KM HYDRAULIC RADIUS = 1.5
1913 KM VELOCITY = 14.5
1914 RM 1 0.05 0.15
*

1915 KK 12B
1916 BA 0.260
1917 PB 3.13
1918 LS 0 91.0
1919 UD 0.233
*

1920 KK C12B
1921 KM COMBINE 12B AND RC12A
1922 HC 2
*

1923 KK RC12B
1924 KM ROUTE C12B TO C57B-3
1925 KM FACILITY = ANGEL PARK SOUTH

Begin
Reference

1926 KM FACILITY # = APSO 0067
 1927 KM NATURAL WASH
 1928 KM LENGTH = 6.000
 1929 KM SLOPE = 2.3%
 1930 KM N = 0.040
 1931 KM HYDRAULIC RADIUS = 1.5
 1932 KM VELOCITY = 11.8
 1933 RM 2 0.141 0.15
 *

ALLGOW3.OUT

HEC-1 INPUT

PAGE 52

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1934 KK 57B-3
 1935 BA 0.310
 1936 PB 3.04
 1937 LS 0 82.1
 1938 UD 0.332
 *

1939 KK C57B-3
 1940 KM COMBINE RC128 AND 57B-3
 1941 HC 2
 *

1942 KK RC57B-3
 1943 KM ROUTE C57B-3 TO C57B-2
 1944 KM FACILITY = ANGEL PARK SOUTH
 1945 KM FACILITY # = APSO 0067
 1946 KM NATURAL WASH
 1947 KM LENGTH = 1.300
 1948 KM SLOPE = 1.7%
 1949 KM N = 0.040
 1950 KM HYDRAULIC RADIUS = 1.5
 1951 KM VELOCITY = 10.2
 1952 RM 0 0.035 0.15
 *

1953 KK 57B-2
 1954 BA 0.362
 1955 PB 3.02
 1956 LS 0 84.1
 1957 UD 0.332
 *

1958 KK C57B-2
 1959 KM COMBINE 57B-2 AND RC57B-3
 1960 HC 2
 *

1961 KK RC57B-2
 1962 KM ROUTE C57B-2 TO CC57B-1
 1963 KM FACILITY = ANGEL PARK SOUTH
 1964 KM FACILITY # = APSO 0067
 1965 KM NATURAL WASH
 1966 KM LENGTH = 1.000
 1967 KM SLOPE = 1.8%
 1968 KM N = 0.040
 1969 KM HYDRAULIC RADIUS = 1.5
 1970 KM VELOCITY = 10.5
 1971 RM 0 0.027 0.15
 *

1

HEC-1 INPUT

PAGE 53

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1972 KK 13B-1
 1973 BA 0.249
 1974 PB 3.19
 1975 LS 0 91.6
 1976 UD 0.284
 *

1977 KK RC13B-1
 1978 KM ROUTE 13B-1 TO C13B-2
 1979 KM GRIFFITH PARK DRIVE AND HUALAPAI WAY
 1980 RD 3000 0.018 0.016 0 TRAP 0 50
 *

1981 KK 13B-2
 1982 BA 0.216
 1983 PB 3.14
 1984 LS 0 89.7
 1985 UD 0.231
 *

1986 KK C13B-2
 1987 KM COMBINE 13B-2 AND RC13B-1
 1988 KM HUALAPAI WAY AND LOCAL FACILITY
 1989 HC 2
 *

1990 KK RC13B-2
 1991 KM ROUTE C13B-2 TO CCPIC-A
 1992 KM LINING = GRASS
 1993 RD 4900 0.021 0.03 0 TRAP 40 6
 *

1994 KK 19A
 1995 BA 0.253
 1996 PB 3.25
 1997 LS 0 89.9
 1998 UD 0.351
 *

1999 KK R19A
 2000 KM ROUTE 19A TO C13A-1
 2001 KM UNNAMED ROAD
 2002 RD 4300 0.021 0.016 0 TRAP 0 50
 *

2003 KK 13A-1
 2004 BA 0.224
 2005 PB 3.19
 2006 LS 0 91.4
 2007 UD 0.302
 *

1

HEC-1 INPUT

PAGE 54

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2008 KK C13A-1
 2009 KM COMBINE 13A-1 AND R19A
 2010 KM TOWN CENTER DRIVE AND SWALE
 2011 HC 2
 *

2012 KK RC13A-1
 2013 KM ROUTE C13A-1 TO C13A-2
 2014 KM NATURAL WASH
 2015 KM TRAVEL LENGTH = 2,800
 2016 KM SLOPE = 2.1%
 2017 KM N = 0.040
 2018 KM HYDRAULIC RADIUS = 1.5
 2019 KM VELOCITY = 11.4
 2020 RM 1 0.068 0.15
 *

2021 KK 13A-2
 2022 BA 0.188
 2023 PB 3.15
 2024 LS 0 90.0
 2025 UD 0.236
 *

2026 KK C13A-2
 2027 KM COMBINE 13A-2 AND RC13A-1
 2028 HC 2
 *

2029 KK RC13A-2
 2030 KM ROUTE C13A-2 TO CPIC-C
 2031 KM LINING = GRASS
 2032 RD 5200 0.015 0.03 0 TRAP 40 4
 *

2033 KK PIC-C
 2034 BA 0.243
 2035 PB 3.08
 2036 LS 0 90.4
 2037 UD 0.373
 *

2038 KK CPIC-C
 2039 KM COMBINE PIC-C AND RC13A-2
 2040 HC 2
 *

2041 KK RCPIC-C
 2042 KM ROUTE CPIC-C TO CPIC-A
 2043 KM LINING = GRASS
 2044 RD 2200 0.025 0.03 0 TRAP 40 4
 *

1

HEC-1 INPUT

PAGE 55

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2045 KK PIC-A
 2046 BA 0.359
 2047 PB 3.03
 2048 LS 0 91.1
 2049 UD 0.499
 *

2050 KK CPIC-A
 2051 KM COMBINE RCPIC-C AND PIC-A
 2052 HC 2
 *

2053 KK CCPIC-A
 2054 KM COMBINE CPIC-A AND RC13B-2
 2055 HC 2
 *

2056 KK RCPIC-A
 2057 KM ROUTE CCPIC-A TO C57B-1
 2058 KM FACILITY = ANGEL PARK - PECCOLE 2
 2059 KM FACILITY # = APP2 0000
 2060 KM LINING = GRASS
 2061 RD 4793 0.021 0.03 0 TRAP 10 2
 *

2062 KK 57B-1
 2063 BA 0.197
 2064 PB 2.92
 2065 LS 0 85.5
 2066 UD 0.277
 *

2067 KK C57B-1
 2068 KM COMBINE 57B-1 AND RCPIC-A
 2069 HC 2
 *

2070 KK CC57B-1
 2071 KM COMBINE C57B-1 AND RC57B-2
 2072 HC 2
 *

2073 KKRCC57B-1

2074 KM ROUTE CC57B-1 TO C57B-4
 2075 KM FACILITY = ANGEL PARK - SOUTH BRANCH
 2076 KM FACILITY # = APSO 0050
 2077 KM LINING = NATURAL WASH
 2078 RD 300 0.0184 0.04 0 TRAP 100 3
 *

ALLGOW3.OUT

1

HEC-1 INPUT

PAGE 56

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2079 KK 57B-4
 2080 BA 0.200
 2081 PB 2.91
 2082 LS 0 90.0
 2083 UD 0.233
 *

2084 KK C57B-4
 2085 KM COMBINE RCC57B-1 AND 57B-4
 2086 HC 2
 *

2087 KK PIC-B
 2088 BA 0.441
 2089 PB 2.98
 2090 LS 0 91.1
 2091 UD 0.471
 *

2092 KK RPIC-B
 2093 KM ROUTE PIC-B TO CC57B-4
 2094 KM FACILITY = ANGEL PARK - PECCOLE 1
 2095 KM FACILITY # = APP1 0000
 2096 KM LINING = RCP
 2097 RD 2982 0.024 0.013 0 CIRC 6
 *

2098 KK CC57B-4
 2099 KM COMBINE RPIC-B AND C57B-4
 2100 HC 2
 *

2101 KK RCC57B-4
 2102 KM ROUTE CC57B-4 TO ANGLPKIN
 2103 KM FACILITY = ANGEL PARK SOUTH
 2104 KM FACILITY # = APSO 0000, 0020
 2105 KM LINING = RCB
 2106 RD 2857 0.0162 0.015 0 TRAP 24 0
 *

2107 KK 38A
 2108 BA 0.353
 2109 PB 2.86
 2110 LS 0 91.6
 2111 UD 0.399
 *

2112 KK R38A
 2113 KM ROUTE 38A TO C38B
 2114 KM FACILITY = ANGEL PARK - DURANGO
 2115 KM FACILITY # = APDG 0000,0060
 2116 KM LINING = RCP
 2117 RD 4500 0.0096 0.015 0 CIRC 6
 *

1

HEC-1 INPUT

PAGE 57

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

2118 KK 38B
 2119 BA 0.440
 2120 PB 2.82
 2121 LS 0 92.9
 2122 UD 0.375
 *

2123 KK C38B
 2124 KM COMBINE 38B AND R38A
 2125 KM DUCHARME AND DURANGO
 2126 HC 2
 *

2127 KK 57BA
 2128 BA 0.317
 2129 PB 2.96
 2130 LS 0 78.2
 2131 UD 0.436
 *

2132 KK R57BA
 2133 KM ROUTE 57BA TO C3C
 2134 KM RAMPART BOULEVARD
 2135 RD 500 0.02 0.016 0 TRAP 0 50
 *

2136 KK 3C
 2137 BA 0.153
 2138 PB 2.90
 2139 LS 0 93.1
 2140 UD 0.246
 *

2141 KK C3C
 2142 KM COMBINE 3C AND R57BA
 2143 KM RAMPART AND REGENT LAS VEGAS
 2144 HC 2
 *

2145 KK RC3C
 2146 KM ROUTE C3C TO ANGLPKIN
 2147 KM LINING = UNLINED

END
 Reference

1837	.	.	.	SF2-C	.
1842	.	.	.	CSF2-C
1845	.	.	.	V	.
1852	.	.	.	RCSF2-C	.
1857	.	.	.	* SW11	.
1863	.	.	.	V	.
1868	.	.	.	RSW11	.
1871	SW17
1877
1882	.	.	.	CSW17
1885	.	.	.	V	.
1896	.	.	.	RCSW17	.
1901	SW18
1904	.	.	.	CSW18
1915	.	.	.	V	.
1920	.	.	.	RCSW18	.
1923	12A
1934	.	.	.	C12A
1939	.	.	.	V	.
1942	.	.	.	RC12A	.
1953	12B
1958	.	.	.	C12B
1961	.	.	.	V	.
1972	.	.	.	RC12B	.
1977	57B-3
1981	.	.	.	C57B-3
1986	.	.	.	V	.
1990	.	.	.	RC57B-3	.
1994	57B-2
1999	.	.	.	C57B-2
2003	.	.	.	V	.
2008	.	.	.	RC57B-2	.
2012	13B-1
2021	.	.	.	13B-1
2026	.	.	.	V	.
2029	.	.	.	RC13B-1	.
2033	13B-2
	.	.	.	C13B-2
	.	.	.	V	.
	.	.	.	RC13B-2	.
	19A
	.	.	.	V	.
	.	.	.	R19A	.
	13A-1
	.	.	.	C13A-1
	.	.	.	V	.
	.	.	.	RC13A-1	.
	13A-2
	.	.	.	C13A-2
	.	.	.	V	.
	.	.	.	RC13A-2	.
	PIC-C

Begin Reference

2038	ALLGOW3.OUT	CPIC-C.....	
		V	
2041		V	
	RPCIC-C		
2045			PIC-A

2050		CPIC-A.....	
			
2053	CCPIC-A.....		
		V	
2056		V	
	RCCPIC-A		
2062			57B-1

2067		C57B-1.....	
			
2070	CC57B-1.....		
		V	
2073		V	
	RCC57B-1		
2079			57B-4

2084		C57B-4.....	
			
2087		PIC-B	
		V	
2092		V	
	RPIC-B		
2098			
	CC57B-4.....		
		V	
2101		V	
	RCC57B-4		
2107			38A
			V
2112			V
		R38A	
2118			
			38B
2123			
		C38B.....	
2127			
			57BA
2132			V
			V
		R57BA	
2136			
			3C
2141			
		C3C.....	
2145			V
			V
		RC3C	
2150			
			AP
2155			
	ANGLPKIN.....		
2160		V	
		V	
	ANGLPKDB		
2181		V	
		V	
	ANGLPKOT		
2187			GD34AB

2192		CGD34AB.....	
		V	
2196		V	
	RCGD34AB		
2202			GD34AC

2207		CGD34AC.....	
			
2211	CCGD34AC.....		
		V	
2216		V	
	RCGD34AC		
2222			K-C
			
2233		----->	DCHEY

* End Reference

ALLGOW3.OUT

2 COMBINED AT	C8B-1	1.14	1	FLOW	1246.	1219.	1173.	1128.	1111.	1098.	1089.	1075.	1056.
ROUTED TO	RC8B-1	1.14	1	FLOW	1222.	1195.	1152.	1110.	1090.	1081.	1071.	1055.	1040.
HYDROGRAPH AT	8B-2	.42	1	FLOW	574.	564.	547.	530.	523.	518.	515.	510.	503.
2 COMBINED AT	C8B-2	1.56	1	FLOW	1795.	1758.	1697.	1632.	1610.	1593.	1578.	1562.	1533.
ROUTED TO	RC8B-2	1.56	1	FLOW	1774.	1736.	1681.	1618.	1593.	1582.	1565.	1547.	1522.
HYDROGRAPH AT	11A-2	.29	1	FLOW	433.	424.	409.	394.	388.	384.	381.	376.	370.
ROUTED TO	R11A-2	.29	1	FLOW	422.	413.	393.	378.	372.	368.	365.	360.	354.
HYDROGRAPH AT	8A	.31	1	FLOW	384.	375.	361.	347.	341.	337.	335.	330.	324.
2 COMBINED AT	C8A	.60	1	FLOW	805.	788.	755.	725.	713.	705.	700.	690.	679.
ROUTED TO	RC8A	.60	1	FLOW	751.	734.	704.	675.	664.	657.	651.	643.	632.
HYDROGRAPH AT	3B-2A	.24	1	FLOW	329.	322.	311.	300.	295.	292.	290.	286.	282.
2 COMBINED AT	C3B-2A	.84	1	FLOW	1040.	1018.	977.	939.	924.	914.	907.	895.	880.
2 COMBINED AT	CC3B-2A	2.40	1	FLOW	2803.	2743.	2644.	2540.	2505.	2476.	2453.	2428.	2384.
ROUTED TO	RCC3B-2A	2.40	1	FLOW	2769.	2725.	2623.	2515.	2493.	2463.	2431.	2413.	2367.
HYDROGRAPH AT	3B-2B	.27	1	FLOW	271.	265.	254.	244.	240.	237.	235.	231.	227.
2 COMBINED AT	C3B-2B	2.67	1	FLOW	3025.	2975.	2863.	2746.	2720.	2687.	2653.	2632.	2582.
2 COMBINED AT	CC3B-2B	14.42	1	FLOW	10916.	10721.	10381.	10032.	9913.	9809.	9738.	9637.	9486.
ROUTED TO	RCC3B-2B	14.42	1	FLOW	10822.	10623.	10284.	9931.	9814.	9701.	9639.	9527.	9379.
HYDROGRAPH AT	SF2-C	.39	1	FLOW	294.	287.	275.	263.	259.	255.	253.	249.	245.
2 COMBINED AT	CSF2-C	14.81	1	FLOW	11116.	10909.	10559.	10195.	10073.	9957.	9891.	9776.	9623.
ROUTED TO	RCSF2-C	14.81	1	FLOW	11007.	10789.	10429.	10061.	9937.	9831.	9758.	9650.	9507.
HYDROGRAPH AT	SW11	.59	1	FLOW	759.	743.	717.	691.	680.	673.	668.	660.	649.
ROUTED TO	RSW11	.59	1	FLOW	754.	738.	712.	686.	676.	668.	663.	655.	644.
HYDROGRAPH AT	SW17	.36	1	FLOW	479.	469.	452.	436.	429.	424.	421.	416.	409.
2 COMBINED AT	CSW17	.94	1	FLOW	1221.	1196.	1153.	1111.	1095.	1083.	1075.	1061.	1044.
ROUTED TO	RCSW17	.94	1	FLOW	1211.	1186.	1143.	1101.	1083.	1073.	1063.	1051.	1035.
HYDROGRAPH AT	SW18	.41	1	FLOW	519.	507.	489.	470.	463.	457.	454.	448.	440.
2 COMBINED AT	CSW18	1.35	1	FLOW	1718.	1682.	1622.	1562.	1537.	1521.	1508.	1490.	1467.

Begin
Reference

ALLGOW3.OUT

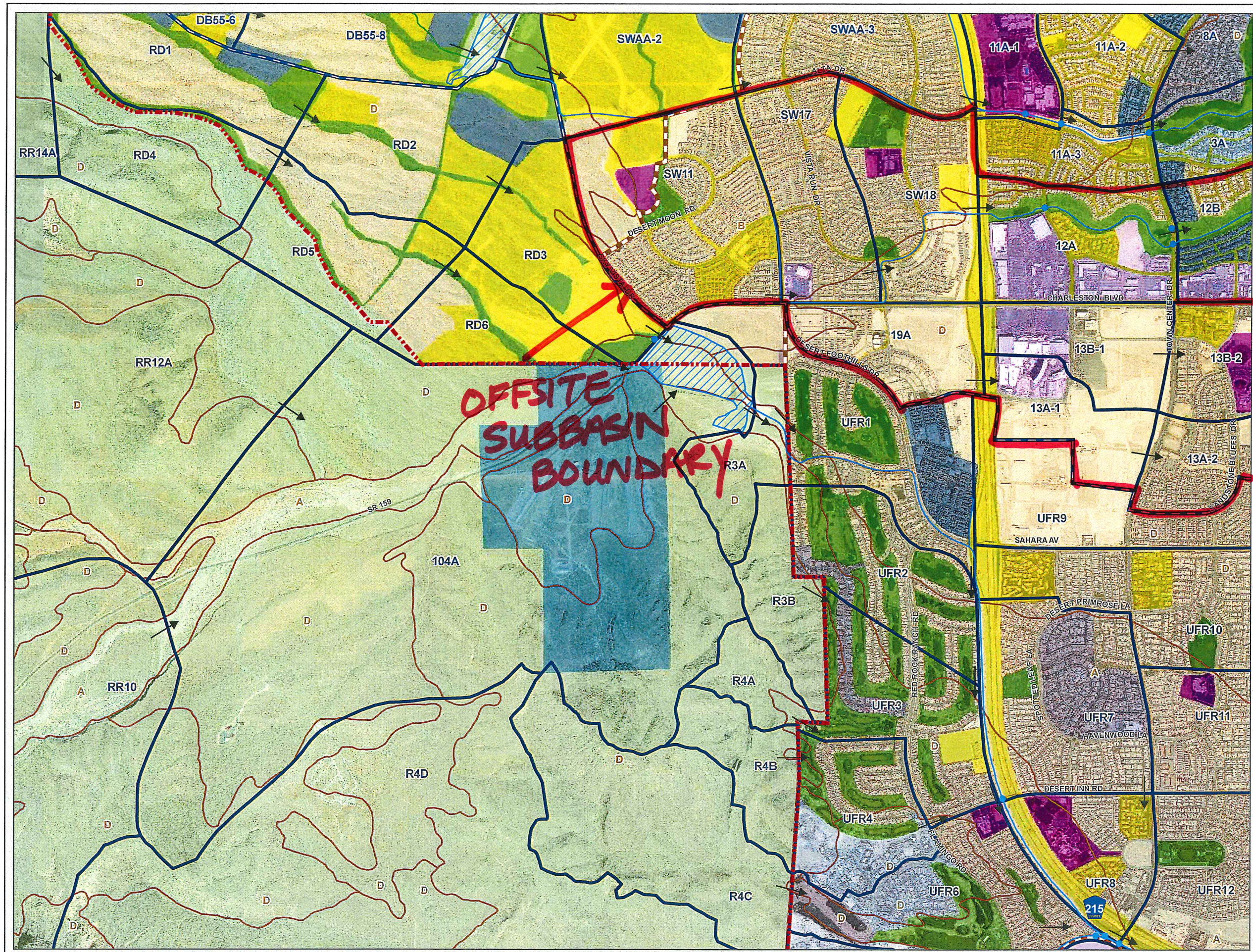
ROUTED TO													
+	RCSW18	1.35	1	FLOW TIME	1610. 3.92	1576. 3.92	1520. 3.92	1464. 3.92	1441. 3.92	1426. 3.92	1414. 3.92	1397. 3.92	1375. 3.92
HYDROGRAPH AT													
+	12A	.39	1	FLOW TIME	576. 3.67	565. 3.67	547. 3.67	529. 3.67	521. 3.67	516. 3.67	513. 3.67	507. 3.67	500. 3.67
2 COMBINED AT													
+	C12A	1.74	1	FLOW TIME	2046. 3.83	2003. 3.83	1932. 3.83	1861. 3.83	1832. 3.83	1813. 3.83	1798. 3.83	1776. 3.83	1748. 3.83
ROUTED TO													
+	RC12A	1.74	1	FLOW TIME	2025. 3.92	1983. 3.92	1913. 3.92	1843. 3.92	1815. 3.92	1796. 3.92	1782. 3.92	1760. 3.92	1732. 3.92
HYDROGRAPH AT													
+	12B	.26	1	FLOW TIME	387. 3.67	380. 3.67	367. 3.67	355. 3.67	350. 3.67	347. 3.67	344. 3.67	340. 3.67	335. 3.67
2 COMBINED AT													
+	C12B	2.00	1	FLOW TIME	2259. 3.83	2212. 3.83	2134. 3.83	2056. 3.83	2024. 3.83	2002. 3.83	1987. 3.83	1962. 3.83	1931. 3.83
ROUTED TO													
+	RC12B	2.00	1	FLOW TIME	2194. 4.00	2148. 4.00	2073. 4.00	1998. 4.00	1967. 4.00	1946. 4.00	1931. 4.00	1907. 4.00	1877. 4.00
HYDROGRAPH AT													
+	57B-3	.31	1	FLOW TIME	267. 3.75	260. 3.75	248. 3.75	237. 3.75	233. 3.75	230. 3.75	227. 3.75	224. 3.75	219. 3.75
2 COMBINED AT													
+	C57B-3	2.31	1	FLOW TIME	2394. 4.00	2344. 4.00	2261. 4.00	2177. 4.00	2144. 4.00	2120. 4.00	2104. 4.00	2077. 4.00	2044. 4.00
ROUTED TO													
+	RC57B-3	2.31	1	FLOW TIME	2375. 4.00	2325. 4.00	2242. 4.00	2158. 4.00	2125. 4.00	2101. 4.00	2085. 4.00	2058. 4.00	2025. 4.00
HYDROGRAPH AT													
+	57B-2	.36	1	FLOW TIME	338. 3.75	329. 3.75	316. 3.75	302. 3.75	297. 3.75	293. 3.75	291. 3.75	286. 3.75	281. 3.75
2 COMBINED AT													
+	C57B-2	2.67	1	FLOW TIME	2626. 4.00	2570. 4.00	2477. 4.00	2384. 4.00	2347. 4.00	2321. 4.00	2302. 4.00	2273. 4.00	2236. 4.00
ROUTED TO													
+	RC57B-2	2.67	1	FLOW TIME	2609. 4.00	2553. 4.00	2460. 4.00	2367. 4.00	2330. 4.00	2304. 4.00	2285. 4.00	2256. 4.00	2219. 4.00
HYDROGRAPH AT													
+	13B-1	.25	1	FLOW TIME	354. 3.67	347. 3.67	336. 3.67	325. 3.67	321. 3.67	318. 3.67	315. 3.67	312. 3.67	307. 3.67
ROUTED TO													
+	RC13B-1	.25	1	FLOW TIME	354. 3.75	347. 3.75	336. 3.75	324. 3.75	320. 3.75	317. 3.75	314. 3.83	311. 3.83	307. 3.83
HYDROGRAPH AT													
+	13B-2	.22	1	FLOW TIME	310. 3.67	304. 3.67	294. 3.67	283. 3.67	279. 3.67	277. 3.67	274. 3.67	271. 3.67	267. 3.67
2 COMBINED AT													
+	C13B-2	.47	1	FLOW TIME	634. 3.75	622. 3.75	602. 3.75	581. 3.75	573. 3.75	567. 3.75	563. 3.75	557. 3.75	549. 3.75
ROUTED TO													
+	RC13B-2	.47	1	FLOW TIME	641. 3.83	628. 3.83	607. 3.83	586. 3.83	578. 3.83	572. 3.83	568. 3.83	561. 3.83	553. 3.83
HYDROGRAPH AT													
+	19A	.25	1	FLOW TIME	318. 3.75	312. 3.75	301. 3.75	291. 3.75	287. 3.75	284. 3.75	282. 3.75	278. 3.75	274. 3.75
ROUTED TO													
+	R19A	.25	1	FLOW TIME	319. 3.92	313. 3.92	302. 3.92	292. 3.92	288. 3.92	285. 3.92	283. 3.92	280. 3.92	276. 3.92
HYDROGRAPH AT													
+	13A-1	.22	1	FLOW TIME	308. 3.75	303. 3.75	293. 3.75	283. 3.75	279. 3.75	277. 3.75	275. 3.75	272. 3.75	268. 3.75
2 COMBINED AT													
+	C13A-1	.48	1	FLOW TIME	595. 3.83	583. 3.83	564. 3.83	545. 3.83	537. 3.83	532. 3.83	528. 3.83	522. 3.83	514. 3.83
ROUTED TO													
+	RC13A-1	.48	1	FLOW TIME	581. 3.92	569. 3.92	551. 3.92	532. 3.92	524. 3.92	519. 3.92	515. 3.92	509. 3.92	502. 3.92
HYDROGRAPH AT													
+	13A-2	.19	1	FLOW TIME	272. 3.67	267. 3.67	258. 3.67	249. 3.67	246. 3.67	243. 3.67	241. 3.67	238. 3.67	235. 3.67
2 COMBINED AT													
+	C13A-2	.66	1	FLOW TIME	782. 3.83	766. 3.83	740. 3.83	715. 3.83	704. 3.83	697. 3.83	692. 3.83	684. 3.83	673. 3.83
ROUTED TO													
+	RC13A-2	.66	1	FLOW TIME	781. 3.92	765. 3.92	738. 3.92	712. 3.92	702. 3.92	694. 3.92	689. 3.92	681. 3.92	670. 3.92
HYDROGRAPH AT													
+	PIC-C	.24	1	FLOW TIME	280. 3.83	274. 3.83	265. 3.83	256. 3.83	252. 3.83	250. 3.83	248. 3.83	245. 3.83	241. 3.83
2 COMBINED AT													
+	CPIC-C	.91	1	FLOW TIME	1041. 3.92	1020. 3.92	985. 3.92	951. 3.92	937. 3.92	927. 3.92	920. 3.92	909. 3.92	895. 3.92

ALLGOW3.OUT

ROUTED TO													
+	RCPIC-C	.91	1	FLOW TIME	1030. 3.92	1009. 3.92	975. 3.92	940. 3.92	922. 3.92	915. 3.92	908. 3.92	896. 3.92	881. 3.92
HYDROGRAPH AT													
+	PIC-A	.36	1	FLOW TIME	356. 3.92	349. 3.92	338. 3.92	326. 3.92	322. 3.92	318. 3.92	316. 3.92	312. 3.92	308. 3.92
2 COMBINED AT													
+	CPIC-A	1.27	1	FLOW TIME	1386. 3.92	1359. 3.92	1313. 3.92	1266. 3.92	1243. 3.92	1233. 3.92	1224. 3.92	1208. 3.92	1188. 3.92
2 COMBINED AT													
+	CCPIC-A	1.73	1	FLOW TIME	1997. 3.92	1959. 3.92	1895. 3.92	1830. 3.92	1800. 3.92	1785. 3.92	1772. 3.92	1750. 3.92	1723. 3.92
ROUTED TO													
+	RCCPIC-A	1.73	1	FLOW TIME	1974. 4.00	1921. 4.00	1874. 4.00	1792. 4.00	1776. 4.00	1769. 4.00	1758. 4.00	1721. 4.00	1690. 4.00
HYDROGRAPH AT													
+	57B-1	.20	1	FLOW TIME	199. 3.67	194. 3.67	186. 3.67	179. 3.67	176. 3.75	174. 3.75	172. 3.75	170. 3.75	167. 3.75
2 COMBINED AT													
+	C57B-1	1.93	1	FLOW TIME	2106. 3.92	2049. 3.92	2004. 3.92	1912. 3.92	1900. 3.92	1876. 3.92	1862. 4.00	1824. 4.00	1791. 4.00
2 COMBINED AT													
+	CC57B-1	4.60	1	FLOW TIME	4702. 4.00	4591. 4.00	4447. 4.00	4268. 4.00	4213. 4.00	4179. 4.00	4148. 4.00	4080. 4.00	4011. 4.00
ROUTED TO													
+	RCC57B-1	4.60	1	FLOW TIME	4694. 4.00	4583. 4.00	4439. 4.00	4260. 4.00	4205. 4.00	4170. 4.00	4139. 4.00	4071. 4.00	4002. 4.00
HYDROGRAPH AT													
+	57B-4	.20	1	FLOW TIME	262. 3.67	257. 3.67	248. 3.67	239. 3.67	236. 3.67	233. 3.67	231. 3.67	229. 3.67	225. 3.67
2 COMBINED AT													
+	C57B-4	4.80	1	FLOW TIME	4813. 4.00	4700. 4.00	4553. 4.00	4371. 4.00	4314. 4.00	4278. 4.00	4246. 4.00	4177. 4.00	4107. 4.00
HYDROGRAPH AT													
+	PIC-B	.44	1	FLOW TIME	442. 3.92	433. 3.92	419. 3.92	405. 3.92	399. 3.92	395. 3.92	392. 3.92	388. 3.92	382. 3.92
ROUTED TO													
+	RPIC-B	.44	1	FLOW TIME	439. 3.92	431. 3.92	416. 3.92	402. 3.92	396. 3.92	392. 3.92	390. 3.92	385. 3.92	379. 3.92
2 COMBINED AT													
+	CC57B-4	5.24	1	FLOW TIME	5243. 4.00	5122. 4.00	4961. 4.00	4765. 4.00	4702. 4.00	4663. 4.00	4628. 4.00	4554. 4.00	4479. 4.00
ROUTED TO													
+	RCC57B-4	5.24	1	FLOW TIME	5225. 4.00	5104. 4.00	4944. 4.00	4747. 4.00	4686. 4.00	4644. 4.00	4606. 4.00	4534. 4.00	4460. 4.00
HYDROGRAPH AT													
+	38A	.35	1	FLOW TIME	374. 3.83	367. 3.83	355. 3.83	343. 3.83	338. 3.83	335. 3.83	333. 3.83	329. 3.83	324. 3.83
ROUTED TO													
+	R38A	.35	1	FLOW TIME	368. 3.92	364. 3.92	350. 3.92	337. 3.92	333. 3.92	331. 3.92	330. 3.92	327. 3.92	320. 3.92
HYDROGRAPH AT													
+	38B	.44	1	FLOW TIME	492. 3.83	483. 3.83	467. 3.83	452. 3.83	446. 3.83	442. 3.83	439. 3.83	434. 3.83	428. 3.83
2 COMBINED AT													
+	C38B	.79	1	FLOW TIME	856. 3.83	842. 3.83	810. 3.83	784. 3.83	775. 3.83	769. 3.83	764. 3.83	753. 3.83	740. 3.83
HYDROGRAPH AT													
+	57BA	.32	1	FLOW TIME	186. 3.92	180. 3.92	171. 3.92	163. 3.92	159. 3.92	157. 3.92	155. 3.92	152. 3.92	149. 3.92
ROUTED TO													
+	R57BA	.32	1	FLOW TIME	185. 3.92	179. 3.92	171. 3.92	162. 3.92	158. 3.92	156. 3.92	154. 3.92	151. 3.92	148. 3.92
HYDROGRAPH AT													
+	3C	.15	1	FLOW TIME	218. 3.67	214. 3.67	207. 3.67	201. 3.67	198. 3.67	196. 3.67	195. 3.67	193. 3.67	190. 3.67
2 COMBINED AT													
+	C3C	.47	1	FLOW TIME	358. 3.75	350. 3.75	335. 3.75	322. 3.75	316. 3.75	312. 3.75	309. 3.75	305. 3.75	299. 3.75
ROUTED TO													
+	RC3C	.47	1	FLOW TIME	358. 3.83	350. 3.83	336. 3.83	322. 3.83	316. 3.83	312. 3.83	310. 3.83	305. 3.83	300. 3.83
HYDROGRAPH AT													
+	AP	.67	1	FLOW TIME	450. 3.83	438. 3.83	418. 3.83	398. 3.83	390. 3.83	385. 3.83	381. 3.83	375. 3.83	367. 3.83
5 COMBINED AT													
+	ANGLPKIN	21.99	1	FLOW TIME	17682. 3.92	17317. 3.92	16736. 3.92	16120. 4.00	15911. 4.00	15749. 4.00	15645. 4.00	15449. 4.00	15212. 4.00
ROUTED TO													
+	ANGLPKDB	21.99	1	FLOW TIME	5746. 5.42	5406. 5.42	4785. 5.58	4149. 5.67	3879. 5.75	3713. 5.75	3566. 5.75	3372. 5.83	3116. 5.92
** PEAK STAGES IN FEET **													
1	STAGE				2620.18	2620.13	2620.04	2619.94	2619.88	2619.85	2619.82	2619.79	2619.74
	TIME				5.42	5.42	5.58	5.67	5.75	5.75	5.75	5.83	5.92

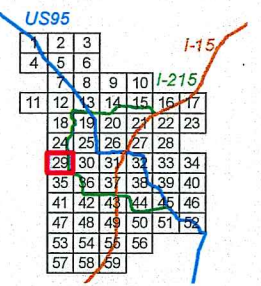
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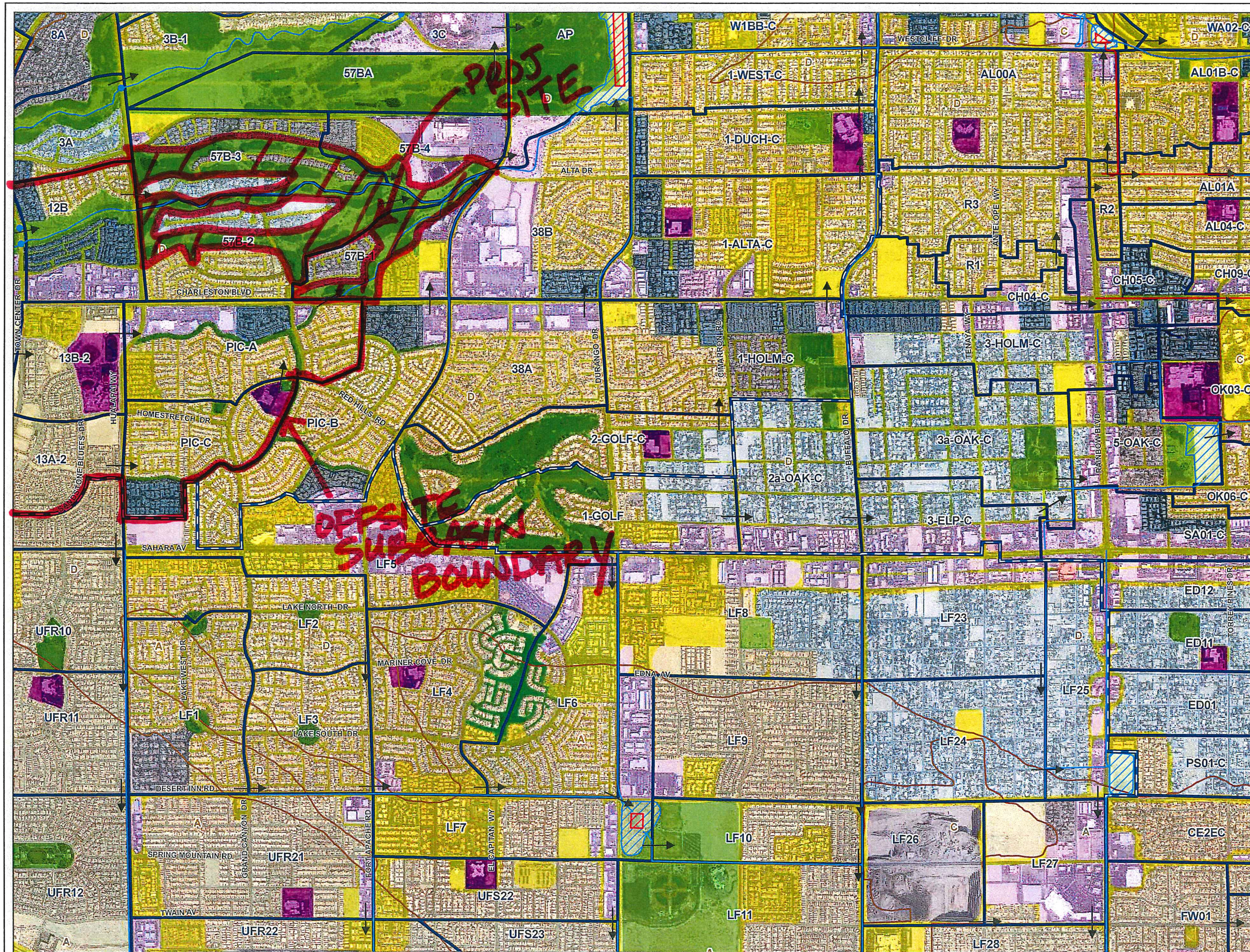
Flow to Rampart + Alta Intersection



2008
LAS VEGAS VALLEY
FLOOD CONTROL
MASTER PLAN UPDATE
FIGURE H- 29
HYDROLOGIC SUMMARY

- LEGEND**
- Ultimate Development Boundary
 - Watershed Boundary
 - Subbasin Boundary
 - Drought Ordinance Boundary
 - Flow Arrows
- Flood Control Facilities**
- Existing Facilities
 - Category A Proposed Facilities
 - Category B Proposed Facilities
 - Category A Remove & Replace/Parallel Facilities
 - Category B Remove & Replace/Parallel Facilities
- Type Hydrologic Soil Groups**
- A Low Runoff Potential
 - B Moderately Low Runoff Potential
 - C Moderately High Runoff Potential
 - D High Runoff Potential/Rock Outcrops
- Typical Land Use**
- 1 Undeveloped Land, Open Desert
 - 2 Parks, Golf Courses
 - 3 Rural
 - 4 / 14* Low Density Residential
 - 5 / 15* Medium Density Residential
 - 6 / 16* High Density Residential
 - 7 / 17* Public Facility, Residential
 - 8 / 18* Very High Density Residential
 - 9 / 19* Commercial, Retail, Casino, High Rise Condominiums
 - 10 / 20* Light Industrial
 - 11 / 21* Heavy Industrial
 - 12 / 22* Schools
 - 13 Lakes
- * Drought Ordinance Applied
- 0 500 1,000 2,000 3,000 Feet
Scale: 1 inch = 2,000 feet
Refer to Figure G-2 for Aerial Source(s)





REGIONAL FLOOD CONTROL DISTRICT

2008
LAS VEGAS VALLEY
FLOOD CONTROL
MASTER PLAN UPDATE
FIGURE H-30
HYDROLOGIC SUMMARY

LEGEND

Ultimate Development Boundary
 Watershed Boundary
 Subbasin Boundary
 Drought Ordinance Boundary
 Flow Arrows

Flood Control Facilities

Existing Facilities
 Category A Proposed Facilities
 Category B Proposed Facilities
 Category A Remove & Replace/Parallel Facilities
 Category B Remove & Replace/Parallel Facilities

Hydrologic Soil Groups

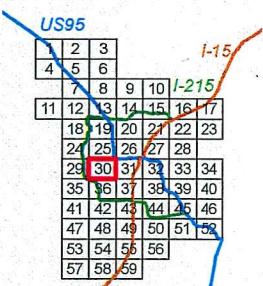
A Low Runoff Potential
B Moderately Low Runoff Potential
C Moderately High Runoff Potential
D High Runoff Potential/Rock Outcrops

Typical Land Use

1 Undeveloped Land, Open Desert
2 Parks, Golf Courses
3 Rural
4 / 14* Low Density Residential
5 / 15* Medium Density Residential
6 / 16* High Density Residential
7 / 17* Public Facility, Residential
8 / 18* Very High Density Residential
9 / 19* Commercial, Retail, Casino, High Rise Condominiums
10 / 20* Light Industrial
11 / 21* Heavy Industrial
12 / 22* Schools
13 Lakes

* Drought Ordinance Applied

0 500 1,000 2,000 3,000 Feet
Scale: 1 inch = 2,000 feet
Refer to Figure G-2 for Aerial Source(s)





Federal Emergency Management Agency

Washington, D.C. 20472

OCT 19 2006

CERTIFIED MAIL
RETURN RECEIPT REQUESTED

The Honorable Oscar B. Goodman
Mayor, City of Las Vegas
City Hall, 10th Floor
400 Stewart Avenue
Las Vegas, NV 89101

IN REPLY REFER TO:

Case No.: 06-09-BF86P

Follows Conditional

Case No.: 05-09-0420R

Community Name: City of Las Vegas, NV

Community No.: 325276

Effective Date of

This Revision:

OCT 19 2006

Dear Mayor Goodman:

The Flood Insurance Rate Map for your community has been revised by this Letter of Map Revision (LOMR). Please use the enclosed annotated map panel(s) revised by this LOMR for floodplain management purposes and for all flood insurance policies and renewals issued in your community.

Additional documents are enclosed which provide information regarding this LOMR. Please see the List of Enclosures below to determine which documents are included. Other attachments specific to this request may be included as referenced in the Determination Document. If you have any questions regarding floodplain management regulations for your community or the National Flood Insurance Program (NFIP) in general, please contact the Consultation Coordination Officer for your community. If you have any technical questions regarding this LOMR, please contact the Director, Federal Insurance and Mitigation Division of the Department of Homeland Security's Federal Emergency Management Agency (FEMA) in Oakland, California, at (510) 627-7175, or the FEMA Map Assistance Center toll free at 1-877-336-2627 (1-877-FEMA MAP). Additional information about the NFIP is available on our website at <http://www.fema.gov/nfip>.

Sincerely,

Kevin C. Long, CFM, Project Engineer
Engineering Management Section
Mitigation Division

For: William R. Blanton Jr., CFM, Chief
Engineering Management Section
Mitigation Division

List of Enclosures:

Letter of Map Revision Determination Document
Annotated Flood Insurance Rate Map

cc: Mr. Randy Fultz, P.E., CFM
Assistant City Engineer
City of Las Vegas

Mr. Kevin Eubanks, P.E., CFM
Assistant General Manager
Clark County Regional Flood Control District

Mr. Michael Ludwig, P.E., Project Manager
G.C. Wallace, Inc.



Federal Emergency Management Agency

Washington, D.C. 20472

LETTER OF MAP REVISION DETERMINATION DOCUMENT

COMMUNITY AND REVISION INFORMATION		PROJECT DESCRIPTION	BASIS OF REQUEST
COMMUNITY	City of Las Vegas Clark County Nevada	STORM DRAIN	HYDRAULIC ANALYSIS HYDROLOGIC ANALYSIS
	COMMUNITY NO.: 325276		
IDENTIFIER	Village at Queensridge	APPROXIMATE LATITUDE & LONGITUDE: 36.168, -115.286 SOURCE: USGS QUADRANGLE DATUM: NAD 83	
ANNOTATED MAPPING ENCLOSURES		ANNOTATED STUDY ENCLOSURES	
TYPE: FIRM* NO.: 32003C2145 E DATE: September 27, 2002		NO REVISION TO THE FLOOD INSURANCE STUDY REPORT	

Enclosures reflect changes to flooding sources affected by this revision.

* FIRM - Flood Insurance Rate Map; ** FBFM - Flood Boundary and Floodway Map; *** FHBM - Flood Hazard Boundary Map

FLOODING SOURCE(S) & REVISED REACH(ES)

Unnamed Wash - from approximately 2,200 feet downstream to approximately 100 feet downstream of Rampart Boulevard

SUMMARY OF REVISIONS

Flooding Source	Effective Flooding	Revised Flooding	Increases	Decreases
Unnamed Wash	Zone A	Contained	NONE	YES

* BFEs - Base Flood Elevations

DETERMINATION

This document provides the determination from the Department of Homeland Security's Federal Emergency Management Agency (FEMA) regarding a request for a Letter of Map Revision (LOMR) for the area described above. Using the information submitted, we have determined that a revision to the flood hazards depicted in the Flood Insurance Study (FIS) report and/or National Flood Insurance Program (NFIP) map is warranted. This document revises the effective NFIP map, as indicated in the attached documentation. Please use the enclosed annotated map panels revised by this LOMR for floodplain management purposes and for all flood insurance policies and renewals in your community.

This determination is based on the flood data presently available. The enclosed documents provide additional information regarding this determination. If you have any questions about this document, please contact the FEMA Map Assistance Center toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMR Depot, 3601 Eisenhower Avenue, Alexandria, VA 22304. Additional Information about the NFIP is available on our website at <http://www.fema.gov/nfip>.

Kevin C. Long

Kevin C. Long, CFM, Project Engineer
Engineering Management Section
Mitigation Division

109770 10.3.1.0609BF86 102-D



Federal Emergency Management Agency

Washington, D.C. 20472

LETTER OF MAP REVISION DETERMINATION DOCUMENT (CONTINUED)

COMMUNITY INFORMATION

APPLICABLE NFIP REGULATIONS/COMMUNITY OBLIGATION

We have made this determination pursuant to Section 206 of the Flood Disaster Protection Act of 1973 (P.L. 93-234) and in accordance with the National Flood Insurance Act of 1968, as amended (Title XIII of the Housing and Urban Development Act of 1968, P.L. 90-448), 42 U.S.C. 4001-4128, and 44 CFR Part 65. Pursuant to Section 1361 of the National Flood Insurance Act of 1968, as amended, communities participating in the NFIP are required to adopt and enforce floodplain management regulations that meet or exceed NFIP criteria. These criteria, including adoption of the FIS report and FIRM, and the modifications made by this LOMR, are the minimum requirements for continued NFIP participation and do not supersede more stringent State/Commonwealth or local requirements to which the regulations apply.

NFIP regulations Subparagraph 60.3(b)(7) requires communities to ensure that the flood-carrying capacity within the altered or relocated portion of any watercourse is maintained. This provision is incorporated into your community's existing floodplain management ordinances; therefore, responsibility for maintenance of the altered or relocated watercourse, including any related appurtenances such as bridges, culverts, and other drainage structures, rests with your community. We may request that your community submit a description and schedule of maintenance activities necessary to ensure this requirement.

COMMUNITY REMINDERS

We based this determination on the 1-percent-annual-chance discharges computed in the submitted hydrologic model. Future development of projects upstream could cause increased discharges, which could cause increased flood hazards. A comprehensive restudy of your community's flood hazards would consider the cumulative effects of development on discharges and could, therefore, indicate that greater flood hazards exist in this area.

Your community must regulate all proposed floodplain development and ensure that permits required by Federal and/or State/Commonwealth law have been obtained. State/Commonwealth or community officials, based on knowledge of local conditions and in the interest of safety, may set higher standards for construction or may limit development in floodplain areas. If your State/Commonwealth or community has adopted more restrictive or comprehensive floodplain management criteria, those criteria take precedence over the minimum NFIP requirements.

We will not print and distribute this LOMR to primary users, such as local insurance agents or mortgage lenders; instead, the community will serve as a repository for the new data. We encourage you to disseminate the information in this LOMR by preparing a news release for publication in your community's newspaper that describes the revision and explains how your community will provide the data and help interpret the NFIP maps. In that way, interested persons, such as property owners, insurance agents, and mortgage lenders, can benefit from the information.

This determination is based on the flood data presently available. The enclosed documents provide additional information regarding this determination. If you have any questions about this document, please contact the FEMA Map Assistance Center toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMR Depot, 3601 Eisenhower Avenue, Alexandria, VA 22304. Additional Information about the NFIP is available on our website at <http://www.fema.gov/nfip>.

A handwritten signature in cursive script that reads "Kevin C. Long".

Kevin C. Long, CFM, Project Engineer
Engineering Management Section
Mitigation Division



Federal Emergency Management Agency

Washington, D.C. 20472

LETTER OF MAP REVISION DETERMINATION DOCUMENT (CONTINUED)

We have designated a Consultation Coordination Officer (CCO) to assist your community. The CCO will be the primary liaison between your community and FEMA. For information regarding your CCO, please contact:

Ms. Sally M. Ziolkowski
Director, Federal Insurance and Mitigation Division
Federal Emergency Management Agency, Region IX
1111 Broadway Street, Suite 1200
Oakland, CA 94607-4052
(510) 627-7175

STATUS OF THE COMMUNITY NFIP MAPS

We will not physically revise and republish the FIRM for your community to reflect the modifications made by this LOMR at this time. When changes to the previously cited FIRM panel(s) warrant physical revision and republication in the future, we will incorporate the modifications made by this LOMR at that time.

This determination is based on the flood data presently available. The enclosed documents provide additional information regarding this determination. If you have any questions about this document, please contact the FEMA Map Assistance Center toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMR Depot, 3601 Eisenhower Avenue, Alexandria, VA 22304. Additional Information about the NFIP is available on our website at <http://www.fema.gov/nfip>.

A handwritten signature in cursive script that reads "Kevin C. Long".

Kevin C. Long, CFM, Project Engineer
Engineering Management Section
Mitigation Division



Federal Emergency Management Agency

Washington, D.C. 20472

LETTER OF MAP REVISION DETERMINATION DOCUMENT (CONTINUED)

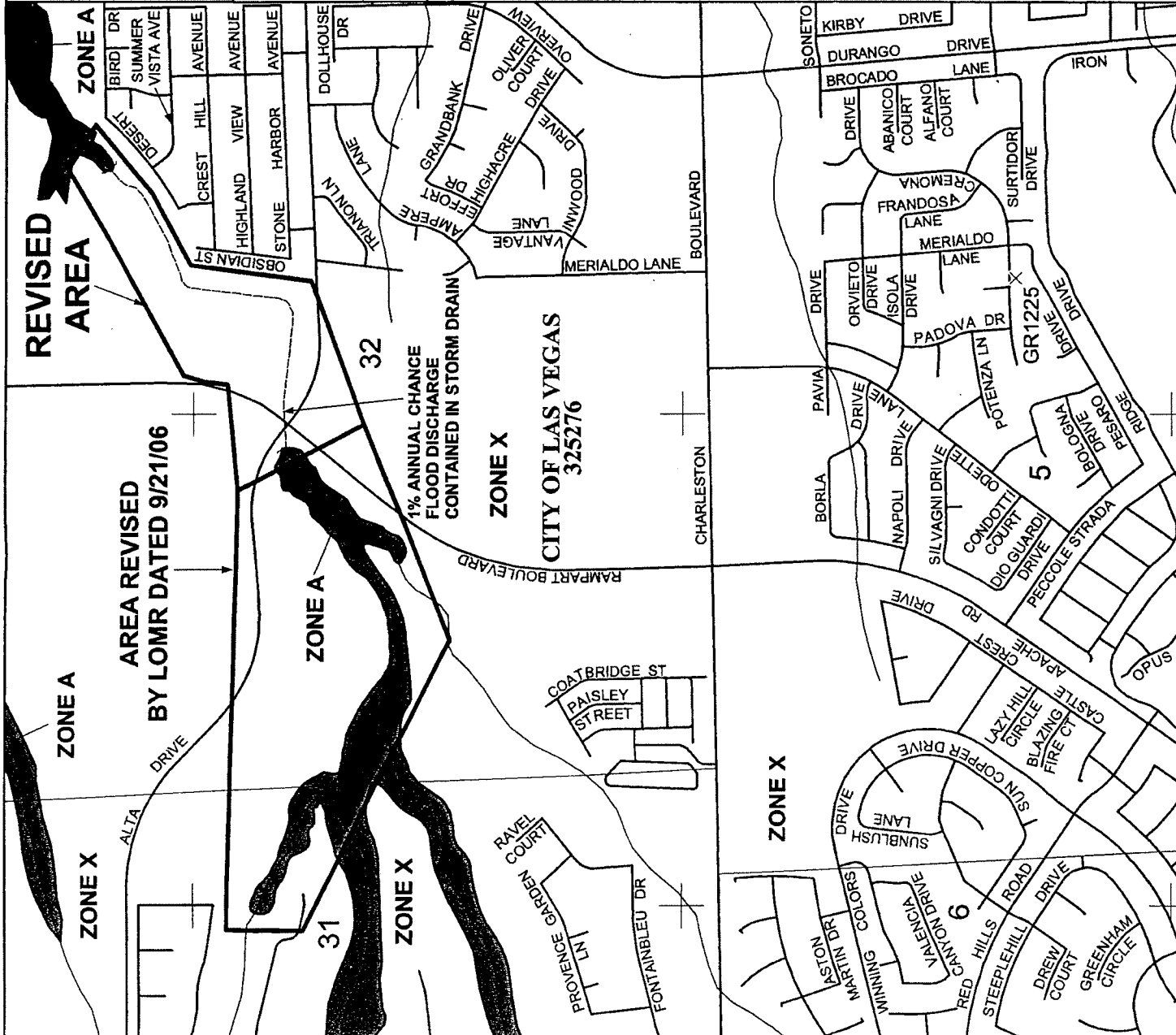
PUBLIC NOTIFICATION OF REVISION

This revision is effective as of the date of this letter. Any requests to review or alter this determination should be made within 30 days and must be based on scientific or technical data.

This determination is based on the flood data presently available. The enclosed documents provide additional information regarding this determination. If you have any questions about this document, please contact the FEMA Map Assistance Center toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMR Depot, 3601 Eisenhower Avenue, Alexandria, VA 22304. Additional Information about the NFIP is available on our website at <http://www.fema.gov/nfip>.

A handwritten signature in cursive script that reads "Kevin C. Long".

Kevin C. Long, CFM, Project Engineer
Engineering Management Section
Mitigation Division

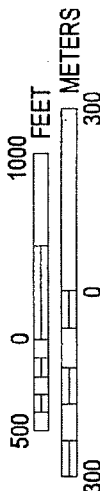


Legend

- 1% annual chance (100-Year) Floodplain
- 1% annual chance (100-Year) Floodway
- 0.2% annual chance (500-Year) Floodplain



MAP SCALE 1" = 1000'



PANEL 2145 E

FIRM

FLOOD INSURANCE RATE MAP

CLARK COUNTY,
NEVADA
AND INCORPORATED AREAS

PANEL 2145 OF 4090

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:
FIRM PANEL SUFFIX
E
UNINCORPORATED AREAS

REFLECT LOMR

EFFECTIVE OCT 19 2006

Notice to User: The Map Number shown below should be used when placing map orders; the Community Number shown above should be used on insurance applications for the subject community.



MAP NUMBER
32003C2145 E

MAP REVISED
SEPTEMBER 27, 2002

Federal Emergency Management Agency



Federal Emergency Management Agency

Washington, D.C. 20472

SEP 21 2006

CERTIFIED MAIL
RETURN RECEIPT REQUESTED

The Honorable Oscar Goodman
Mayor, City of Las Vegas
400 Stewart Avenue
Las Vegas, NV 89101

IN REPLY REFER TO:

Case No.: 06-09-B483P
Community Name: City of Las Vegas, NV
Community No.: 325276
Effective Date of
This Revision: **SEP 21 2006**

Dear Mayor Goodman:

The Flood Insurance Rate Map for your community has been revised by this Letter of Map Revision (LOMR). Please use the enclosed annotated map panel(s) revised by this LOMR for floodplain management purposes and for all flood insurance policies and renewals issued in your community.

Additional documents are enclosed which provide information regarding this LOMR. Please see the List of Enclosures below to determine which documents are included. Other attachments specific to this request may be included as referenced in the Determination Document. If you have any questions regarding floodplain management regulations for your community or the National Flood Insurance Program (NFIP) in general, please contact the Consultation Coordination Officer for your community. If you have any technical questions regarding this LOMR, please contact the Director, Federal Insurance and Mitigation Division of the Department of Homeland Security's Federal Emergency Management Agency (FEMA) in Oakland, California, at (510) 627-7175, or the FEMA Map Assistance Center, toll free, at 1-877-336-2627 (1-877-FEMA MAP). Additional information about the NFIP is available on our website at <http://www.fema.gov/nfip>.

Sincerely,

Kevin C. Long, CFM, Project Engineer
Engineering Management Section
Mitigation Division

For: William R. Blanton Jr., CFM, Chief
Engineering Management Section
Mitigation Division

List of Enclosures:

Letter of Map Revision Determination Document
Annotated Flood Insurance Rate Map

cc: Mr. Randy Fultz, P.E.
Assistant City Engineer
City of Las Vegas

Mr. Kevin Eubanks, P.E., CFM
Assistant General Manager
Clark County Regional Flood Control
District

Mr. Michael J. Ludwig, P.E.
Project Manager
Flood Control District
G.C. Wallace, Inc.



Federal Emergency Management Agency

Washington, D.C. 20472

LETTER OF MAP REVISION DETERMINATION DOCUMENT

COMMUNITY AND REVISION INFORMATION		PROJECT DESCRIPTION	BASIS OF REQUEST
COMMUNITY	City of Las Vegas Clark County Nevada	CULVERT	HYDRAULIC ANALYSIS HYDROLOGIC ANALYSIS NEW TOPOGRAPHIC DATA
	COMMUNITY NO.: 325276		
IDENTIFIER	Queensridge Place	APPROXIMATE LATITUDE & LONGITUDE: 36.165, -115.293 SOURCE: USGS QUADRANGLE DATUM: NAD 83	
ANNOTATED MAPPING ENCLOSURES		ANNOTATED STUDY ENCLOSURES	
TYPE: FIRM* NO.: 32003C2145E DATE: September 27, 2002		NO REVISION TO THE FLOOD INSURANCE STUDY REPORT	

Enclosures reflect changes to flooding sources affected by this revision.

* FIRM - Flood Insurance Rate Map; ** FBFM - Flood Boundary and Floodway Map; *** FHBM - Flood Hazard Boundary Map

FLOODING SOURCE(S) & REVISED REACH(ES)

Unnamed Wash - from approximately 3,600 feet upstream to approximately 100 feet downstream of South Rampart Boulevard

SUMMARY OF REVISIONS

Flooding Source	Effective Flooding	Revised Flooding	Increases	Decreases
Unnamed Wash	Zone A	Zone A	YES	YES
	Zone A	Contained	NONE	YES

* BFEs - Base Flood Elevations

DETERMINATION

This document provides the determination from the Department of Homeland Security's Federal Emergency Management Agency (FEMA) regarding a request for a Letter of Map Revision (LOMR) for the area described above. Using the information submitted, we have determined that a revision to the flood hazards depicted in the Flood Insurance Study (FIS) report and/or National Flood Insurance Program (NFIP) map is warranted. This document revises the effective NFIP map, as indicated in the attached documentation. Please use the enclosed annotated map panels revised by this LOMR for floodplain management purposes and for all flood insurance policies and renewals in your community.

This determination is based on the flood data presently available. The enclosed documents provide additional information regarding this determination. If you have any questions about this document, please contact the FEMA Map Assistance Center toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMR Depot, 3601 Eisenhower Avenue, Alexandria, VA 22304. Additional Information about the NFIP is available on our website at <http://www.fema.gov/nfip>.

Kevin C. Long

Kevin C. Long, CFM, Project Engineer
Engineering Management Section
Mitigation Division

106979 10.3.1.0609B483 102-I-C



Federal Emergency Management Agency

Washington, D.C. 20472

LETTER OF MAP REVISION DETERMINATION DOCUMENT (CONTINUED)

COMMUNITY INFORMATION

APPLICABLE NFIP REGULATIONS/COMMUNITY OBLIGATION

We have made this determination pursuant to Section 206 of the Flood Disaster Protection Act of 1973 (P.L. 93-234) and in accordance with the National Flood Insurance Act of 1968, as amended (Title XIII of the Housing and Urban Development Act of 1968, P.L. 90-448), 42 U.S.C. 4001-4128, and 44 CFR Part 65. Pursuant to Section 1361 of the National Flood Insurance Act of 1968, as amended, communities participating in the NFIP are required to adopt and enforce floodplain management regulations that meet or exceed NFIP criteria. These criteria, including adoption of the FIS report and FIRM, and the modifications made by this LOMR, are the minimum requirements for continued NFIP participation and do not supersede more stringent State/Commonwealth or local requirements to which the regulations apply.

NFIP regulations Subparagraph 60.3(b)(7) requires communities to ensure that the flood-carrying capacity within the altered or relocated portion of any watercourse is maintained. This provision is incorporated into your community's existing floodplain management ordinances; therefore, responsibility for maintenance of the altered or relocated watercourse including any related appurtenances such as bridges, culverts, and other drainage structures rests with your community. We may request that your community submit a description and schedule of maintenance activities necessary to ensure this requirement.

COMMUNITY REMINDERS

We based this determination on the 1-percent-annual-chance discharges computed in the submitted hydrologic model. Future development of projects upstream could cause increased discharges, which could cause increased flood hazards. A comprehensive restudy of your community's flood hazards would consider the cumulative effects of development on discharges and could, therefore, indicate that greater flood hazards exist in this area.

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We will not print and distribute this LOMR to primary users, such as local insurance agents or mortgage lenders; instead, the community will serve as a repository for the new data. We encourage you to disseminate the information in this LOMR by preparing a news release for publication in your community's newspaper that describes the revision and explains how your community will provide the data and help interpret the NFIP maps. In that way, interested persons, such as property owners, insurance agents, and mortgage lenders, can benefit from the information.

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Kevin C. Long, CFM, Project Engineer
Engineering Management Section
Mitigation Division



Federal Emergency Management Agency

Washington, D.C. 20472

LETTER OF MAP REVISION DETERMINATION DOCUMENT (CONTINUED)

We have designated a Consultation Coordination Officer (CCO) to assist your community. The CCO will be the primary liaison between your community and FEMA. For information regarding your CCO, please contact:

Ms. Sally M. Ziolkowski
Director, Federal Insurance and Mitigation Division
Federal Emergency Management Agency, Region IX
1111 Broadway Street, Suite 1200
Oakland, CA 94607-4052
(510) 627-7175

STATUS OF THE COMMUNITY NFIP MAPS

We will not physically revise and republish the FIRM for your community to reflect the modifications made by this LOMR at this time. When changes to the previously cited FIRM panel(s) warrant physical revision and republication in the future, we will incorporate the modifications made by this LOMR at that time.

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A handwritten signature in cursive script that reads "Kevin C. Long".

Kevin C. Long, CFM, Project Engineer
Engineering Management Section
Mitigation Division



Federal Emergency Management Agency
Washington, D.C. 20472

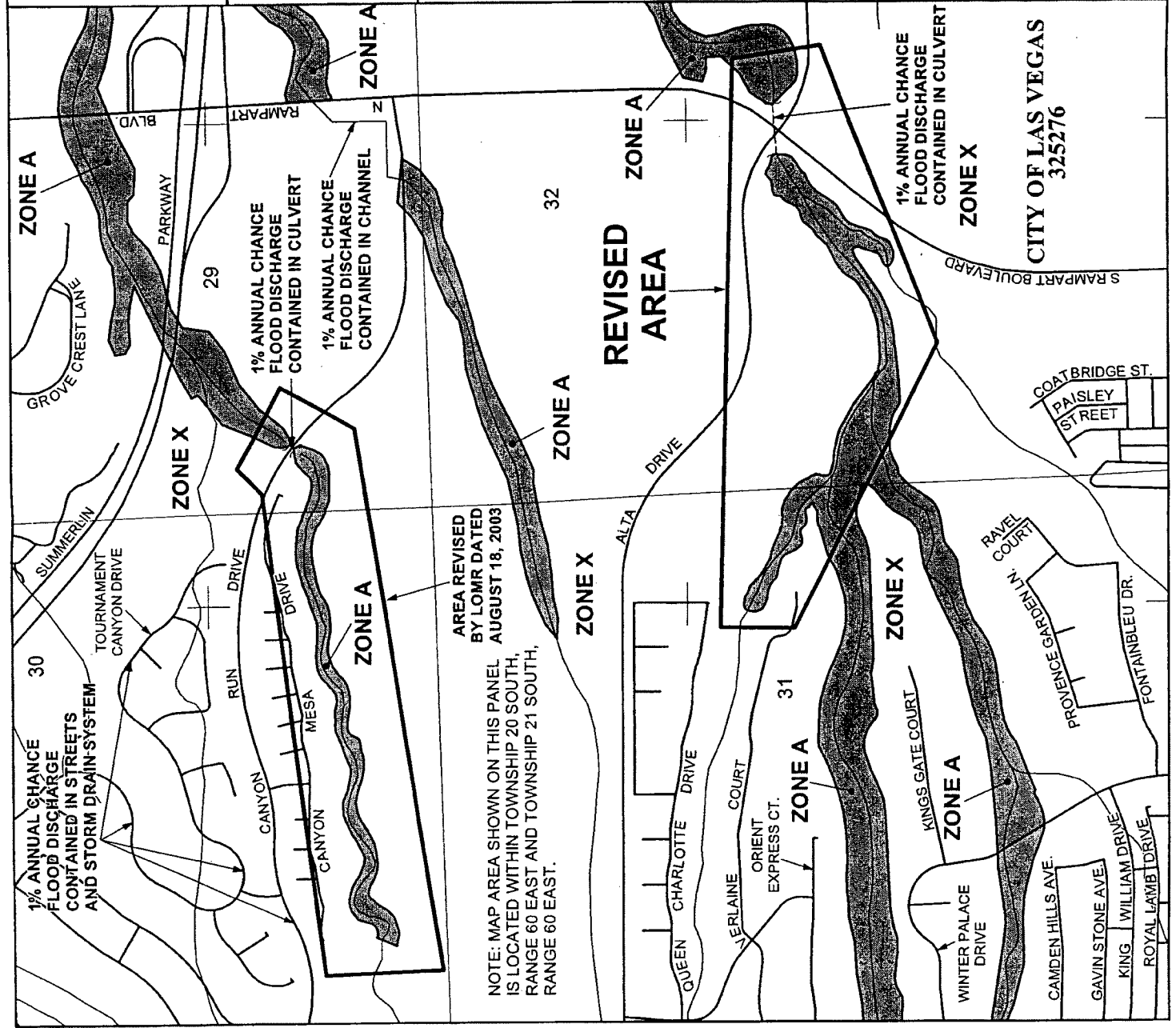
**LETTER OF MAP REVISION
DETERMINATION DOCUMENT (CONTINUED)**

This revision is effective as of the date of this letter. Any requests to review or alter this determination should be made within 30 days and must be based on scientific or technical data.

This determination is based on the flood data presently available. The enclosed documents provide additional information regarding this determination. If you have any questions about this document, please contact the FEMA Map Assistance Center toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMR Depot, 3601 Eisenhower Avenue, Alexandria, VA 22304. Additional information about the NFIP is available on our website at <http://www.fema.gov/nfip>.

Kevin C. Long

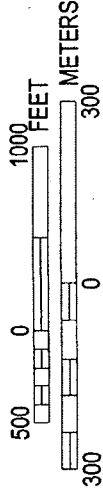
Kevin C. Long, CFM, Project Engineer
Engineering Management Section
Mitigation Division



- Legend**
- 1% annual chance (100-Year) Floodplain
 - 1% annual chance (100-Year) Floodway
 - 0.2% annual chance (500-Year) Floodplain



MAP SCALE 1" = 1000'



NFIP **NATIONAL FLOOD INSURANCE PROGRAM**

PANEL 2145E

FIRM
FLOOD INSURANCE RATE MAP

CLARK COUNTY,
NEVADA
AND INCORPORATED AREAS

PANEL 2145 OF 4090

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:
COMMUNITY NUMBER
PANEL SUFFIX

REVISED TO REFLECT LOMR

EFFECTIVE SEP 21 2006

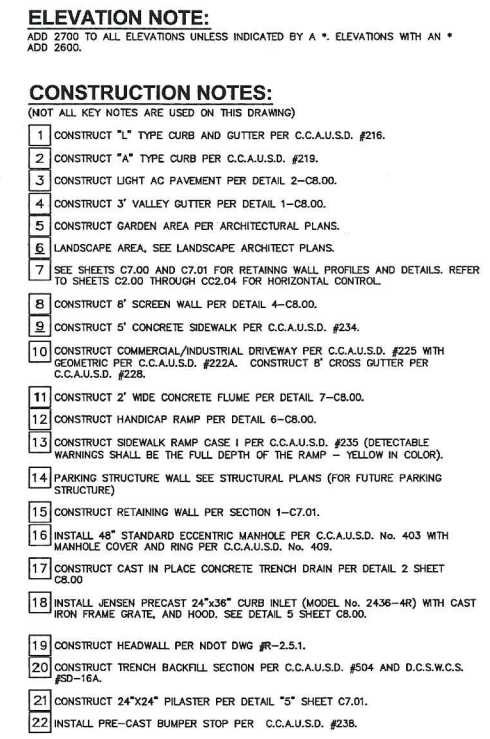
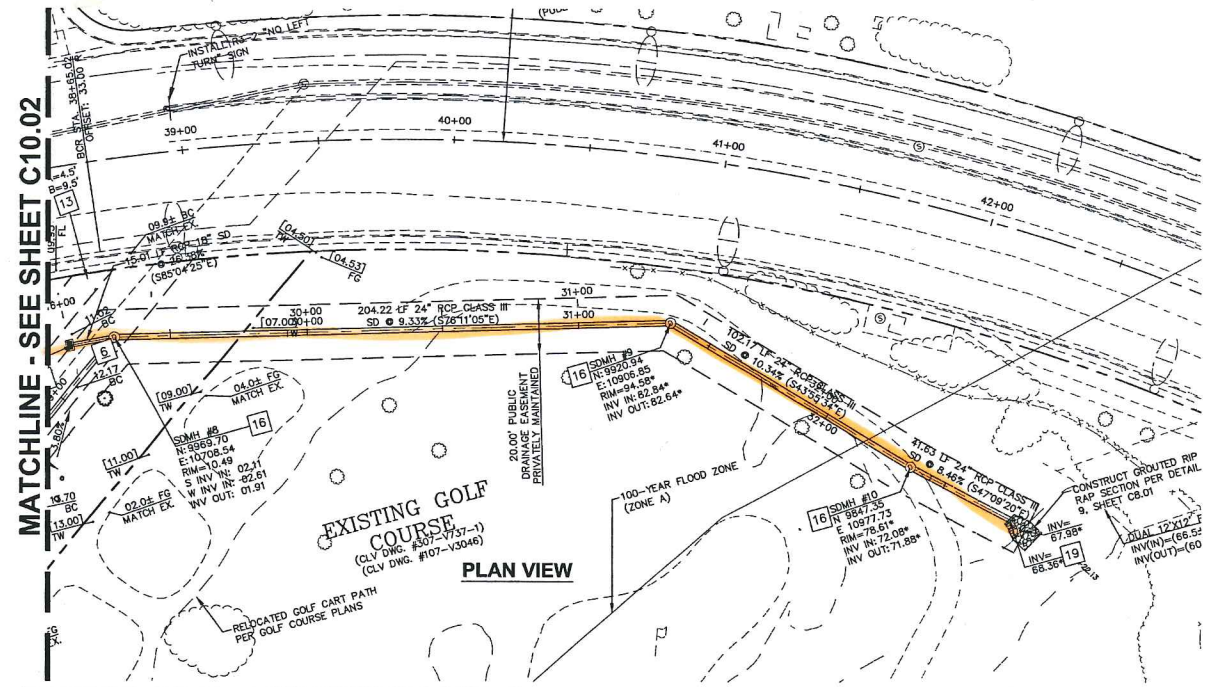
Notice to User: The Map Number shown below should be used when placing map orders; the Community Number shown above should be used on insurance applications for the subject community.



MAP NUMBER
32003C2145 E

MAP REVISED
SEPTEMBER 27, 2002

Federal Emergency Management Agency

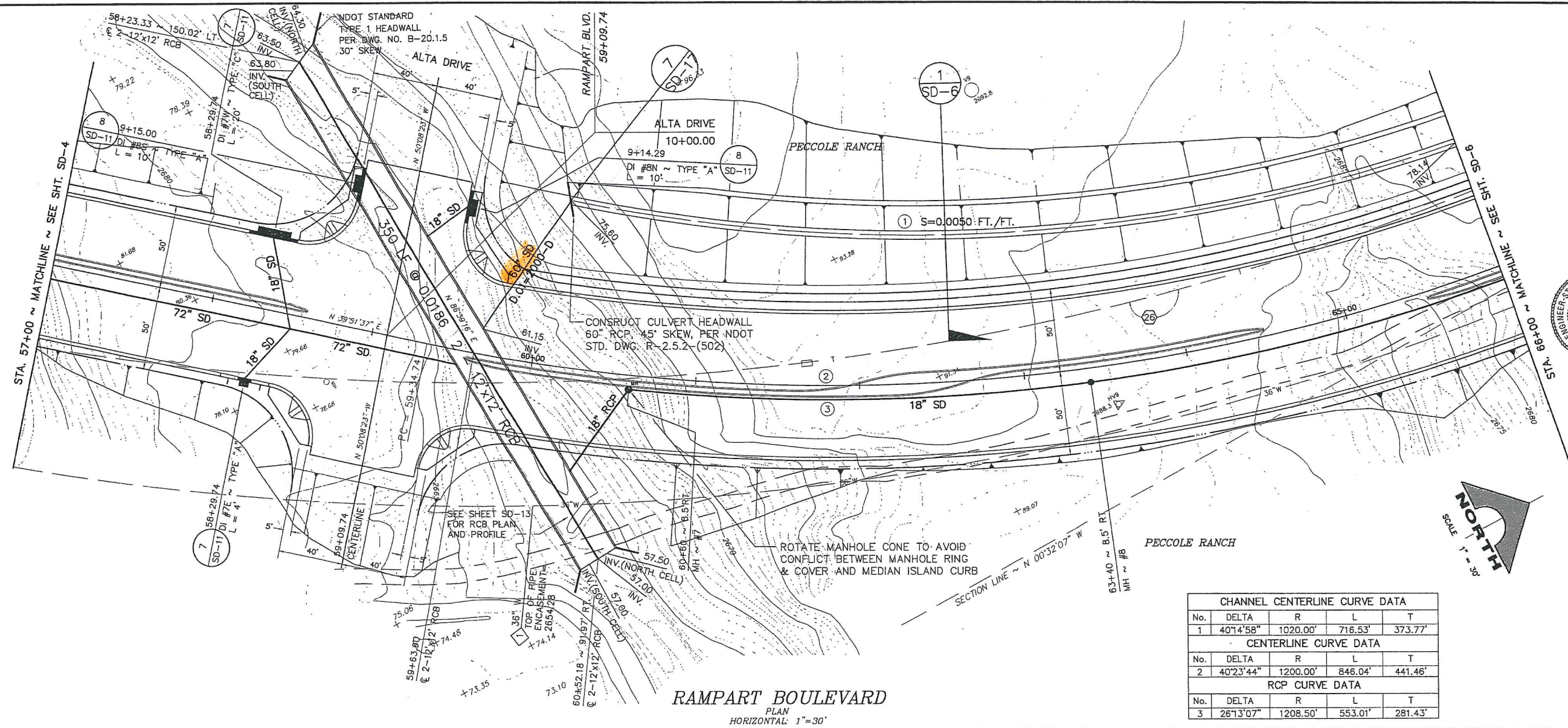


 <p>Call before you Dig Under Ground</p> <p>1-702-455-7511</p> <p>CLARK COUNTY TRADING OPERATIONS AND 1-702-920-6614</p> <p>LOCAL WAREHOUSE AND DISTRIBUTION SYSTEM</p>	<p>Avoid overhead power line contact. It's costly.</p> <p>Call before you Dig OVERHEAD</p> <p>1-702-593-6111</p>	<p>Avoid cutting underground utility lines. It's costly.</p> <p>Call before you Dig DIG</p> <p>1-800-227-2600</p>
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LEGEND

11/15/23
RB-S05

JOB NO. 412.380

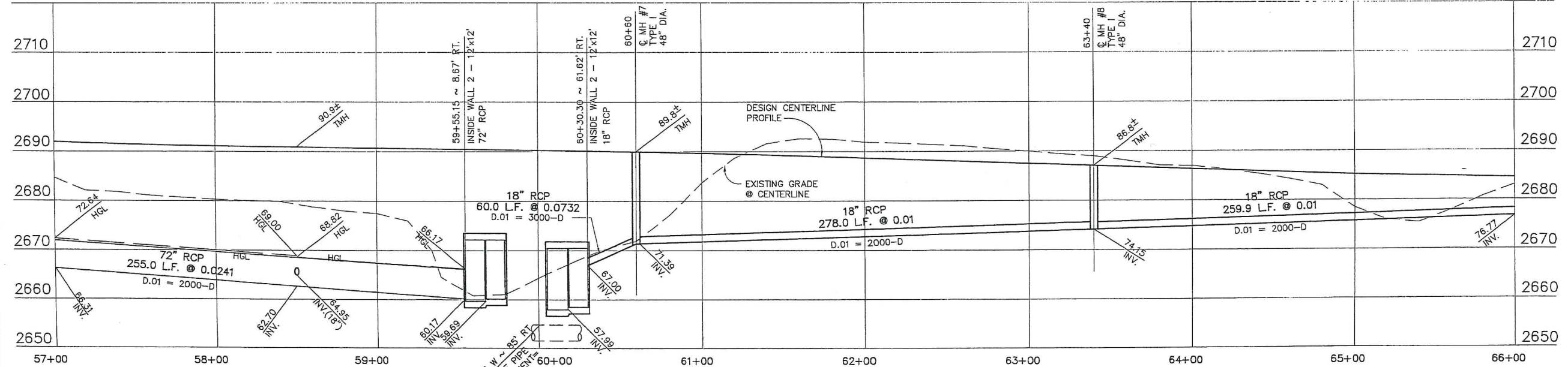


RAMPART BOULEVARD
PLAN
HORIZONTAL: 1"=30'

CHANNEL CENTERLINE CURVE DATA				
No.	DELTA	R	L	T
1	40°14'58"	1020.00'	716.53'	373.77'

CENTERLINE CURVE DATA				
No.	DELTA	R	L	T
2	40°23'44"	1200.00'	846.04'	441.46'

RCP CURVE DATA				
No.	DELTA	R	L	T
3	26°13'07"	1208.50'	553.01'	281.43'



PROFILE
HORIZONTAL: 1"=30'
VERTICAL: 1"=10'

C.L.V. DWG. No. 107-V2088
BID NO. 94.1730.03

REV	DATE	DESCRIPTION

ENGINEER: G.C. WALLACE, INC.
1555 SOUTH RAMPART BLVD., LAS VEGAS, NEVADA 89102

CITY OF LAS VEGAS
RAMPART BOULEVARD
STORM DRAIN PLAN & PROFILE
STA. 57+00 TO STA. 66+00

SHEET
SD-5
SHT 23 OF 116